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# Grain boundaries in high temperature superconducting ceramics

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## Abstract

The aim of this paper is to review the different types of grain boundaries found in  $\text{YBa}_2\text{Cu}_3\text{O}_{7-d}$  superconducting ceramics which have been investigated over the past decade. A variety of samples covering a wide range of current density  $J_c$  values are examined including: classical bulk ceramics, melt-textured bulk ceramics, bulk and thin film bicrystals with specific orientations, thin films and single crystals. From electronic coupling,  $J_c$  is expected and found to decrease with increasing grain boundary (GB) misorientation. From the magnetic behaviour, the critical current density  $J_c(H)$  is expected to increase with the number of pinning centres. The properties of the various types of GB's are discussed. All the studies reviewed lead to the conclusion that grain boundaries in YBCO materials cannot be understood without specific information about their local composition, structure and electronic state. They confirm that research on bicrystals is crucial for high-temperature superconductor development.

## 1. Introduction

Before 1987, most of the superconducting materials were characterized by a low critical temperature ( $T_c$ ) close to liquid helium temperature (4.2K). They were metal or intermetallic compounds ( $\text{Nb}_3\text{Ge}$  for instance with  $T_c=23\text{K}$ ). New high temperature superconducting cuprates (HTSC) with high  $T_c$  (above liquid nitrogen at 77K) based on lanthanides (Y, Ho, Nd for example), baryum and copper oxides were then discovered and found useful for industrial applications. Among them,  $\text{YBa}_2\text{Cu}_3\text{O}_{7-d}$  (YBCO) ceramics, with a  $T_c$  close to 90K, was synthesized and extensively studied [1], [2]. At present, other compounds like Bi-Sr-Ca-Cu-O ( $T_c =108\text{K}$ ) [2] and Tl-Sr-Ca-Cu-O ( $T_c =135\text{K}$ ) [3] have become well known.

All these HTSC's are complex layered copper oxides, separated by  $\text{CuO}_2$  layers which are

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3 mainly responsible for the superconductivity. One of the applications of the superconducting  
4 state makes use of the variation of the electrical resistance as a function of temperature, i.e. at  
5 the critical temperature the resistivity drops suddenly to zero, due to condensation and  
6 coupling between the superconducting electron Cooper pairs. The critical transport current  
7 density ( $J_c$ ) property dictates the type of application which can be achieved with a particular  
8 superconductor. The value of  $J_c$  is proportional to the percolation paths, and depends strongly  
9 on the quality of grain boundaries (GB's) in these ceramics. Understanding and controlling  
10 GB's is found to be crucial for bulk material and thin film applications. Among the structural  
11 defects formed in ceramics, GB's are especially interesting, because they act as Josephson  
12 junctions [4], [5] and thus are good candidates for elucidating the mechanism of  
13 superconductivity.  
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Jc is found to be maximum in single crystals and thin films and decreases with increasing GB content. Figure 1 shows a comparison of the different types of superconducting ceramics having been investigated over the past decade and of the corresponding ranges of Jc values measured for classical bulk ceramics, melt-textured bulk ceramics, bulk and thin film bicrystals with specific orientations, thin films and single crystals. The maximum Jc values obtained in synthesized bulk ceramics via solid-state diffusion do not exceed  $10^3$  A/cm<sup>2</sup> at 77K. When the number of GB's decreases, as in melt-textured ceramics, Jc increases ( $10^4 < Jc < 10^5$  A/cm<sup>2</sup> at 77K) and reaches a maximum for some preferential orientations, as in epitaxial thin films ( $10^6 < Jc < 10^7$  A/cm<sup>2</sup> at 77K). Beside the aspect of grain boundary transport, two fundamental steps of great importance make it difficult to obtain a material with good superconducting properties. The first difficulty is to achieve the formation of the single superconducting phase YBa<sub>2</sub>Cu<sub>3</sub>O<sub>7-d</sub> in spite of the complex Y-Ba-Cu-O phase diagram [6]. The second difficulty lies in the phase transformations and their consequences on the superconducting properties and the oxygen content. One of the most important challenges for these ceramics is to obtain high quality grain boundaries for both general and special orientations. As an example, the short coherence length ( $\xi = 1nm$ ) in these compounds requires very clean and sharp grain boundaries on the atomic scale. This is a limiting step for industrial applications. A high current density Jc value can be obtained inside a grain, due to the formation of twins as a result of the tetragonal to orthorhombic transition from high to low temperatures. On the other hand, a very low GB current density Jc can also be found, depending on the GB quality (clean versus degraded) and on the species involved.

## 2. Superconducting properties and their consequences for applications

A determining characteristic for HTSC's is their magnetic behaviour at the critical temperature Tc. They are characterized by the coexistence of superconducting and non-superconducting areas in the sample between the two critical magnetic fields Hc<sub>1</sub> and Hc<sub>2</sub>. Such zones, resulting from the penetration of the applied magnetic field (H<sub>appl</sub>), are described as vortex centres. Each of them carries a magnetic flux H. As a result, supercurrents are produced around each vortex, leading to the expulsion of the magnetic flux (Meissner effect). The resulting critical current density Jc is proportional to the number of pinning centers; the higher the number of vortices, the higher is the critical density Jc. Consequently, structural defects like point defects, dislocations, GB's and interfaces, will act as pinning centers and favour the increase of Jc due to the pinning energy dissipation. This property will compensate for the Jc limiting effect of weak-link coupling at grain boundaries. Consequently, GB Jc

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3 values can be deduced from hysteresis loop magnetic measurements at low magnetic fields  
4 (see section 5).

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6 Generally, properties of devices based on GB Josephson junctions are strongly influenced by  
7 the GB microstructure, due to the tunneling phenomenon itself, and also due to the presence  
8 of a thin interface layer between two superconductors. This layer can have either normal  
9 metal (S/N/S), insulating (S/I/S) or weakly superconducting properties. The superconducting  
10 state of Cooper pair electrons across the interface is characterized by a pseudo-wave function  
11 which depends on the phase  $\Delta F$  of the superconducting order parameter  $\Delta$  (OP). The  
12 Josephson effect is very sensitive to the phase shift  $\Delta F$  of this order parameter ( $J_c = J_1 \sin \Delta F$ ).  
13 For conventional low  $T_c$  superconductors, the OP is characterized by « s-wave symmetry »  
14 with isotropic properties. As a result, phase and current are both constant. For HTSC's, the OP  
15 presents a « d-wave symmetry » characterized by anisotropic properties and an internal phase  
16 whose value depends on crystallographic orientation, in the same way as the current  $I_c =$   
17  $f(\Delta F)$  does. This latter is maximum only along some crystallographic orientations and null  
18 outside. This characteristic is fundamental for the understanding of GB properties. Figure 2  
19 schematizes a S/I/S junction with its characteristics for both types of superconducting  
20 mechanisms. In low- $T_c$  superconductors (LTS) the coherence length  $\xi = 10^2$ - $10^3$  nm is large  
21 and isotropic, compared to HTSC's for which  $\xi$  is of the order of the interatomic d-spacing  
22 ( $\xi \approx 1$  nm) and anisotropic. Such a small value makes the OP amplitude and phase very  
23 sensitive to the effect of a local structural change. Consequently, any change in GB  
24 misorientation on the atomic scale will strongly affect the coupling between the two grains,  
25 leading to a local decrease of  $J_c$ , as shown for bicrystal thin films (see section 8).

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27 Thus, it is the grain boundary misorientation which controls the macroscopic  $J_c$  characteristic,  
28 due to decreasing coupling between the two grains. The higher the misorientation angle, the  
29 lower the coupling is expected to be. Hence,  $J_c$  is expected to have a defined value for a  
30 specific misorientation between the two grains. High angle grain boundaries (HAGB) act as  
31 Josephson junction weak-links. Consequently, a HAGB in the microstructure introduces a  
32 network of weak-links (corresponding to regions of reduced  $J_c$ ) into a superconducting path  
33 which otherwise would have  $J_c$  characteristics appropriate for applications. Nevertheless, it  
34 was shown that some HAGB's are strongly coupled, leading to rather good properties as in the  
35 BSCCO system, although YBCO ceramics show a weak-link character with locally oxygen  
36 deficient GB areas. It has become increasingly clear from electromagnetic measurements and  
37 microstructural studies that weak-link boundaries are heterogeneous on various scales. The  
38 characteristic properties of Josephson junctions, like weak-links, include a strongly magnetic  
39 field dependent  $J_c(H)$  which can decrease by more than an order of magnitude for weak fields  
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of just a few (1-10) millitesla. Such  $J_c(H)$  characteristics clearly pose a serious problem for magnetic applications (energy storage systems, motors, generators,...). As a result, a great number of HAGB's represent an obstacle to the development of bulk materials for such applications. Improvement of the  $J_c$  limiting effect of weak-link coupling at grain boundaries can be achieved, either by improving the  $J_c$  of individual grain boundaries, or by texturing the materials in order to reduce the number of weak-link grain boundaries in the current path. The high sensitivity of  $J_c$  to weak magnetic fields, at grain boundary Josephson junctions, enables HTSC applications in electronic materials and particularly in thin films (squids).

The anisotropy of coherence length values in the YBCO superconducting plane ( $\xi_{ab} = 1-2\text{nm}$ ) and in the c-axis direction ( $\xi_c = 0.3\text{nm}$ ) leads to a dependence of various superconducting properties on the crystallographic orientation of the sample. Based on the  $d_{x^2-y^2}$  symmetry [7], [8] of the superconducting order parameter, a strong coupling is expected along [100] and [103] orientations, while [001] and [110] will present a weak coupling. Thus, as schematized in figure 3, only some orientations will carry the supercurrent. Among them, GB's containing (001) superconducting planes will be the most favourable.

From electronic coupling, it can be expected that  $J_c$  will decrease with increasing GB misorientation. This effect is used to study Josephson junction applications based on thin films. From the magnetic behaviour, the critical current density  $J_c(H)$  is expected to increase with the number of pinning centres, such as structural defects (point defects, dislocations, twins, clean interfaces). This particular property is used for high current transport applications in bulk ceramics. Among these cuprates, YBCO is the one that has been most extensively studied in bulk ceramics, thin films and heterostructures. Because of its particular interest, YBCO has been chosen as a model for understanding structure and superconductivity mechanisms.

The aim of this paper is to review the different types of grain boundary configurations and properties found in the YBCO system for bulk ceramics, melt-textured ceramics, thin films, bicrystals and single crystals used in the field of superconduction research and applications.

### **3. YBaCuO system properties and their consequences on grain boundary structure**

#### ***3.1. Structure and properties***

YBCO superconducting ceramics, like almost all HTSC, have a complex layered structure of perovskite blocks containing one or a few  $\text{CuO}_2$  layers which are currently considered to be mainly responsible of the superconductivity. In these layers, the copper atoms form a square network, whereas the oxygen atoms are placed along the copper-oxygen chains (fig. 3a). As

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3  $\text{YBa}_2\text{Cu}_3\text{O}_{7-d}$  has an orthorhombic structure based on that of perovskite oxides, it belongs to  
4 the class of compounds displaying, for copper atoms, a mixed valence which leads to a  
5 flexible chemistry. Another particular aspect of this system is the possible variation in  
6 cationic and oxygen stoichiometry.  
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10 The formation of the YBCO superconducting phase (also called the (123) phase referring to  
11 the cationic content in Y, Ba, and Cu atoms) involves a second order reaction transforming  
12 the high temperature tetragonal insulating  $\text{YBa}_2\text{Cu}_3\text{O}_6$  phase into the low temperature  
13 orthorhombic superconducting structure. The crystallographic structure of YBCO strongly  
14 depends on oxygen stoichiometry. The lower  $O_d$ , the higher is  $T_c$ . Its maximum value is  
15 obtained for an oxygen deficiency  $d = 0.03$ . For  $d = 1$ , the structure becomes tetragonal  
16 corresponding to an insulating material. Within this range, crystal structure and physical  
17 properties undergo changes. Two orthorhombic structures have been characterized, called  
18 "Ortho I" and "Ortho II". The first one refers to the fully oxygenated superconducting phase.  
19 The second one contains vacancies along the O-Cu-O chains and particularly one oxygen  
20 vacancy every two structural unit cells. The first one corresponds to an oxygen content in the  
21 range  $O_7$ - $O_{6.9}$  with a critical  $T_c$  remaining at 91K. The second one is characterized by an  
22 oxygen content of  $O_{6.6}$  or  $O_{6.7}$ , for which  $T_c$  drops to a plateau at 60K and finally to zero  
23 between  $O_{6.5}$  and  $O_{6.4}$ . These various oxygen concentrations and related YBCO structures are  
24 summarized in Table 1. For special oxygen contents ( $0.15 < d < 0.6$ ), various types of oxygen  
25 vacancy ordering occur. They have been extensively studied by Transmission Electron  
26 Microscopy (TEM) and electron diffraction patterns by Alario-Franco et al [9, 10]. Other  
27 authors [11, 12] give numerous details on oxygen vacancy ordering near  $O_{6.5}$ . A review of  
28 YBCO and its derived structures can be found in reference [13]. These experimental results  
29 are in good agreement with theoretical calculations reported by Ceder [14] and Matic et al  
30 [15] and more recent studies based on first principle calculations which predict all possible  
31 oxygen vacancy orderings [16].  
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48 Figure 4 shows that lattice parameters change as a function of oxygen deficiency  $d$  for various  
49 oxygen partial pressures [6]; note the change of the transformation temperature from 798K to  
50 943K. This corresponds to an oxygen gain along the Cu-O chains of the tetragonal structure  
51 (fig.3 and fig.4). It generates an increasing strain in the crystal due to the simultaneous  
52 increase of lattice parameter  $b$  and decrease of lattice parameter  $a$ . Twins are formed and  
53 induce stress relaxation. The higher the number of twins formed, the higher is the stress.  
54 Twins are grain boundaries of special symmetry lower than that of the single crystal. Due to  
55 their origin, they are found in all superconducting YBCO crystals, bulk ceramics, melt-  
56 textured ceramics and thin films. Their presence increases  $J_c$  inside each grain, because they  
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act as pinning centres for the vortices. Twins are not the subject of this review and will not be described here.

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### 3.2. Phase diagram and stoichiometry

The important characteristic in the Y-Ba-Cu-O system is the non-congruent melting behaviour of the  $\text{YBa}_2\text{Cu}_3\text{O}_{7-d}$  compound which favours the formation of secondary phases such as CuO,  $\text{Y}_2\text{O}_3$ , BaO,  $\text{BaCuO}_2$  and  $\text{Y}_2\text{BaCuO}_5$ . The cationic non-stoichiometric (123) phase was observed in many RBCO ceramics, as well as secondary phases with specific properties. An understanding of the phase diagram has been mainly sought in order to determine the conditions of formation of the (123) phase and that of the secondary phases which also affect the physical properties of the bulk and of the interfaces. These secondary phases are formed outside of the thermodynamic growth conditions of the (123) superconducting phase. Cationic non-stoichiometry can be understood from the complex Y-Ba-Cu-O ternary phase diagram associated to the BaO- $\text{Y}_2\text{O}_3$ -CuO system (fig. 5). The diagram contains different domains of coexistence of solid-solid and solid-liquid phases. It shows the most likely domains for non-superconducting secondary phases to be (132), (211), beside the (123) phase. Among the secondary phases formed out of equilibrium, one may find barium, copper oxides or deficiency phases which are not superconducting such as (234), (235), and (113) [17], [18] and [19]. These authors observed in various ceramics synthesized by classical sintering, like  $\text{RBaCuO}$  (R=Y and Ho), a large variety of cationic non-stoichiometric ceramics. The (123) superconducting phase can be formed either by solid-solid diffusion (close to the domain of the (132) phase) or by solid-liquid diffusion in the region of the (211) phase. Depending on thermodynamic conditions, the resulting (123) phase will have specific microstructures and properties. At high temperature, the YBCO phase decomposes (above 1233K), due to non-congruent melting. Depending on oxygen partial pressure, solid-solid diffusion takes place between 1193K and 1233K. Grain growth governed by solid-solid atomic diffusion should lead to clean grain boundaries. Between the domain of  $\text{BaCuO}_2$ -CuO and the (211) region, there is formation of a liquid with the diffusion governed by a liquid-solid process. At still higher temperatures near the peritectic reaction ( $T=1288\text{K}$  in atmospheric conditions) YBCO decomposes in a liquid-rich phase containing CuO,  $\text{BaCuO}_2$  and (211) precipitates. During this step, solid-liquid diffusion occurs leading to dissolution of the (211) precipitates into the liquid. This reaction is used to grow melt-textured ceramics. Grain growth governed by solid-liquid diffusion can lead to grain boundaries with secondary phases due to recrystallization of the liquid. This will be detailed in the section dealing with grain boundaries in melt-textured ceramics (see section 6).

The role of oxygen partial pressure should also be stressed in connection with the structural phase diagram. This diagram highlights the effect of oxygen partial pressure and of oxygenation temperature on the formation of the (123) oxygen stoichiometric phase, as

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3 reported in figure 6. In particular, it shows the narrowness of the domain in which the  
4 optimum oxygen content for the (123) phase is achieved. It can be noticed that both the  
5 oxygen content at the orthorhombic-tetragonal transition and the transition temperature  
6 decrease with decreasing oxygen partial pressure [6].  
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10 Finally, the complexity of this system makes intrinsically difficult the formation of a single  
11 YBCO phase with oxygen and cationic stoichiometry. Improving YBCO growth has led to a  
12 better knowledge of the structures and superconducting properties. As a consequence, an  
13 increasing number of applications have been developed with bulk ceramics (for high current  
14 transport), thin films (electronic device applications, squids) and heterostructures  
15 (ferroelectric device applications, hard memories, ...).  
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#### 22 **4. Grain boundaries in bulk ceramics**

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24 Conventional ceramic sintering leads to a current density with a maximum value  
25  $J_c=10^3 \text{ A/cm}^2$  at 77K (fig. 1) which is one thousand times less than that obtained for thin films  
26 and single crystals ( $J_c=10^6 \text{ A/cm}^2$ ). This large difference has various origins :

- 27 (i) The strong dependence of  $J_c$  on crystallographic orientation which is due to the  
28 intrinsic anisotropic properties of the YBCO structure;
- 29 (ii) The oxygen content due to oxygen self-diffusion;
- 30 (iii) The oxygen content dependence on GB misorientation;
- 31 (iv) The quality of the grain boundaries, either clean or damaged;
- 32 (v) Last but not the least , the type of processing used to make bulk samples ready for  
33 applications and leading to high quality GB's.

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36 All these parameters are interacting simultaneously inside the grains and for each GB in the  
37 ceramic. Therefore,  $J_c$  results from a combination of these phenomena.  
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##### 46 **4.1. Oxygen diffusion as the limiting step for grain boundary properties in polycrystals**

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48 An important challenge for obtaining good superconducting properties is to control the  
49 elaboration process in order to reach the maximum oxygen content  $O_{6.9-O_7}$  . This problem  
50 can be dealt with by considering oxygen self-diffusion in ceramics. Sabras et al [20]  
51 investigated oxygen self-diffusion and its effects on grain boundary oxygen content by means  
52 of Secondary Ion Mass Spectroscopy (SIMS). From diffusion profiles using oxygen  $O^{18}$  as a  
53 tracer and from oxygen ion images, these authors found a heterogeneous distribution of the  
54 tracer in the material, as well as an influence of microcracks on oxygen diffusion. On  
55 polycrystalline ceramics exhibiting various grains sizes and an inhomogeneous grain size  
56 distribution, they find an oxygen diffusion coefficient along grain boundaries of the same  
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3 order as in the bulk. Figure 7 depicts these experimental results and those found in the  
4 literature. Figure 7a shows oxygen diffusion depth profiles on a sample polished according to  
5 a small angle ( $\alpha = 1.56^\circ$ ,  $T = 823\text{K}$ ,  $p_{\text{O}_2} = 22\text{kPa}$ ). It exhibits the presence of microcracks in  
6 the ceramic. In Figure 7b an ion image obtained from  $\text{O}^{18}$  species shows the heterogeneous  
7 distribution of the tracer in the material, as well as the influence of microcracks on the  
8 oxygen diffusion. The results reported in references [20], [21], [22] are gathered on Figure 7c  
9 where Arrhenius plots of oxygen self-diffusion are drawn, corresponding to Arrhenius plots  
10 of volume and GB diffusion along the (ab) planes and parallel to the  $c$  axis in single crystals.  
11 All these data are in general agreement with the oxygen diffusion behaviour in a ceramic,  
12 suggesting that oxygen diffusion in a polycrystal is clearly governed by GB diffusion. This  
13 latter is the limiting step, because the diffusion coefficient in the  $\text{CuO}_2$  superconducting (ab)  
14 planes is  $10^6$  times larger than along the  $c$  axis i.e. the direction perpendicular to the (001)  
15 superconducting planes. This strong anisotropy of diffusion was observed and quantified for  
16 the first time on single crystals by Rothman et al [21] and on polycrystals by Routbort and  
17 Rothman [23].

18 An additional anisotropy of oxygen diffusion exists in the (ab) planes : the faster diffusion  
19 being along the  $b$  axis, i.e. along the O-Cu-O chains which carry the oxygen vacancies.  
20 Therefore, the anisotropic oxygen diffusion in the (001) planes and along the [001] direction  
21 of the lattice will strongly affect oxygen diffusion inside each grain of the ceramic during  
22 processing. Therefore, the sample geometry will strongly affect the final properties of the  
23 ceramics. This explains the smaller critical density values found in bulk samples, compared to  
24 thin films which are deposited according to a favourable orientation.  
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#### 4.2. Sintering parameters

29 Generally, sintering requires a high temperature step for the growth, followed by cooling to  
30 room temperature. In these conditions, the (123) phase obtained is not superconducting and is  
31 generally oxygen deficient. It requires a second step of annealing around 823K in order to  
32 optimize the oxygen content. Even if the initial powder is stoichiometric, the synthesized(123)  
33 phase contains oxygen vacancies. Consequently, there may be local changes in the  
34 microstructure and in properties which are related to the oxygen content, such as critical  
35 temperature, lattice parameters.  
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43 Various sintering parameters are exploited to densify the material, to reach the maximum  
44 oxygen content of the (123) orthorhombic phase and to produce various microstructures with  
45 specific features. The challenge in synthesizing dense materials is to avoid microcracks due to  
46 an inhomogeneous distribution of grain sizes and to keep an adequately interconnected  
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3 porosity inside the material, which ensures oxygenation into the bulk.  
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5 Four main steps are involved in the growth of the (123) phase:  
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- 7 (i) The first one is the preparation of the starting powders from different materials:  
8 oxides, nitrates or carbonates. According to their nature and quality, various kinds of  
9 ceramics may be obtained. These initial powders must consist of a high purity single  
10 phase to ensure the formation of the single(123) phase as reported in reference [24].  
11  
12 (ii) The second step, sintering at high temperatures, requires well-defined experimental  
13 conditions concerning the heating rate, the annealing time for the grain growth and  
14 the oxygen gas flow. These conditions will determine either solid-solid or solid-  
15 liquid diffusion reactions.  
16  
17 (iii) The third step is the cooling stage from high temperature, which is performed either  
18 with a low cooling rate or by quenching under oxygen gas flow, depending on the  
19 nature of the study. Slow cooling stabilizes the structure and morphology of the (123)  
20 phase. Quenching is the only way of preserving metastable high temperature phases.  
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22 (iv) The fourth step is the oxygenation of YBCO : it is performed by annealing between  
23 753K and 823K under oxygen gas flow. This step, and particularly the choice of the  
24 annealing time at this temperature, will determine the superconducting properties.  
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32 As these parameters act simultaneously, all these steps are critical and have to be controlled,  
33 because they strongly influence the physical properties, microstructure and chemical  
34 composition of the synthesized ceramics.  
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37 Various types of sintering were investigated for the synthesis of bulk ceramics. Among them  
38 we find classical sintering [25], [17], hot-press sintering [26], [27], [18], [19], and melt-  
39 textured sintering [28], [29], [30], [31]. For classical sintering, powders are pressed into  
40 pellets at room temperature under uniaxial or isostatic pressure, and then sintered. In hot-press  
41 sintering, an isostatic pressure from 5 Kbars to 40Kbars [18] is maintained during sintering.  
42 In the melt process, pellet sintering is performed with a thermal gradient applied to the  
43 substrate [30], [32], under a magnetic field [31] or using flux growth from a seed [33], [34].  
44 Thermodynamic equilibrium and out-of-equilibrium states vary from one type of sintering to  
45 the other one and can also vary inside a given ceramic from one point to another . Considering  
46 all the types of sintering which have been investigated, it appears that hot-press processing  
47 and the melt-textured process are the best means to increase  $J_c$ . The former implies solid-  
48 solid and the latter solid-liquid diffusion.  
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## 5. Grain boundaries from solid-solid diffusion

### 5.1. Influence of processing on grain boundary microstructure and properties

Studies by Ayache et al [25, 35] have reported the influence of sintering conditions on microstructure and physical properties. They described the effects of the high temperature annealing stages, of the oxygenation step, and those of either a new annealing using classical sintering, or of hot-press sintering under various conditions. Initially, two samples were hot-pressed and sintered at 1199K during respectively 13h (sample A<sub>0</sub>) and 96h (sample B<sub>0</sub>). Next, they were submitted to an oxygenation step at 753K (respectively for 24h and 72h). Several effects of the high temperature stage were observed: increase of the density from 88% to 92%, of the grain size from 3 $\mu$ m to 5 $\mu$ m, of the critical temperature T<sub>c</sub> from 43K to 63K, of J<sub>c</sub> by a factor of 3 from 130 to 393 A/cm<sup>2</sup>, and a decrease of the width  $\Delta$ T<sub>c</sub> from 16K to 12K. A second sintering (samples A<sub>1</sub> and B<sub>1</sub>) favoured the increase of T<sub>c</sub> and a decrease of  $\Delta$ T<sub>c</sub>, improves the magnetic property of the grains, i.e. the shielding efficiency was much better in the second sample inside the grain, although J<sub>c</sub> became smaller. It was also shown, from a grain boundary study of YBCO sintered under quasi-isostatic pressure, that a small change in the oxygenation temperature during the final step produces a drastic change in the microstructure (density, grain size, oxygen content from O<sub>7</sub> to O<sub>6</sub>) of different types of GB's (clean versus damaged GB) and in the superconducting properties.

### 5.2. Influence of microstructure on transport properties

The superconducting transition can be observed by plotting the resistance as a function of temperature. The transition profile can be separated in two regimes [36], [37], [38]. The first one, called the main transition regime, corresponds to the drop of the resistance in the grains. It depends mainly on the chemical composition and on the oxygen stoichiometry of these grains. The second one, lying immediately below the main one and covering the range down to zero resistance, is the tail regime. Transport in this regime is controlled by the grain boundaries (weak-links) and corresponds to the temperature range where the Josephson coupling energy of the weak-links is insufficient to overcome the thermal energy. This regime becomes broader with the presence of defects in the grain boundaries (intergranular phases, misorientations, GB oxygen deficiency, or GB cationic deficiency). Figure 8 shows the experimental R(T) measurements obtained from sintered samples A<sub>0</sub>, A<sub>1</sub>, B<sub>0</sub> and B<sub>1</sub>. The results show clearly an increase in the transition width as T<sub>c</sub> decreases, revealing a low oxygen content and a low homogeneity in the ceramic, and also the presence of secondary phases at grain boundaries. The curves also indicate that an additional sintering of sample A<sub>0</sub> and B<sub>0</sub> improves the transition. The semi-conducting behaviour of sample A<sub>0</sub> has disappeared

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3 in sample A<sub>1</sub> which still exhibits a wide  $\Delta T_c$  and a tail region. In sample B<sub>1</sub>, the oxygen  
4 content is optimum, but the tail effect has increased compared to sample B<sub>0</sub>.

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6 Such an additional annealing increases the oxygen content and improves the quality of the  
7 weak-links, as shown by TEM analysis of sample A<sub>1</sub> (figure 9) . This figure shows a grain  
8 surrounded by four other grains and particularly by different clean GB's (fig. 9a) with various  
9 misorientation angles : a small angle GB (4°) characterized by (001) planes in the two grains  
10 (fig. 9b), a clean triple junction showing twinning inside the grains (fig. 9c) and a faceted  
11 HAGB exhibiting (001) planes in one grain (fig. 9d).

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13 GB TEM analysis of sample B<sub>0</sub> indicates the presence of second phases like BaO (and/or  
14 CuO) in HAGB (fig. 10). The presence of a second phase is often an indication of a local  
15 liquid state in the ceramic [35] . Figure 10a shows the HAGB change from a symmetric  
16 faceted GB (fig. 10b) to an asymmetric GB (fig. 10c) in the vicinity of an intergranular defect  
17 (fig. 10a). Such a GB has a special orientation close to the coincident site lattice (CSL)  $\Sigma 13$   
18 GB and contains (001) CuO<sub>2</sub> superconducting planes which are favourable in terms of  
19 current. Even with a high angle misorientation of 67°- 69°, the GB could act as a Josephson  
20 junction weak-link. As this GB contains a second phase, it is not superconducting.

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22 For sample B<sub>1</sub>, R(T) has been seriously improved in the first part of its profile (fig. 8), but the  
23 second part of this curve, corresponding to the tail regime where the transport is controlled by  
24 grain boundary weak-links, becomes broader due to the presence of intergranular phases and  
25 GB oxygen deficiency. TEM analysis of this sample shows strong changes of the  
26 morphology, structure and chemistry on different scales. Figure 11 illustrates the resulting  
27 grain size gradient observed by polarized optical microscopy, scanning electron microscopy  
28 (SEM) and TEM. This ceramic contains elongated crystals 5 $\mu$ m to 100 $\mu$ m in length. This  
29 elongated shape (fig. 11a and fig. 11b), generally found in these ceramics, is due to the fact  
30 that the direction of maximum grain growth is parallel to the (ab) planes (anisotropic  
31 direction). The presence of cavities or microcracks, whose size ranges between 10 $\mu$ m to  
32 20 $\mu$ m, is due to an inhomogeneous grain size distribution and to grain misorientations. The  
33 external part is well oxygenated as can be seen from the splitting of the 110 reflections in the  
34 electron diffraction pattern (right part of fig. 11c). The inner part is characterized by a higher  
35 density, a lower oxygen content and the absence of splitting of 110 reflections (right part of  
36 fig. 11d). The oxygen gradient clearly affects the lattice parameters deduced from the  
37 diffraction patterns and also the twinning morphology. In particular, the twins present in the  
38 external part (left part of fig. 11c) of the ceramic are fully relaxed and the lattice parameters  
39 correspond to an orthorhombic structure with an oxygen content close to O<sub>7</sub>. The twins of the  
40 inner part are ferroelastic-like (left part of fig. 11d), and are not completely relaxed by the  
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3 phase transformation. The lattice parameters are those of a tetragonal (123) phase with an  
4 oxygen content close to  $O_{6.5}$ . The microstructure of this inner part explains the remaining tail  
5 region in the  $R(T)$  curve of figure 8.  
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### 8 9 10 **5.3. Magnetic measurements and weak-link behaviour**

11 The use of hysteresis loop measurements under increasing magnetic field (from 0-250 mT to  
12  $H_{\text{appl}} > H_{c2}$ ) was investigated on ceramics by [39] in order to measure the current density.  $J_c$   
13 was calculated from Bean's Model [40]. The  $J_c$  versus field behaviour was very similar to that  
14 described by a simple self-field limitation hypothesis [41]. These authors found a good  
15 agreement between  $J_c$  values deduced from this model and from transport current  
16 measurements. Magnetic hysteresis loops under low magnetic fields at 4.2K are directly  
17 correlated to the GB weak-link behaviour. The higher the hysteresis area, the higher is the  
18 shielding efficiency of the weak-links [39]. The shielding effect improves after a new  
19 annealing revealing a better magnetic behaviour inside the grains. Figure 12 gathers the  $J_c$   
20 results calculated from Bean's model for samples  $A_0$ ,  $A_1$ ,  $B_0$  and  $B_1$   
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### 30 **5.4. Critical current density and grain size dependence**

31 Bulk ceramics show a strong dependence of  $J_c$  on grain size [25], with an exponential  
32 decrease, comparable to that found in  $J_c$  curves as a function of misorientation in the case of  
33 bulk bicrystals and thin film bicrystals (see paragraph 8).  $J_c$  values, calculated from magnetic  
34 hysteresis loops measurements, as a function of grain size are related to grain boundary  
35 transport in ceramics. The smaller the grain size, the higher is  $J_c$ . In figure 12 the results of  
36 classical sintering (ceramic C) and hot-press sintering (ceramics  $A_0$ ,  $A_1$ ,  $B_0$  and  $B_1$ ) are  
37 compared. The highest value of  $J_c$  is obtained by classical sintering which gives the lowest  
38 porosity (78%), the maximum oxygen content ( $O_7$ ) and the minimum grain size ( $2\mu\text{m}$ ). The  
39 smallest value corresponds to the largest grain size (from 5 to  $100\mu\text{m}$ ) with an  
40 inhomogeneous distribution, a high density (96%) and an oxygen gradient between the inner  
41 and external parts of the material. Compared to classical sintering, the hot-press process has  
42 the advantage of giving the highest density ceramics. The drawback is the limited oxygen  
43 diffusion due to higher compacity.  
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54 There is a competition between density, grain size and oxygen content. Oxygen diffusion is  
55 favoured by porosities which play a possible role as diffusion paths. High density ceramics  
56 will have more difficulty to reach the maximum oxygen content, as compared to low density  
57 ceramics which will be fully oxygenated. The presence of a grain size gradient, as observed in  
58 sample  $B_1$ , prevents the connection between grains and makes the  $J_c$  value decrease strongly  
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3 (figure 12).  
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## 8 **6. Grain boundaries from solid-liquid diffusion : Melt-textured ceramics**

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10 Melt-textured processes allow the synthesis of YBCO ceramics with highly improved  
11 transport properties in the presence of a large magnetic field, due to aligned microstructures  
12 almost free of weak-link grain boundaries [42], [43]. Melt-processing involves the peritectic  
13 melting of the YBCO phase well above the peritectic temperature (1288K in air), yielding a  
14 solid phase  $Y_2BaCuO_5$  plus a liquid phase (called «m1») having an approximate  
15 stoichiometry Y/Ba/Cu : 1/16/27 [44]. On subsequent slow cooling through the peritectic  
16 temperature, directional solidification of YBCO occurs. It was demonstrated from TEM  
17 chemical analysis of melt-textured samples that the YBCO phase grows directly from an  
18 undercooled yttrium-bearing liquid and not from heterogeneous nucleation sites on  
19  $Y_2BaCuO_5$  crystals [45], [46]. The growth rate limiting factor is expected to be yttrium  
20 diffusion at the liquid-YBCO interface. The difference between the growth rate parallel to  
21 (001) superconducting planes and that along the perpendicular direction  $c$ , induces a  
22 microstructure characterized by aligned platelets separated by gaps [47]. These growth-  
23 induced defects are filled with secondary phases which have solidified from the trapped  
24 liquid. The knowledge of the stable and metastable equilibrium phases at high temperatures,  
25 especially in the YBCO primary solidification region, has proved essential to determine the  
26 effective conditions for both single crystal growth and YBCO peritectic crystallization. Until  
27 now, the solid-state equilibrium, the melting temperatures, the extension of the primary  
28 crystallization fields of the solid phases and their dependence on oxygen pressure have been  
29 extensively studied [48], [49], [50], [51]. A review of the chemical principles of the  
30 preparation of metal-oxide superconductors can be found elsewhere [52].  
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### 48 **6.1. Influence of processing on microstructure**

49 The advantage of melt-textured ceramics is the large extent of a single crystallographic  
50 domain, comparable in size to a single crystal. Therefore, they can be used for direct  
51 measurements of transport properties. Compared to ceramics made by a solid-solid diffusion  
52 process, melt-textured ceramics contain far less GB's due to directional melt growth. They  
53 look-like quasi «single-crystals» which contain, in addition, residual gaps from the  
54 crystallization of the liquid. These gaps appear as lines in optical microscopy images. Their  
55 microstructure also contains  $Y_2BaCuO_5$  (211) precipitates resulting from the peritectic  
56 transformation.  
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3 In these materials,  $J_c$  is mainly due to the pinning energy of the vortices at the interfaces  
4 between precipitates, (211) and (123) phases, and at twin grain boundaries. The striking  
5 feature of these melt-textured ceramics is that a single grain can extend over the whole length  
6 of the sample, particularly when the melt process is performed under a magnetic field. Such  
7 conditions favour the alignment of the superconducting planes parallel to the applied field  
8 [31], so that the sample contains only one or two large domains of the order of a few  
9 millimeters (10-30mm), separated by low angle GB's. As an example of YBCO melt-grown  
10 under magnetic field, figure 13a shows an optical polarized image with two large domains  
11 exhibiting a small misorientation of about  $10^\circ$ . TEM images (fig.13b) show that twins  
12 crossing the growth defect are either coherent or incoherent. The growth defect corresponding  
13 to a gap filled by the liquid during (123) growth, keeps the same orientation in the sample,  
14 parallel to the (001) superconducting planes. The (123) phase also keeps the same orientation  
15 across the (211) precipitates.

16 Besides, the melt-process is also commonly used [32] on substrates like MgO single crystals  
17 or polycrystalline  $Y_2O_3$ ,  $Y_2BaCuO_5$  or  $Al_2O_3$ . In these cases, the growth of YBCO gives rise to  
18 a higher proportion of grain boundaries compared to the magnetic field process which takes  
19 place without any support. Figure 13c shows an optical micrograph of YBCO melt-textured  
20 on a  $Y_2O_3$  polycrystalline substrate. In the centre of the image, one can observe four different  
21 domains with a large GB misorientation of  $67^\circ$ . Here again the single domain extends over a  
22 few millimeters. The TEM image [46] of figure 13d exhibits characteristic clean interfaces  
23 between two (211) precipitates and the (123) phase.

24 Twins are the main GB's present in these materials. Figure 14a shows a polarized light  
25 micrograph of a melt-textured ceramic grown on a  $Y_2O_3$  substrate, exhibiting white bands as a  
26 result of the twinned microstructure. The light lines correspond to (110) and  $(\bar{1}10)$  twin  
27 domains. The twin width distribution appears non-uniform. In its centre, a long  $89^\circ$  tilt grain  
28 boundary corresponds to a HAGB with an angle departing by  $1^\circ$  from  $90^\circ$  because of the two  
29 variants of the orthorhombic (123) structure. Figure 14b shows a TEM micrograph of this  
30 [001] tilt grain boundary with evidence of facetting of the (100) and (110) planes. Such a GB  
31 contains areas with symmetrical  $90^\circ$  tilt GB's and asymmetrical tilt GB's. The symmetrical  
32 one is not energetically favoured, which explains oscillations between these two structures.

## 33 **6.2. Influence of the substrate on microstructure and physical properties**

34 Melt-growth under a magnetic field is directly performed on a (123) bulk ceramic. Applying  
35 a magnetic field gives the best results for  $J_c$ . In the case of melt-growth, with or without a  
36 thermal gradient, the ceramic is lying on a substrate whose reactivity determines the final  
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3 superconducting properties. Because melt-growth results from the crystallization of a liquid  
4 brought at a high temperature, any interaction of the liquid with the substrate during the  
5 formation of the (123) phase can decrease  $J_c$  or, in the worst conditions, can destroy the  
6 microstructures and properties. Thus,  $J_c$  of melt-textured ceramics will be maximum only if  
7 no secondary chemical interaction takes place with the substrate. If the chemical composition  
8 of the substrate belongs to the phase diagram ( $Y_2O_3$  or  $Y_2BaCuO_5$ ), there will be no  
9 additional phases. In the case of  $Al_2O_3$  or  $MgO$  substrates, chemical reactions lead to  
10 secondary phases and damaged microstructures. In particular, the use of  $MgO$  single crystal  
11 leads to the formation of a non-superconducting YBCO carbonate phase which can be found  
12 at the (123)-(211) interfaces as was reported by Gotor et al [53]. The carbon contained in  
13  $MgO$  substrates diffuses into the liquid and alters the fabrication process. Long time pre-  
14 annealing of  $MgO$  substrates at high temperatures can cure this effect.

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17 Two YBCO ceramics were synthesized by the melt-growth method. The first one (D), was  
18 prepared on a  $MgO$  substrate using a thermal gradient for texturing [54]. The second one (E)  
19 was grown on a sintered polycrystalline  $Y_2O_3$  substrate which reacts with part of the liquid  
20 stemming from the melt. It forms an orientated layer of the  $Y_2BaCuO_5$  (211) phase, which  
21 acts as a seed for the growth of (123) [55]. In both cases, after the high temperature cycle, a  
22 low temperature sintering was carried out to obtain the superconducting (123) phase with the  
23 good oxygen content and  $J_c$  was directly measured (see Table 2). Despite the long annealing  
24 time used for oxygenation, sample (D) exhibits a low critical temperature and a large  
25 transition width. Such a  $\Delta T_c$  indicates a low oxygen content, so as the presence of oxygen  
26 non-stoichiometry and secondary phases. Susceptibility measurements on sample (D) reveal  
27 both intragranular and intergranular magnetic behaviours denoting the presence of defects at  
28 grain boundaries and/or the formation of secondary phases in the melt-textured ceramic. TEM  
29 imaging (fig. 15) displays damaged interfaces between (211) and (123) phases due to carbon  
30 impurity diffusion proceeding from the  $MgO$  substrate [55]. The magnetic behaviour of  
31 sample (E) is the same as that of a superconducting single crystal, in which only the  
32 intragranular properties are visible, indicating that (123) GB's and (123)-(211) interfaces are  
33 clean as can be seen from figure 13d. The magnetic behaviour indicates a good shielding  
34 effect for both samples (D) and (E), although the GB current transport is null in sample (D)  
35 and high in sample (E).

### 6.3. Melt-textured process as a means of studying YBCO grain boundary bicrystals

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The use of seed melt-processing allows the fabrication of larger samples with domain lengths  
as large as 20-50mm. In a TEM study aimed at high magnetic field applications, Zhang [34]

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3 found a twist component which forms the faceted boundary segments, in addition to the  
4 well known symmetrical  $90^\circ$  tilt domain boundaries, and to the asymmetrical  $90^\circ$  tilt  
5 boundaries. These GB's are expected to improve current transport in these materials.  
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8 The melt-textured process has also been applied to the synthesis of GB bicrystals in order to  
9 study their properties for specific orientations. Among these studies, Field et al [56] extended  
10 their investigations to transport properties and magnetic resistance properties across high-  
11 angle bicrystals using melt-textured  $\text{YBa}_2\text{Cu}_3\text{O}_{6+x}$ . More recently, characterization of natural  
12 and artificial low-angle boundaries in YBCO melt-textured samples were investigated by  
13 Delamare et al [57]. Results obtained from a study of controlled bicrystal misorientation, by  
14 use dual seeding using single crystals of  $\text{Nd}_{1+x}\text{Ba}_{2-x}\text{Cu}_3\text{O}_y$ . Todt et al [58] have been reported,  
15 giving  $J_c$  values very comparable to those observed in thin film bicrystals.  
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## 25 **7. Grain boundaries in epitaxial thin films**

26 Since the synthesis of  $\text{YBa}_2\text{Cu}_3\text{O}_{7-d}$  thin films, there has been a tremendous interest in  
27 epitaxial thin films for fundamental studies of the pairing mechanism, using Josephson  
28 and tunnelling junctions [7], [59], [60] and for electronic applications. Due to the short  
29 coherence length of these materials, high quality tunnel and Josephson junctions require  
30 S/N/S or S/I/S interfaces that are very sharp on the atomic scale, and therefore a surface  
31 roughness close to the lattice parameters.  
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### 39 **7.1. Influence of processing on epitaxial growth**

40 Perfect control of the growth is necessary to guarantee a reliable correlation between physical  
41 properties and film structure, especially for a contribution to the understanding of the  
42 superconducting mechanism. In particular, it is essential to define the optimum conditions for  
43 growing a single phase (123) superconducting thin film orientated along a specific direction,  
44 without secondary phases and without any oxygen deficiency which would strongly affect the  
45 study of its intrinsic properties. YBCO film morphology and microstructure are strongly  
46 dependent on the sintering process. The optimization of the deposit and the understanding of  
47 the dependence of its orientation on temperature, are related to the growth mechanism and to  
48 the nature of the substrate [61].  
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56 The most usual growth process for HTSC films is pulsed laser deposition which corresponds  
57 to a high energy process favouring out-of-thermodynamic-equilibrium conditions. It is  
58 difficult to accurately control the microstructure in such a process. In particular, the formation  
59 of high roughness, of out-growths, which are secondary phases produced during the process,  
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3 are very critical and can change from one film to another. For example, in YBCO  
4 heterostructures grown by this process, the layer roughness increases with increasing  
5 thickness [62], [63] can reach the value of 5nm deteriorating the local properties.  
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7 Nevertheless, a lot of studies on bicrystal-based Josephson junctions, or on interface  
8 Josephson junctions, produced optimized films for the study of electronic properties [64],  
9 [65], [66], [67] studied in YBCO films the effects of cooling time on the electrical properties  
10 of grain boundary Josephson junctions with 24° and 36.8° tilt misorientations. A particular  
11 study of the effect of sintering, under various oxygen atmospheres, on the weak-link  
12 behaviour of YBCO by [68] demonstrated an improvement of the properties of the junctions.  
13 In the case of thermal evaporation, a low energy process (in the 10eV range), the growth rate  
14 can be very low ( $10^{-1}$  -  $10^{-2}$  nm/s) which allows a longer time for surface diffusion. This leads  
15 to a growth close to the thermodynamic conditions with no or only very few out-growths, and  
16 to a surface roughness as low as 0.3nm for some orientations [69].

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18 YBCO films grown by reactive co-deposition on SrTiO<sub>3</sub> substrates have been recently used to  
19 make *in-situ* planar tunnel junctions Pb/YBCO of high electronic quality and reproducible  
20 properties [70]. This process is optimized for a very low deposition rate (0.00625nm/s) on a  
21 substrate heated at 1023K. These conditions yield films of high crystalline quality. X-ray  
22 diffraction rocking curves on the intense 005 reflection and atomic force microscopy (AFM)  
23 measurements detect a low mosaicity of the film with FWHM  $\approx 0.26^\circ$  and a surface roughness  
24 as low as 3.5nm on a  $1\mu\text{m}^2$  scale. The junctions grown in these conditions exhibit good  
25 conduction properties ( $T_c=89\text{K}$ ,  $\Delta T_c=1\text{K}$  for 50nm thickness) [71]. Using the same process,  
26 the best conditions to grow YBCO on a MgO substrate are different due to 3D island growth,  
27 whereas on a SrTiO<sub>3</sub> substrate 2D growth takes place. The optimum temperature on MgO is  
28 1003K. Far from the optimum conditions, the roughness of the film increases drastically  
29 within a 10K range and out-growths form on both SrTiO<sub>3</sub> and MgO substrates [69]. It is  
30 important to point out the difficulty of preparing a pure [001] thin film without forming also  
31 another orientation, because of the closeness of the interfacial energies. In particular, [100]  
32 precipitates are often present in [001] YBCO thin films. They introduce 90° planar and  
33 vertical GB's which behave as weak-link GB's and decrease  $J_c$ .  
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37 The anisotropy of the coherence length makes it difficult to obtain high quality interface  
38 junctions with specific orientations such as [100] and [110]. As an example, the growth of a  
39 film with a single [110] orientation is extremely difficult to achieve without forming also the  
40 [103] orientation. Only the use of special X-ray experiments for controlling the different steps  
41 in the formation of (123), makes it possible to obtain a single orientation [100] or [110] [69].  
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### 7.2. Influence of YBCO growth on film microstructure

A SrTiO<sub>3</sub> single crystal (cubic structure,  $a=0.3905\text{nm}$ ) is the usual substrate for obtaining HTSC films and devices because of its dielectric constant and good matching with YBCO. When YBCO is grown on STO, [001] and [100] zone axes can be formed, depending on thermal conditions. YBCO growth on MgO leads to the formation of misorientations in the films due to 3D island growth and also due to the fact that commercial MgO is not a true single crystal as it contains numerous sub-grain boundaries. Consequently, YBCO epitaxial growth leads to strong planar misorientations around the [001] axis. Those observed from various studies are: 35°, 30.6° and 62.7° [71], [72], [73], [74]. These particular values correspond in fact to coincidence site lattices (CSL) at YBCO GB's. Marshall and Ramesh [75] studied the effect of synthesis conditions on film orientation for different substrates like STO, LaAlO<sub>3</sub>, MgO and Y-ZrO<sub>2</sub> (YSZ). They found that STO was the best concerning lattice mismatch, orientation and T<sub>c</sub>. MgO and YSZ were the poorest substrates. On MgO they observed 8°, 18°, 26° and 45° misorientations. Other studies of YBCO grown on a YSZ single crystal substrate showed also various misorientated grain boundaries in the thin film [77]. These authors found misorientations of small angle (6.5°), high angle (29°, 45°) and also 90° GB's which correspond to the (ab) plane twinning.

The morphology of YBCO thin films consists of growth islands with terraces of either spherical or square shape, faceted or not, depending on growth conditions. The resulting surface may be either flat (2D growth) or rough (3D growth). Figure 16 shows YBCO thin films grown by a co-evaporation process respectively on STO (a, b, and c) and on MgO substrates (d, e and f). Figures 16a and figure 16d show AFM images of growth islands. Figures 16b and Figure 16e show TEM planar view images of a large area with a single [001] orientation on a STO substrate, and various GB misorientations around the [001] direction on a MgO substrate. The GB rotation angles of 35°, 30.6° and 62.7° about the [001] direction are visible by the rotation angles between the twins of the two grains. Both films exhibit 90° grain boundaries corresponding to (001) plane twinning. The Moires of figures 16c and 16f correspond to the superposition of YBCO 100 and 010 reflections of the (123) phase with those of the substrates. For a MgO substrate there is only one kind of Moire, whereas for STO there are chevron-like Moire structures exhibiting various d-spacings. Those formed on MgO have a constant value, indicating full relaxation in the film. The morphology of YBCO films on STO reveals a residual strain in the vicinity of the substrate.

All YBCO thin films contain growth defects induced by the epitaxial growth, and others resulting from the YBCO structure itself. Stacking faults due to the local chemistry (double

CuO planes are often formed), antiphase grain boundaries created by the presence of steps located either near the surface of the substrate or along the island terraces, are observed. An other type of defect, always observed in  $c$ -axis films, is the formation of local  $a$ -axis nuclei or grains formed mainly at the interface with the out-growths [71]. Their growth always competes with that along the  $c$ -axis as described by Granozio et al [77]. It depends mainly on deposition temperature and rate.

The critical thickness of YBCO on STO ranges between 15 and 30nm, which corresponds to the limit of elastic deformation in a YBCO film. In this range, growth takes place by a 2D to 2D-3D growth mechanism. Above this range, the growth is 3D and the film is relaxed. Its parameters tend towards those of the bulk. 50nm thick films grown on STO are still partially relaxed, while those on MgO are completely relaxed. In the case of MgO, growth takes place by a straightforward 3D mechanism. This difference comes from the large mismatch between YBCO and MgO ( $\delta a_f/a_s = 9.26\%$  and  $\delta a_f/a_s = 7.84\%$ ), as opposed to the small mismatch for STO ( $\delta a_f/a_s = 2.17\%$  and  $\delta a_f/a_s = 0.64\%$ ). This explains the formation of a YBCO/STO coherent interface and of a YBCO/MgO semi-coherent interface relaxed by dislocations. Films on MgO present a granular behaviour of the R(T) curve [70] with a tail regime due to growth island GB's.

### ***7.3. Influence of the YBCO growth process on grain boundary structure : thin film bicrystals***

There is a feature common to all YBCO thin films epitaxially grown on bicrystal substrates STO, MgO or YSZ: the meandering of the grain boundary. Numerous studies were reported concerning YBCO thin film bicrystals grown on STO bicrystal substrates, with the aim of making bicrystal based Josephson junctions. As YBCO is epitaxially grown on STO, MgO, or YSZ GB bicrystal substrates, knowledge of the bicrystal substrate boundary structure is essential for a perfect control of the process and of the intrinsic characteristics of YBCO junctions.

TEM investigations of YBCO thin films grown on various STO bicrystals with misorientations of  $24^\circ$ ,  $36^\circ$ ,  $53^\circ$  and  $67^\circ$  were performed by various research teams. [78], [79], [80], [81], [82], [83] From these studies, it follows that the meandering behaviour observed does not depend on the misorientation of the bicrystal, but on the growth of the thin film. Even for small misorientations, thin film samples show GB meandering.

Investigations of GB meandering in YBCO bicrystal thin films grown on MgO and YSZ bicrystal substrates were reported by Miller et al [79] for various misorientations ( $10^\circ$ ,  $24^\circ$ ,

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3 36.8°, 45°, 53.2° and 67°) as a function of the growth process. These experiments point out  
4 the strong dependence of the meandering width upon the growth process. In a more detailed  
5 study [84] compared, for a 36.8° GB, the magnitude and wavelength of the meander in off-  
6 axis magnetron sputtered thin films grown respectively at a high rate of 0.4nm/mn and at a  
7 low rate of 0.16 nm/min. They found that the meandering width decreases as the growth rate  
8 decreases. In another study of the influence of low energy (co-evaporation) versus high energy  
9 processing (laser ablation) [85], [86], showed, in a near  $\Sigma 13$  GB, that meandering decreases  
10 strongly for lower growth rates. They also observed an increased faceting of the growth  
11 islands and consequently of the meandering. Alarco et al [81] studied microstructures and  
12 properties of artificial grain boundaries in epitaxial YBCO thin films grown on [001] tilt YSZ  
13 bicrystals. They observed by TEM that a 45° [001] tilt GB also presents some wavyness.  
14 They also detected the presence of [100] and [110] orientations in their film. Microstructure  
15 and Josephson phenomenology of 45° tilt and twist YBCO artificial GB's were investigated  
16 by Tafuri et al [83] who also detected GB meandering.

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28 A detailed study of a 24° misorientated [001] tilt GB grown on a STO bicrystal by laser  
29 ablation, combining TEM, high resolution electron imaging (HREM), AFM, low voltage  
30 SEM and energy dispersive X-ray spectroscopy (EDS) observations was done by Ayache et al  
31 [82]. They determined the 3D grain boundary topography from quantitative analysis of  
32 HREM Moire images of the overlapping zones, and deduced a GB growth model. In this  
33 study they characterized, on different scales, firstly the orientation of the bicrystal substrate  
34 and the surface morphology before deposition, and then the YBCO GB's after growth. Moire  
35 analysis determined, from the change in lattice parameters, a variation in the oxygen content  
36 along the grain boundary, as well as a variation by 4° of the angle of the GB misorientation.  
37 Figure 17a shows a TEM image of a YBCO 24°  $\Sigma 13$  [001] tilt GB grown on a STO substrate,  
38 exhibiting meandering of the GB plane. The electron diffraction pattern is visible in the insert.  
39 Figure 17b shows a HREM image of a portion of the overlapping zones corresponding to the  
40 superimposition of grain 1 on top of grain 2 (or vice versa) along the GB, on either side of  
41 the GB plane. One can notice the oscillation and faceting of the GB plane.

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52 The way the GB plane oscillates on either side of the GB line is determined by the underlying  
53 substrate. It also meanders all along the GB, changing from a symmetrical to an asymmetrical  
54 character, depending on its location along the GB and also on the film thickness. Such a GB  
55 oscillation induces strong local changes of the current from one place to another.

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60 From the strikingly converging results obtained by investigating YBCO growth on top of a  
bicrystal, it has become clear that, during film growth, the YBCO grain boundary deviates



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3 from the path defined by the boundary of the underlying substrate. YBCO GB meandering  
4 behaviour is related to the nucleation and growth mechanisms of the film. All studies indicate  
5 that the extent of the meandering may reach 500nm. These appear as general features which  
6 confirm the correlation between island-like growth of the film and magnitude of the GB  
7 deviation, as well as the relation between shape and GB faceting. As an example, figure 18  
8 shows AFM images of YBCO thin film GB's grown on a  $24^\circ \Sigma 13$  [001] tilt GB. Figure 18a  
9 corresponds to the AFM image of a thin film made by laser ablation and figure 18b to the  
10 AFM image of a film made by co-evaporation using a low deposition rate. They differ by the  
11 morphology of the growth-islands which present either square-shaped terraces or blurred  
12 faceting. The lower the rate, the larger are the faceted islands. Such island shapes are in  
13 accordance with what is expected from the thermodynamic conditions of the deposition.  
14 Those presenting a clear facetting correspond to the lower deposition rate, i.e. the one  
15 allowing the maximum time for atomic diffusion. The results given in the literature confirm  
16 that it is the kinetic factor which governs the growth, and not the epitaxial growth nor GB  
17 interfacial energies. At the beginning, the epitaxial growth determines the orientation. As  
18 growth proceeds, the driving force for the YBCO grain boundary structure becomes the  
19 growth mechanism. Figure 19a schematizes the shape of terraces with the holes formed via  
20 island coalescence, and figure 19b shows the model derived from a quantitative analysis of  
21 the grain boundary which exhibits clearly an oscillation of the GB plane in the thickness of  
22 the film. The extent of the meandering on either side of the GB can vary from 10nm to 500nm  
23 depending on the growth conditions. As a result, the growth mechanism alters the epitaxial  
24 relationships between the YBCO film bicrystal and STO or MgO bicrystals at the GB plane,  
25 where the growth terraces come into contact. This situation becomes conflictual and the  
26 growth fronts interpenetrate, leading to alternating domains of overlap. These results could  
27 well affect the interpretation of the experiments which have been recently carried out to test  
28 the symmetry of the superconducting order parameter, through Josephson coupling  
29 measurements on grain boundaries with special orientations [87], [88].

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50 An interesting microstructural study on YBCO bicrystal films grown on MgO substrates by  
51 liquid phase epitaxy [89], concerned large single faceted GB's. Various misoriented  $4^\circ$ ,  $8^\circ$ ,  
52  $12^\circ$ ,  $16^\circ$ ,  $24^\circ$ ,  $36^\circ$  and  $45^\circ$  [001] tilt GB's were analyzed on different scales. TEM  
53 observations showed single straight faceting over a length of 10-30 $\mu$ m. HREM studies  
54 showed that all GB's were faceted on the atomic scale, except the  $24^\circ$  and  $36^\circ$  ones, on the  
55 scale of a few nanometers. The experimental  $J_c(\Theta)$  curve overlaps that observed in classical  
56 thin films (see Figure 28) [90].  
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## 8. Grain boundary structure and properties

### 8.1. Grain boundary structure and misorientation

A study of small angle [001] tilt GB's by Tsu et al [91] showed faceting, dislocation structures and heterogeneity on various scales. More recently, TEM-EELS studies of hole concentrations near strongly and weakly coupled GB's associated with YBCO flux-grown bicrystals [33], [92] were performed on small and large angle (001) tilt pre-oriented GB's with misorientations of 7°, 12°, 28° and 31°. The key aspect in this work is that the electromagnetic properties and the coupling character of each of the bicrystals were explicitly determined. It was shown that small angle GB's are strongly coupled and that their structures consist in primary GB dislocations. A slight hole depletion was noted near the GB's. In addition, some high angle, mainly [001] tilt GB's are weakly coupled and some are resistive at  $T > 4.2\text{K}$ . In the former case, the cation structural width is apparently narrow, although GB's can be broad, exhibiting severely depleted zones. The resistive GB's contain a thin coating layer of a second phase:  $\text{Cu}_2\text{O}$ . The chemical composition at small and high angles shows a slight Cu enrichment at the GB's, in good agreement with the characteristic copper non-stoichiometry found in flux-grown YBCO ceramics [54]. GB enrichment in Cu comes from the flux-growth process. The oxygen hole deficiency zone extends over 20 to 40 nm into each crystal.

A systematic study [93] of the structure of symmetric and asymmetric tilt GB's was carried out using geometrical modelling and particularly the coincidence site lattice (CSL) configuration of the (a-b) and (a-c) types. The first one corresponds to atomic planes containing either a,b lattice parameters, or b,c lattice parameters adjoining the boundary. The YBCO layered structure allows four different types of atomic planes to meet at the interface both for a-b and a-c type boundaries. These are Cu-vacancy-Cu, Ba-O-Ba, Cu-O-Cu and Y-Y atomic planes. In this modelling, the fraction of the continuous superconducting planes and the charge associated with the boundary void configurations were determined as a function of the misorientation angle of the a-b boundaries. The geometrical modelling was extended to describe the distortions, the unbalanced charge and the continuity of the Cu-O planes in the asymmetric GB's, and disclinations as well. The critical current density obtained in terms of the depression of the order parameter, the width, and the coalesced region of the boundary were found to agree with experimental observations. Figure 20 shows the resulting models obtained for  $\Sigma 37$ ,  $\Sigma 13$ ,  $\Sigma 5$  large angle grain boundaries (20a, 20b and 20c) with their coalesced configuration. One can point out the distortion of the lattice superconducting a-b planes and the voids at the grain boundary. Another example (Fig 20d) corresponds to the (a-c) type GB, showing continuity of the lattice planes a and c, with a mixture of two types of

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3 structural units at the GB. The continuity of the Cu-O planes responsible for the  
4 superconducting current is found to depend on the atomic species occupying the common  
5 lattice positions of the two adjoining grains. It also determines the critical current density of  
6 the GB's. The distribution of the excess charge at the grain boundary is shown to be important  
7 in scattering the superconducting pairs. The necessity of neutrality also leads to cation and  
8 anion vacancies at the boundary, in turn leading to non-stoichiometry.

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10 A HREM study of current HAGB's like  $\Sigma 1$   $90^\circ$  grain boundaries by Jia and Urban [94]  
11 showed different types of atomic planes at the interface. Three models have been deduced for  
12 thin film (100)/(001) interfaces projected along the [010] direction. These models are shown  
13 in figure 21 where figure 21a is the HREM image and figure 21b shows the three models of  
14 the grain boundary. In model a, grain 1 shows a (001)  $\text{CuO}_2$  plane at the upper grain face, and  
15 grain 2 a (100) Y-Ba-O plane at the lower face. In model b, grain 1 shows a (001) Ba-O plane  
16 and grain 2 a (100) Cu-O plane; in model c, grain 1 shows a (001) CuO plane and grain 2 a  
17 (100) Ba-O-Y-O-Ba plane.

## 28 29 **8.2. Grain boundary misorientation and oxygen content**

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31 TEM-EELS (electron energy loss spectroscopy) studies by Zhu et al [95, 96] on YBCO bulk  
32 ceramics prepared via solid-solid diffusion allowed the analysis of low and high angle GB's  
33 and the measurement of the oxygen stoichiometry of GB's using the oxygen K edge pre-peak.  
34 It was found that small angle ( $\theta < 10^\circ$ ) and high angle GB's ( $\theta > 10^\circ$ ) can be either fully  
35 oxygenated or oxygen deficient. These results, obtained from 20 GB characterizations and  
36 exploited using the coincident site lattice (CSL) model, show that all high angle  $\Sigma$  GB's  
37 (from  $\Sigma 3$  to  $\Sigma 20$ ) present a departure from perfect orientation varying between  $3.24^\circ$  and  
38  $10.90^\circ$ . All high angle  $\Sigma 3$ ,  $\Sigma 9$ ,  $\Sigma 10$ ,  $\Sigma 13$  and  $\Sigma 26$  boundaries studied by Zhu [97] present an  
39 oxygen deficiency near the GB's over a width of about 80 nm on either side of each crystal.  
40 Figure 22 shows the variation of oxygen content for high angle grain boundaries close to  $\Sigma 10$ ,  
41  $\Sigma 13$  and  $\Sigma 26$ .

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43 Studies of [001] tilt GB's in YBCO thin films by HREM, Z-contrast and STEM-EELS [98],  
44 [99] showed the important role of symmetry in YBCO high angle CSL  $\Sigma 5$  and  $\Sigma 17$  GB's.  
45 The oxygen content does not change in symmetrical GB's, as shown by the presence of the  
46 oxygen K pre-edge peak, which is absent in asymmetrical GB's. Figure 23 reproduces the  
47 profiles of the oxygen K pre-edge peak used to quantify the oxygen content in GB's. Figure  
48 23a shows the pre-edge peak corresponding to the superconducting  $\text{O}_7$  phase and figure 21b  
49 shows the oxygen deficiency peak corresponding to the  $\text{O}_6$  non-superconducting phase.  
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3 Oxygen deficiency in asymmetrical GB's appears clearly in the spatial profile of the  
4 normalized oxygen pre-edge peak [99].  
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### 8.3. Grain boundaries in bulk and transport properties

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10 It is well known that the limiting factor for current transport is linked to intergranular GB's  
11 which are weakly superconducting areas. In granular superconductors, the current flows  
12 through complex paths formed by a junction network connecting the grains. Earlier reviews  
13 suggested that the limitation of  $J_c$  in YBCO materials had to do with both the lack of effective  
14 pinning of magnetic flux lines and with the presence of weak-link boundaries across which  
15 the supercurrent is limited. Later, based on studies of thin film GB's exhibiting a dependence  
16 of  $J_c$  upon misorientation, various authors claimed that not all GB's were suitable for high  $J_c$   
17 transport. Even later, some high angle boundaries were found to have a noticeable  $J_c$  transport  
18 capability [100], [101], [102].  
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21 It is difficult to obtain high  $J_c$  values with classical ceramics, because of the presence of GB's  
22 with random orientations. A large number of GB orientations are present in a classical  
23 ceramic from small ( $4^\circ$ ) to large angles ( $90^\circ$ ), as well as special coincident site lattice  $\Sigma$   
24 HAGB's. In grain-boundary studies on bulk ceramics [95], found that the coincident-site  
25 lattice model allows the characterization of a number of grain boundaries present in YBCO as  
26 near CSL sigmas :  $\Sigma 13$  ( $22.6^\circ$ ),  $\Sigma 17$  ( $28.7^\circ$ ),  $\Sigma 5$  ( $36.8^\circ$ ),  $\Sigma 29$  ( $45^\circ$ ) and:  $\Sigma 1$  ( $90^\circ$ ), as [001]  
27 tilt grain boundaries. A study of GB geometry and energy, in relation with critical currents in  
28 YBCO, analyzed numerous data from the literature and showed that random GB's are not  
29 clean and cannot transport the supercurrent, while small angle and some high coincidence  
30 GB's are clean and can transport the current [103].  
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33 A study combining TEM analysis, electrical and magnetic measurements [25] quantified the  
34 influence of sintering conditions on current density. Firstly, the variation of the current  
35 density in bulk ceramics shows a strong dependence on grain size. The smaller the grain size  
36 is, the higher is  $J_c$ . A decrease in grain size leads to an increase in the number of junctions,  
37 thus making more percolative paths available for current flow [104]. Secondly, due to the  
38 Josephson penetration depth of the current in the junction, the effective surface for current  
39 transport is weaker for large junctions than for small ones [105]. Thirdly, microcracks can be  
40 formed due to the anisotropy of YBCO grain growth. Microstructural studies displayed  
41 microcracks in grains larger than  $10\mu\text{m}$  [106], [20]. The effect of microcracks is to break  
42 possible pathways for the current, thus leading to a decay of  $J_c$ . The observed drop of  $J_c$  as  
43 the grain size increases (Figure 12) is a combination of the these three phenomena.  
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*In-situ* TEM electrical experiments were carried out for various ceramics [107]. These authors

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3 detected, on large angle near  $\Sigma$  GB's, previously characterized by  $I(V)$  measurements, a low  
4 attenuation of the supercurrent for HAGB's  $\Sigma 29$  and  $\Sigma 7$ . In particular, they measured across a  
5 single GB like  $\Sigma 7$  a drop of the grain current  $I(V)$  by a factor of 3. As shown by HREM,  
6 boundaries which do not contain (ab) planes display a small atomic disorder. These  
7 experiments are interesting, but cannot be extended to predict a current in the bulk, due to  
8 connections with adjacent GB's. Reliable electrical measurements on a single GB are only  
9 possible on perfectly pre-oriented GB's.

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12 On bulk GB bicrystals obtained via a melt-process, several workers [56], [57], [58] managed  
13 to produce a large range of misorientations from  $1^\circ$  to  $45^\circ$ , controlling the growth using a  
14 thermal gradient and controlling the planarity of the grain boundary bicrystal plane. In a series  
15 of [100] tilt grain boundaries, they found a difference in critical current density of nearly two  
16 orders of magnitude between small ( $\theta < 10^\circ$ ) and high ( $\theta > 20^\circ$ ) misorientation angles. Figure  
17 24 shows the variation of the GB current density with its two regimes [58]. This  $J_c$  GB curve  
18 shows a decrease of  $J_c$  GB as a function of the misorientation angle, similar to that seen in  
19 figure 12 as a function of grain size. The difference lies in the order of magnitude of  $J_c$ : it is  
20  $10^2$  times higher in thin film bicrystals than in bulk ceramics. This is in agreement with the  
21 larger number of grain boundaries in ceramics. Compared to thin film bicrystal GB's,  
22 displaying various misorientations of the grain boundary plane (as described below), bulk  
23 bicrystal GB's have a linear and planar GB plane with a single orientation. Such a bulk GB  
24 allows a less ambiguous interpretation of the relationship between microtexture and transport  
25 properties.

#### 26 27 28 **8.4. Grain boundary structure and current transport modelling**

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31 The limiting factor for transport properties in GBs is the intergranular critical current density.  
32 In many materials  $J_c$  is suppressed at grain boundaries by phenomena such as interface  
33 charging and electronic band structure bending. Current transport mechanisms through low-  
34 angle grain boundaries were investigated [108] by calculation of the solutions of the  
35 Ginzburg-Landau equation, which account for the observed rapid decrease of the critical  
36 current  $J_c$  as a function of the misorientation angle. They proposed a mechanism of  
37 progressive superconductivity suppression in GB's as a function of  $\theta$ , due to an excess ion  
38 charge on the GB's which shifts the chemical potential in a layer of the order of the screening  
39 length in the vicinity of the GB's. They showed that the  $J_c(\theta)$  dependence is mostly  
40 determined by the decrease of the current-carrying cross section by insulating dislocation  
41 cores and by the progressive local suppression of the superconducting order parameter near  
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3 the GB's as  $\theta$  increases. The insulating region near the dislocation cores results from a local  
4 strain-induced transition to the insulating antiferromagnetic phase.  
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7 When the misorientation increases, the separation of the dislocation cores decreases. At the  
8 point where the strain fields around dislocation cores begin to overlap, i.e. at the end of the  
9 low angle regime (for large HAGB's), models based on linear elasticity become inapplicable.  
10 At this stage, the alternative methodology to describe the grain boundary structure is by  
11 structural units as shown by Browning et al [99]. The advantage of such a model is that, once  
12 the structural unit has been determined, it is possible to predict the structure of the GB for any  
13 orientation. But such a deduction in perovskite oxide GB's is very difficult due to the  
14 inhomogeneity along the atomic GB's structure. As an example, Ayache et al [109] found  
15 new atomic structural units of a symmetric [001]  $67.4^\circ$  near- $\Sigma 13$  tilt grain boundary in  $\text{SrTiO}_3$   
16 identified by a quantitative analysis of lattice images, reconstructed electron exit waves, and  
17 Z-contrast images. They found evidence for the formation of three new structural units  
18 centered either on Sr columns or on TiO columns. This GB presents a multiplicity of  
19 structural units (i.e. various stoichiometries along the GB) which contain 4 and 5 columns in  
20 coincidence, and the same number of doublets of columns of the same nature in close  
21 proximity. These results highlight new interpretations of the formation of grain boundary  
22 structural units in perovskite oxide system.  
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35 Atomic scale modelling of the GB potential in cubic perovskite oxides was developed by  
36 Klie et al [110], based on a combination of experiments on  $8^\circ$  and  $58^\circ$  [001] tilt  $\text{SrTiO}_3$  GB's  
37 and on theoretical calculations. Distance–valence least square analysis and multiple scattering  
38 calculations were used to determine the density of the GB states. They showed, for both high  
39 and low angle tilt GB's, the validity of the Thomas-Fermi approach of screened charges  
40 associated to the classical Schottky model. Figure 25 (a and b) shows the density of states for  
41 two  $\text{SrTiO}_3$  GB's (pristine). One can see clearly the charge distribution in the dislocation  
42 cores for low (a) and high (b) angle GB's. The smallest misorientation corresponds to the  
43 largest distance between the dislocations cores avoiding the overlap of the strain field [110].  
44 In comparison, figure 25c shows the charge distribution in a  $4^\circ$  [100] tilt boundary in Ca-  
45 doped (left) and undoped (right) YBCO [111]. The core centre corresponds to a negative  
46 charge.  
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56 A numerical simulation study of the influence of temperature and interface space charge on  
57 the GB conductivity in Ni acceptor-doped  $\text{SrTiO}_3$  ceramics [112] showed that the electrical  
58 characteristics of these GB's could be deliberately modified by decorating the GB's with  
59 suitable dopants (Ni, Ag, Ca).  
60

### 8.5. Grain boundaries in thin films and transport properties

The first studies of transport properties in thin film bicrystals were performed on samples prepared by laser ablation [113]. Various STO bicrystals with misorientation angles ranging from  $0^\circ$  to  $35^\circ$  were produced by melt-processing and used as substrates for growing YBCO bicrystals films in order to study the orientation dependence of the GB critical current. The critical current density across GB's on the (ab) basal plane of YBCO bicrystals was measured at 4.2K as a function of misorientation. The ratio of grain boundary critical current density ( $J_{cGB}$ ) to average value of the critical current density in the two grains ( $J_{cG}$ ) was plotted as a function of misorientation (Fig.26). The  $J_{cGB}/J_{cG}$  ratio decreases exponentially with increasing GB misorientation.

This curve shows that, even for  $0^\circ$  GB misorientation,  $J_{cGB}/J_{cG}$  decreases by a factor of two. This means that, even for a junction free from any misorientation, coupling between the two grains is decreased. Due to the sensitivity of  $J_c$  to crystallographic orientation, the coupling is maximum along the crystallographic axis and decreases with increasing GB misorientation. Such a behaviour cannot be related to classical coupling, but rather to pinning. Results obtained from the study of the residual critical current in HTSC bicrystal GB junctions tend to support such an hypothesis [65]. They showed that the residual current increases as the misorientation decreases. In this kind of systems, the residual critical current is attributed to inhomogeneities inside the barrier. The GB model proposed considers a periodic modulation of the order parameter, associated with a periodic structural change element which is consistent with only some of the properties of GB's junctions [114], and also with the presence of a residual current. Within the framework of such a model, defects such as dislocations depress the GB order parameter. A GB can be described as an array of a large number of parallel Dayem bridges [115] separated by normal areas. Figure 27 shows such a grain boundary model schematically.

Magneto-optical studies of flux penetration and critical current density in [001] tilt YBCO thin film bicrystals were made for small misorientation angles ( $5^\circ < \theta < 7^\circ$ ) by Plyanskii et al [116]. They found a characteristic cusp in the flux distribution, which indicates that the critical current density  $J_{cGB}$  across the GB is smaller than the  $J_{cG}$  of the grain. They used Bean's model to separate the GB contribution from that of the grains. They found that small angle grain boundaries can provide additional flux pinning. This is plausibly associated with GB dislocations which accommodate the GB misorientation.

Another recent work on grain-boundary dissipation in HTSC's by Gray et al [90] re-examined the explanation of the zero field data obtained for thin films and bulk bicrystals

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3 [001] tilt GB's. Their  $J_{cGB}$  values are plotted in Figure 28 as a function of the misorientation  
4 angle. Both bulk and thin film bicrystals appear to behave in the same way. This work took  
5 advantage of microscopically more perfect bicrystals. The explanation is based on the pinning  
6 of Josephson junction vortices by the meandering found in thin film GB's. These authors also  
7 point out that there is no evidence that  $J_{cGB}$  of GB's does not drop with applied magnetic field  
8 as quickly as expected from a simple Josephson junction model. Experiments [116], [65] and  
9 modelling [117] show that the pinning of vortices is a key process involved in the  
10 superconducting behaviour of GB's, as well as in the dissipation in the bulk. The Gurevich  
11 and Cooley mechanism implies that the trapped flux can improve the critical current  $I_c$ , if it is  
12 not governed only by grain boundaries.  
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### 22 **8.6. Critical current density and doping of the grain boundaries**

23 The critical current density  $J_c$  of the supercurrent which can pass through polycrystalline  
24 materials without destroying superconductivity is remarkably small. There have been various  
25 attempts to enhance the transport properties of multicrystalline ceramics and to understand the  
26 mechanism leading to a reduction of the critical currents at GB's. Appropriate doping of the  
27 grains provides a mean of optimizing the transport properties of GB's in HTSC. This is  
28 demonstrated in the exemplary case of GB's in bicrystalline Ca- and Co-doped YBCO films  
29 [118]. By Ca doping, the critical current density is strongly increased and the normal state  
30 resistivity significantly reduced, as compared to the values obtained for equivalent junctions  
31 in undoped films.  
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34 Hammerl et al [119], investigating YBCO polycrystals, found that the partial replacement of  
35 yttrium by doping  $YBa_2Cu_3O_{7-d}$  with calcium increased grain boundary  $J_c$  values  
36 substantially, but only at temperatures lower than 77K. The resulting doped grain boundary  
37 suggests a viable approach for producing cost-effective superconducting power cables  
38 operating at liquid nitrogen temperature. Recently, Klie et al [111] reported image simulations  
39 and spectroscopy at the atomic scale, that demonstrate that in poly-crystalline YBCO, highly  
40 strained grain boundary regions contain excess O vacancies, which reduce the local hole  
41 concentration. Calculation of Ca and O vacancy formation energies were performed using  
42 density-functional theory in the local density approximation. They deduce for bulk YBCO  
43 that Ca impurities indeed substitute for Y, but in GB regions under compression and tension  
44 they also replace Ba and Cu, relieving strain and suppressing O-vacancy formation. They also  
45 used atomic resolution Z-contrast imaging in the STEM to show the arrangement of the cation  
46 columns at the grain boundary, in correlation with EELS to probe the concentration of Ca and  
47 the local concentration of holes. As an example, figure 29 shows atomic resolution Z-contrast  
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3 images of an undoped pristine ( $\text{SrTiO}_3$ )  $4^\circ$  [001] tilt grain boundary and of a Ca-doped  $4^\circ$   
4 [001] tilt YBCO GB [111]. Figure 29a shows dislocation cores in the typical pentagonal  
5 arrangement of the GB structural unit. This latter corresponds to one type of structural units  
6 found in  $\text{SrTiO}_3$  and described by Duscher et al [120]. Figure 29b shows the Y/Ba column  
7 pentagonal arrangement in the Ca-doped GB, which encloses three columns, two on the Cu-O  
8 and one on the Y/Ba sublattice. Figures 29c and 29d show the scheme of the core structure  
9 where EELS probe analysis was performed. Their profiles through positions 1-5 show a high  
10 Ca content and less O-deficiency in the doped dislocation cores.

11  
12 Another study on the modification of transport properties in low angle GB's via calcium  
13 doping of YBCO textured thin films [121], showed an increase of the critical density  
14 [ $J_{cGB}(\theta)$ ] by up to 40% and 100% for respectively the  $4^\circ$  and  $8^\circ$  GB's. Considering the  
15 Gurevich and Pashitskii model [108] for current transport at low angles, the improvement can  
16 be attributed to a reduction of the strain field and the localized charges, leading to a reduced  
17 built-in potential in the dislocation cores.

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19 For  $5^\circ$  [001] tilt GB's, Ca addition is clearly beneficial, particularly when the sample is  
20 oxygen-treated to further overdope the sample after growth, as demonstrated by Daniels et al  
21 [122]. They showed that Ca-doping decreases excess GB resistance and diminishes the gap  
22 between inter- and intra-grain density over a wide field and temperature range. Another study  
23 investigated transport properties on low angle YBCO GB's of undoped and doped thin film  
24 bicrystals [123] of  $4^\circ$ ,  $8^\circ$ ,  $12^\circ$ ,  $16^\circ$  misorientation angles. They reported that Ca-doped  
25 YBCO bicrystal films, with 10% Ca substitution, showed no significant  $J_c$  enhancement at  
26  $77\text{K}$  in zero field, but a strong decrease of  $J_c$  at higher magnetic fields due to a reduced  
27 irreversibility field at  $77\text{K}$ . Ag-doped YBCO films showed increased critical current densities  
28 at higher fields and a slightly shifted transition from strong to weak behaviour with respect to  
29 undoped YBCO bicrystal films.

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31 Recently, direct evidence for negative grain boundary potential in Ca-doped and undoped  
32  $\text{YBa}_2\text{Cu}_3\text{O}_{7-d}$  was obtained using electron holography in a transmission electron microscope  
33 [124]. They found a reduction of negative charge at grain boundary dislocations in Ca-doped  
34 YBCO, as compared to undoped YBCO, and particularly a significant decrease of the size of  
35 the perturbed region in the Ca-doped samples (see Figure 25). This appears to be the principal  
36 mechanism for the improved interfacial superconductivity.

37  
38 Very recently, statistical thermodynamics and kinetics were applied to study the origin and  
39 evolution of space charge and band-bending effects at low angle [001] tilt GB's and the  
40 effects of Ca doping upon them [125]. Atomistic simulations, using shell models of  
41 interatomic forces, were used to calculate the energetics of various relevant point defects.

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3 They found that segregation of calcium is strongly determined by the strain field, and that the  
4 nature of the space charge is closely related to the oxygen content. Doping calcium at small  
5 angle YBCO tilt GB's leads to an increase of  $J_c$  through an increase of the hole content,  
6 which enhances negative potential regions due to the segregation of calcium, and helps to  
7 passivate disorder at the boundary.  
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### 12 13 **8.7. Grain boundaries: from the bulk to thin films**

14 Table 3 summarizes the various types of ceramics investigated in the field of YBCO  
15 superconducting grain boundaries. It indicates also the GB quality, i.e. either clean or  
16 degraded (oxygen deficiency or cationic stoichiometry change) for small and high angle  
17 GB's.  
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22 Figure 28 reproduces the results taken from the literature, concerning the variation of  $J_c$  as a  
23 function of the misorientation angle in YBCO [001] tilt bulk [58], [126] and thin film [127],  
24 [128], [129] grain boundary bicrystals. The black symbols correspond to  $J_{cGB}$  in thin films  
25 and the white ones to bulk bicrystals. Grain boundaries, both in bulk and in thin films, have  
26 been improved with high quality materials allowing reliable measurement of the physical  
27 properties. Comparison of GB's  $J_{cGB}$  in the bulk and in thin films indicates clearly a similar  
28 behaviour as a function of misorientation. The  $J_c$  values in films are larger by a factor of  $10^2$   
29 than those for a perfectly defined bulk GB's, even though they have, on the atomic scale, a  
30 perfect GB plane linearity. The reason for such a behaviour lies in the pinning of the vortices  
31 along the GB plane [90]. In thin films, it is the growth island configuration which induces the  
32 high current density. This latter has its origin in the high pinning energy due to the film  
33 microstructure, i.e. dislocations at the interfaces between growth islands (Figure 17). These  
34 defects have a suitable size, of the order of the coherence length, so as a suitable orientation  
35 for pinning vortices. Comparing an equal GB misorientation in a bulk bicrystal and in a thin  
36 film bicrystal, the additional  $J_c$  observed is only due to the film growth. Finally,  $J_{cGB}$   
37 determined by the misorientation itself is the same for bulk and thin films. On this basis  
38 Mannhart et al [130] devised their experiment for the creation of magnetic flux by single  
39 grain boundaries in YBCO.  
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54 In thin films, the critical current path across a grain boundary varies with the local  
55 misorientation. It can be represented by a diagram (fig. 30) which shows the combination of  
56 symmetrical and asymmetrical faceting on either side of the GB plane. With reference to  
57 calculations based on the influence of  $d_{x^2-y^2}$  symmetry in device applications of HTSC grain  
58 boundary junctions, Mannhart et al [130] modelled the GB current density as a function of the  
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3 misorientation, taking into account the GB geometry. In their model the GB plane is vertical,  
4 which is unrealistic from the point of view of previously quoted experimental studies.  $J_c$  is  
5 calculated considering various GB geometries: symmetrical GB, asymmetrical GB, and  
6 another model taking into account the OP  $d_{x^2-y^2}$  symmetry and the vertical faceting of the GB  
7 plane. These GB models are represented in figure 31a and the results of the calculation in  
8 Figure 31b, which includes also the experimental data from Dimos et al [113]. None of these  
9 calculations reproduces the experimental data in thin films. Based on the knowledge of the  
10 GB plane structure, and taking into account the pinning contribution for small angle GB's,  
11 new calculations should be done to fit the experimental results obtained on well-defined grain  
12 boundaries. An extensive review of the nature of GB's in HTSC's can be found in Babcock  
13 and Vargas [131].  
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24 The results of TEM-EELS studies of hole concentrations near strongly and weakly coupled  
25 grain boundaries in electromagnetically characterized YBCO bicrystals show that the  
26 electronic structure of the boundary region differs from that of the bulk [92]. It is substantially  
27 wider than both the YBCO coherence length and the structural and compositional width of the  
28 GB, as suggested by HRTEM imaging and cation non-stoichiometry studies. These results  
29 also suggest a continuous transition from a strongly to a weakly coupled GB character. The  
30 very recent results on the modification of transport properties in low angle GB's via calcium  
31 doping [121] show the role of impurities on the electronic structure and particularly the space  
32 charge effect. The improvement of  $J_c$  can be attributed to a reduction of the strain field and  
33 the localized charges at the GBs. Nevertheless, calculation and experiments performed by  
34 Klie et al. [111] on Ca doped YBCO demonstrate that ionic radii are more important than  
35 their electronic valences for enhancing  $J_c$ .  
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## 47 9. Conclusion

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49 All the data reviewed give evidence that grain boundaries in YBCO materials cannot be  
50 understood without having available specific information about their local composition,  
51 structure, ionic and electronic state. They confirm that studies of bicrystals are crucial for  
52 HTSC development. As a general rule, the observations are consistent with the predominance  
53 of current fluxes in the (001) superconducting planes of HTSC materials. Consequently, some  
54 high angle GB's can transmit a reasonably high supercurrent, provided they correspond to a  
55 coincidence relationship between adjacent crystals and also provided their configuration is  
56 compatible with an easy propagation of Cooper pair electrons in the  $\text{CuO}_2$  (ab) planes.  
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For small angle GB misorientations ( $\theta < 10^\circ$ ), the pinning contribution has to be taken into account in the models, in addition to the  $d_{x^2-y^2}$  symmetry of the order parameter. These implications are contained in the weak-link behaviour for large angle grain boundaries. Experiments and modelling also show that the pinning of vortices is a basic mechanism which governs the superconducting behaviour of GB's, so as the dissipation in the bulk. Accordingly,  $J_{c(GB)}$  is determined by the misorientation itself, thus being the same for the bulk and for thin films. The current density difference  $(J_{cGB})_{\text{film}} - (J_{cGB})_{\text{bulk}}$  is only due to the growth of the film and to the induced structure of the GB plane.

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## Figure Captions

**Figure 1:** The various types of superconducting ceramics synthesized during the past decade with their respective  $J_c$  values: classical bulk ceramics, melt-textured bulk ceramics, bulk bicrystals, thin film bicrystals, thin films and single crystals. Note that the three bottom configurations are governed by controlled orientations.

**Figure 2:** Representation of a S/I/S junction with its characteristics for the Low  $T_c$  and High  $T_c$  superconductivity mechanisms.

**Figure 3:** (a) Structural unit-cell of the (123) phase showing  $\text{CuO}_2$  planes and Cu-O chains. (b) Based on the  $d_{x^2-y^2}$  symmetry of the superconducting order parameter, a schematic diagram of the strong coupling along [100] and [103] orientations, as opposed to the weak coupling along [001] and [110].

**Figure 4:** (a) Tetragonal and orthorhombic unit-cells of the (123) phase. (b) Evolution of the lattice parameter as a function of the oxygen deficiency  $d$  for various oxygen partial pressures. Note the change in the transition for temperatures between 798K and 943K [6].

**Figure 5:** Ternary phase diagram of the  $\text{BaO}-\text{Y}_2\text{O}_3-\text{CuO}$  system showing the various possible secondary phases (132), (211).

**Figure 6:** Structural phase diagram of the (123) phases displaying the effect of oxygen partial pressure and of temperature on the formation of the (123) oxygen stoichiometric phase [6].

**Figure 7:** (7a) Oxygen diffusion depth profiling on a ceramic polished with a small angle ( $\theta = 1.56^\circ$ ,  $T = 823\text{K}$ ,  $p\text{O}_2 = 22\text{kPa}$ ) exhibiting the presence of microcracks.

(7b) Ionic image obtained with  $\text{O}^{18}$  showing the anisotropy of oxygen diffusion.

(7c) Arrhenius plots of volume and grain boundary diffusion in ceramics along (ab) planes and parallel to the  $c$  axis in a single crystal. Full triangles up and down represent respectively the coefficient of volume diffusion in the  $c$  direction and in (ab) planes [21]. Diamonds represent the diffusion coefficient in polycrystals [23]. Squares and stars represent respectively volume diffusion and grain boundary diffusion [20]. Crosses represent the chemical diffusion coefficient taken from [22].

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5 **Figure 8** : R(T) measurements on  $A_0$ ,  $A_1$ ,  $B_0$  and  $B_1$  samples sintered under various  
6 conditions. The transition width becomes larger as  $T_c$  decreases, revealing a low oxygen  
7 content, a low homogeneity in the ceramic and the presence of secondary phases at grain  
8 boundaries.  
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13 **Figure 9** : (a) TEM image of ceramic  $A_1$  showing a grain surrounded by several clean GB's .  
14 (b) : HREM lattice image of a small angle ( $4^\circ$ ) GB exhibiting (001) planes. (c) :TEM image  
15 of a clean triple junction showing twinning inside the grains. (d) HREM lattice image of some  
16 faceted GB exhibiting (001) planes in one grain.  
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22 **Figure 10** : TEM and HREM lattice images of ceramic  $B_0$  exhibiting the change of a high  
23 angle grain boundary (a) from a symmetrical faceted GB (b) to an asymmetrical one (c)  
24 near an intergranular defect. Both GB's have a misorientation close to CSL  $\Sigma 13$  ( $67^\circ$ - $69^\circ$ ).  
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29 **Figure 11** : Optical micrographs (a), SEM (b), TEM image and electron diffraction patterns  
30 (c and d) for ceramic  $B_1$ , exhibiting morphologies resulting from the grain size gradient  
31 produced by the sintering. Note that twins formed in the external part of the ceramic are  
32 completely relaxed (left part of figure c) and have an oxygen content close to  $O_7$  as  
33 measured by the splitting of the 110 reflections (insert in diffraction pattern (c)). Twins of the  
34 inner part of the ceramic are of the ferroelastic type (left part of figure d). They are not  
35 completely relaxed by the phase transformation as deduced from the absence of splitting of  
36 the 110 reflections (right part of figure d) and their oxygen content is close to  $O_{6.5}$ .  
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46 **Figure 12** : Critical current density  $J_c$  measured as a function of the grain size in bulk  
47 ceramics.  $A_0$ ,  $A_1$ ,  $B_0$  and  $B_1$  samples correspond to hot-press sintering and sample (C) to a  
48 low density material made by classical sintering.  
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53 **Figure 13** (a) Polarized optical image showing two large domains with a low misorientation  
54 of about  $10^\circ$ , observed in a YBCO melt-textured ceramic synthesized under magnetic field.  
55 (b) : TEM micrograph of (a) exhibiting coherent and incoherent twins crossing a line defect.  
56 This growth defect, filled with liquid during (123) growth, keeps the same orientation, parallel  
57 to the (001) superconducting planes. (c) : Optical micrograph of a YBCO melt-textured  
58 ceramic grown on a  $Y_2O_3$  polycrystalline substrate. This image shows four different domains  
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with a large GB misorientation in its centre. Characteristic clean interfaces are formed between two (211) precipitates and (123) phases as seen in figure d.

**Figure 14 :** (a) Polarized light micrograph of a melt-textured ceramic grown on a  $Y_2O_3$  substrate exhibiting white bands in the ceramic microstructure, and a  $90^\circ$  HAGB in its centre. Light lines correspond to (110) and (-110) twin planes. A non-uniform distribution of the twin widths can be observed. (b) : TEM micrograph of the same GB showing faceting along (100) and (110) planes. There are regions with  $90^\circ$  tilt symmetrical and asymmetrical GB's.

**Figure 15 :** TEM image of a (123) phase / (211) precipitate interface damaged due to the presence of carbon impurities in the MgO substrate and due to carbon diffusion in the liquid.

**Figure 16 :** YBCO Thin films grown by co-evaporation respectively on a  $SrTiO_3$  (a, b, and c) and on a MgO substrate (d, e and f). (a and d) AFM images showing the growth islands. (b) and (e) : TEM planar view image which shows large areas of the same [001] orientation in films on STO, and various GB misorientations around the [001] direction with rotation angles of  $35^\circ$ ,  $30,6^\circ$  and  $62,7^\circ$  (visible by the twin rotation) for MgO. Both films exhibit  $90^\circ$  GB's corresponding to twinning of the (ab) superconducting planes. (e) and (f) : Moires of the 100 and 010 reflections of the (123) phase with the substrates. One can notice that those present on STO (c) show a residual strain in the (123) film appearing in chevron- shaped Moires with various d-spacings, while those formed on MgO keep a constant value, indicating full relaxation of the film.

**Figure 17 :** (a) TEM image of a YBCO  $24^\circ \Sigma 13$  [001] tilt GB grown on a STO substrate, exhibiting meandering of the GB plane. The electron diffraction pattern is visible in the insert. (b) : HREM image of part of the overlapping zones corresponding to the superposition of grain 1 on top of grain 2, or vice versa, along the YBCO GB. Note the faceting.

**Figure 18 :** AFM image of the same YBCO  $24^\circ \Sigma 13$  [001] tilt GB. (a) corresponds to a laser ablated thin film of 120nm thickness ; (b) co-evaporated thin film of 50nm thickness, grown using a low deposition rate. The morphology of the growth-islands presents either square - shaped growth terraces or not very clear faceting. Notice a 20 nm wide area with a weak contrast of the island shapes, corresponding to the region of overlapping.

**Figure 19 :** (a) schematic representation of the terrace shape and of the holes due to island coalescence. (b) : model of moires at the grain boundary based on HREM quantitative analysis. The lateral extension of GB meandering on either side of the grain boundary plane depends on the growth conditions. It may vary from 10nm to 500nm.

**Figure 20 :** Models of large angle grain boundaries (a, b and c) :  $\Sigma 37$ ,  $\Sigma 13$ ,  $\Sigma 5$  grain boundaries with coalesced configuration and exhibiting discontinuity of a-b lattice planes at the GB ; (d)  $\Sigma 5$  (a-c) type GB showing continuity of lattice planes a and c [93].

**Figure 21 :** HREM image of  $\Sigma 1$   $90^\circ$  (100)/(001) interface projected along the [010] direction; (a) ,( b), (c): the three models of the grain boundary . **Model a :** grain 1 shows a (001)  $\text{CuO}_2$  plane at the upper face, and grain 2 a (100) Y-Ba-O plane at the lower face. **Model b :** grain 1 shows a (001) Ba-O plane and grain 2 a (100) Cu-O plane. **Model c :** grain 1 shows a (001) CuO plane and grain 2 a (100) Ba-O-Y-O-Ba plane [94].

**Figure 22 :** Variation of oxygen content and lattice parameter in the vicinity of high angle grain boundaries corresponding to near  $\Sigma 10$ ,  $\Sigma 13$  and  $\Sigma 26$  GB's. They present a departure from the perfect orientation varying from  $3.24^\circ$  to  $10.90^\circ$  [97].

**Figure 23 :** (a) EELS profile of the oxygen K pre-edge peak corresponding to the superconducting  $\text{O}_7$  phase; (b): oxygen peak deficiency corresponding to the  $\text{O}_6$  non-superconducting phase. (c) : Quantitative analysis of the normalized oxygen pre-peak showing oxygen deficiency in an asymmetrical GB (stars represent symmetrical and circles asymmetrical GB's) [100].

**Figure 24 :** Variation of the current density  $J_{\text{CGB}}$  of grain boundaries as a function of the misorientation angle between  $1^\circ$  and  $45^\circ$  in YBCO melt-grown bulk bicrystals [58].

**Figure 25 :** (a and b) Density of states for these two  $\text{SrTiO}_3$  GB's (pristine). Notice the charge distribution in the dislocation cores for the low (a) and high (b) angle GB's. The smallest misorientation corresponds to the largest distance between the dislocations cores avoiding the overlap of the strain field [110]. (c) Charge distribution in a  $4^\circ$  [100] tilt boundary in Ca-doped (left) and undoped (right) YBCO [123].

**Figure 26 :** Variation of current density  $J_c$  as a function of GB misorientation in YBCO thin

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3 film bicrystals [113].  
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7 **Figure 27:** Representation of a superconducting GB as an array of a large number of parallel  
8 Dayem bridges simulating superconducting regions (B) separated by normal or non-  
9 superconducting regions (A).  
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13 **Figure 28 :** Variation of current density  $J_c$  of bulk and thin film bicrystals as a function of  
14 GB misorientation [91].  
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18 **Figure 29 :** Atomic resolution Z-contrast images of a pristine  $4^\circ$  [001] tilt grain boundary in  
19 undoped and Ca-doped YBCO. (a) dislocation core with the typical pentagonal arrangement  
20 of structural units found in  $\text{SrTiO}_3$ . (b) Ca-doped YBCO GB where the Y/Ba pentagonal  
21 column arrangement encloses three columns, two on the Cu-O and one on the Y/Ba sublattice.  
22 (c and d) diagram of the core structure where EELS analysis was performed [111].  
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29 **Figure 30 :** Representation of grain boundaries found in thin films containing a combination  
30 of symmetrically and asymmetrically faceted GB's. The critical current  $I_c$  across the grain  
31 boundary changes locally between null and a maximum value depending on the local  
32 crystallographic orientation of the GB faceting.  
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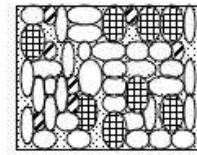
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37 **Figure 31 :** (a) Model of the various GB geometries used for calculation; (b) Results from  
38 calculations by Mannhart et al [130] compared with experimental data [113].  
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## Tables

**Table 1 :**  $\text{YBa}_2\text{Cu}_3\text{O}_{7-d}$  structures, related oxygen contents and critical temperatures. For  $0.15 < d < 0.6$  various oxygen vacancies ordering occur.

**Table 2 :** Superconducting values for melt-textured YBCO ceramics prepared with a thermal gradient on a MgO substrate single crystal (sample D) and on a polycrystalline  $\text{Y}_2\text{O}_3$  substrate (sample E).

**Table 3 :** GB's relative quality and  $J_c$  values for YBCO bulk, thin films, single and bicrystals.

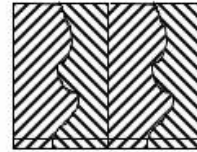


### Classical ceramics

$$J_c < 10^3 \text{ A/cm}^2$$

Polycrystals

Solid-solid  
Diffusion

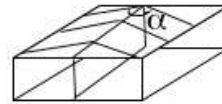


### Melt textured ceramics

$$10^4 < J_c < 10^5 \text{ A/cm}^2$$

On polycrystalline substrates:  
Y<sub>2</sub>BaCuO<sub>5</sub>, Y<sub>2</sub>O<sub>3</sub>, MgO, LaAlO<sub>3</sub>

Solid-liquid  
Diffusion

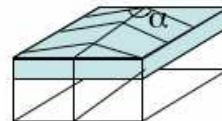


### Bulk bicrystals

$$J_c = f(\alpha)$$

From YBCO Melt ceramics

Solid-liquid  
Diffusion

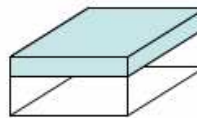


### Thin film bicrystals

$$J_c = f(\alpha)$$

Grown on bicrystal substrates:  
SrTiO<sub>3</sub>, MgO, Y-ZrO<sub>2</sub>

Solid-gas  
reaction

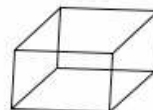


### Thin films

$$10^6 < J_c < 10^7 \text{ A/cm}^2$$

On single crystal substrates:  
SrTiO<sub>3</sub>, MgO, LaAlO<sub>3</sub>

Solid-gas  
reaction



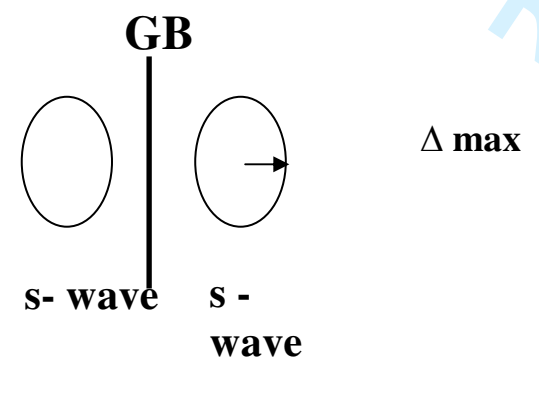
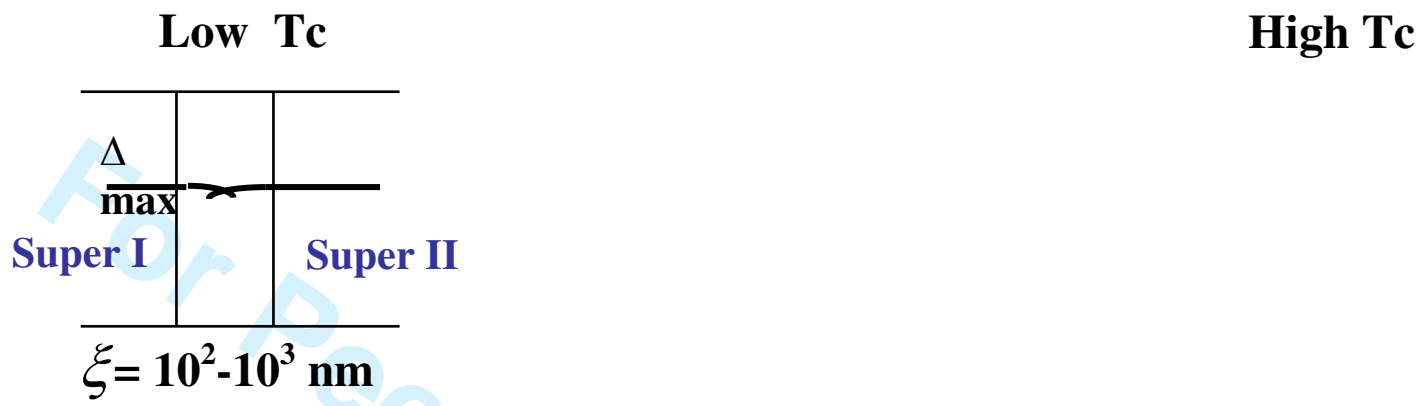
### Single crystals

$$10^4 < J_c < 10^5 \text{ A/cm}^2$$

Solid-liquid  
Diffusion  
Flux growth

Figure 1



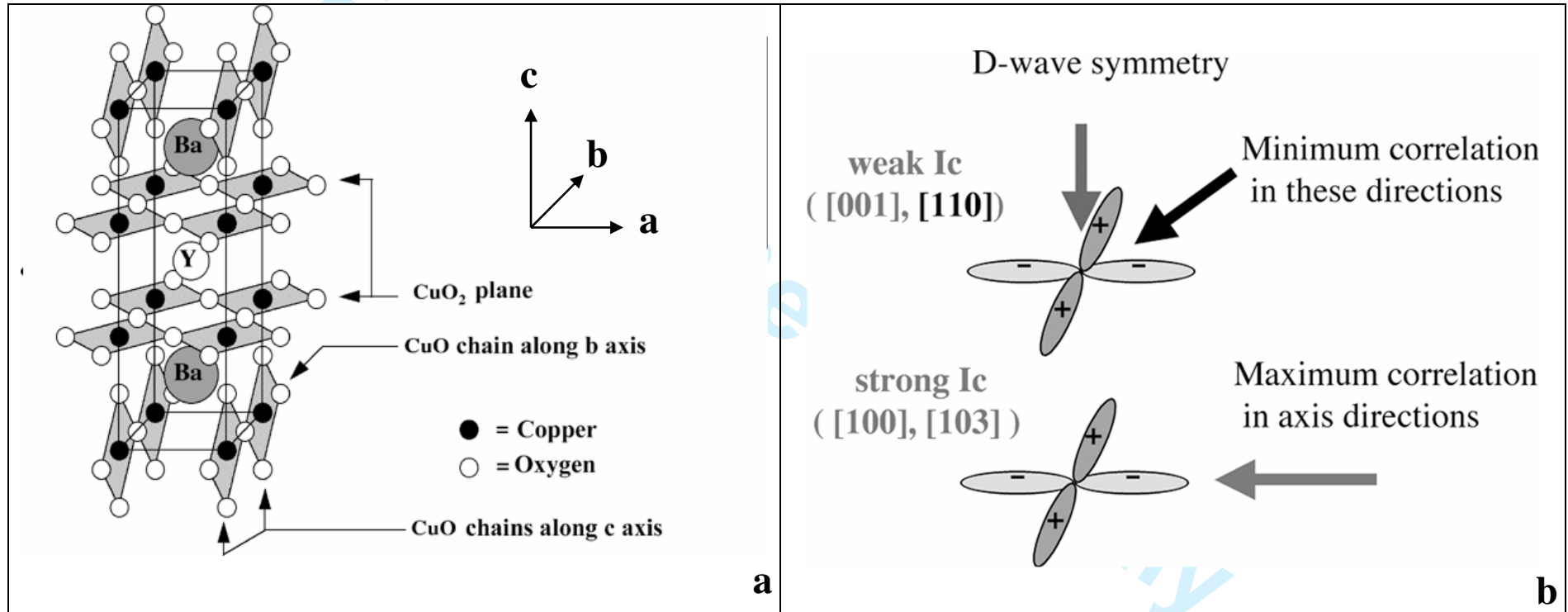


[010]

**Figure 2**

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Figure 3



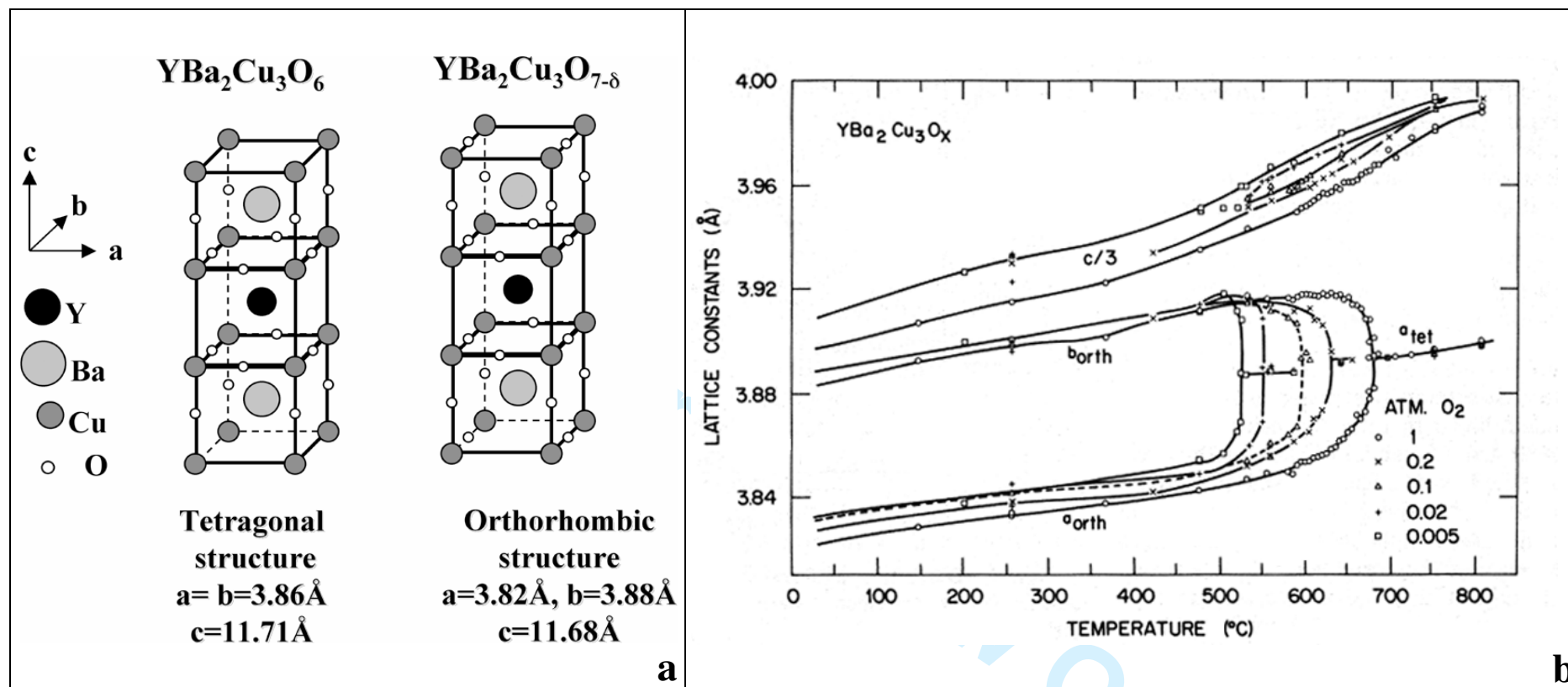


Figure 4

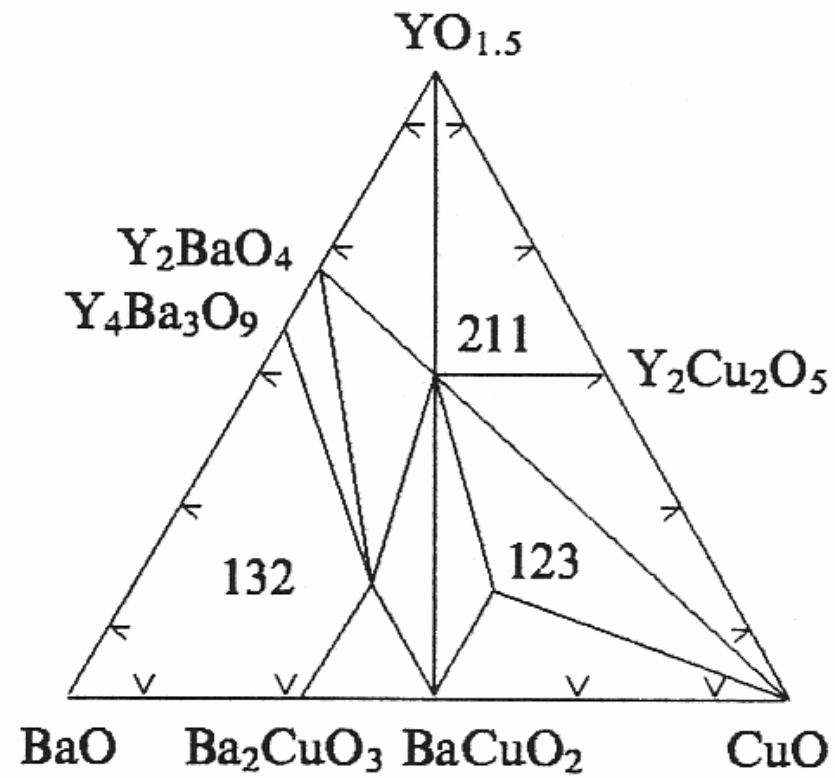


Figure 5

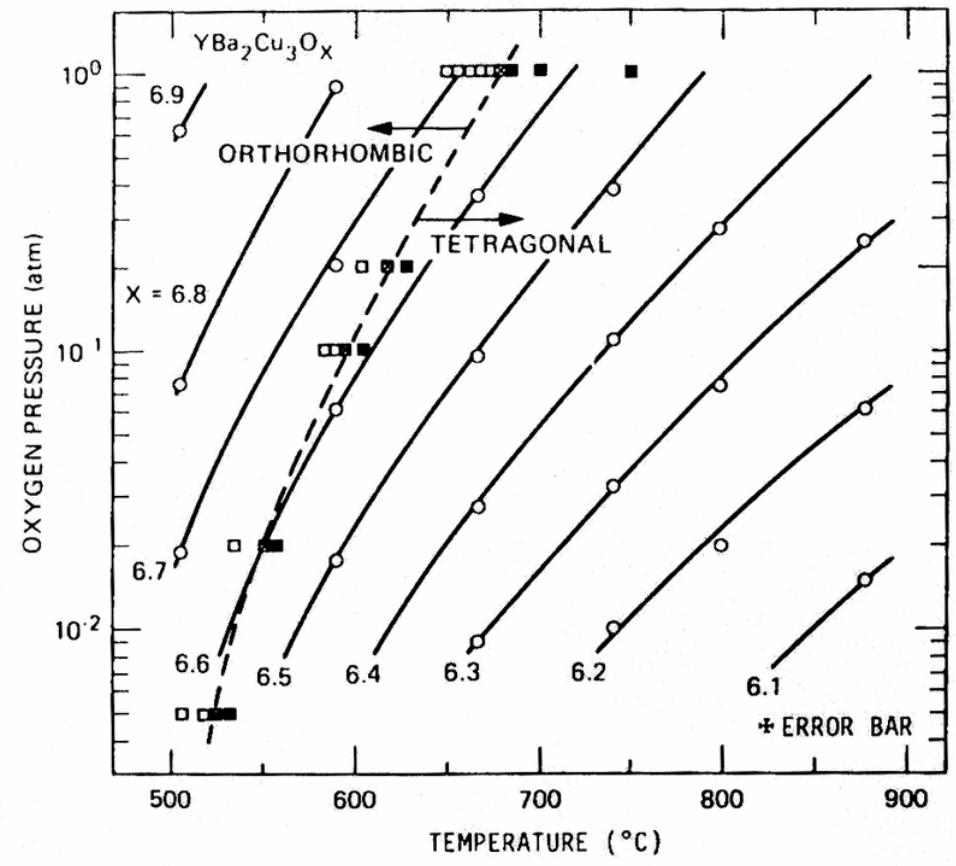


Figure 6

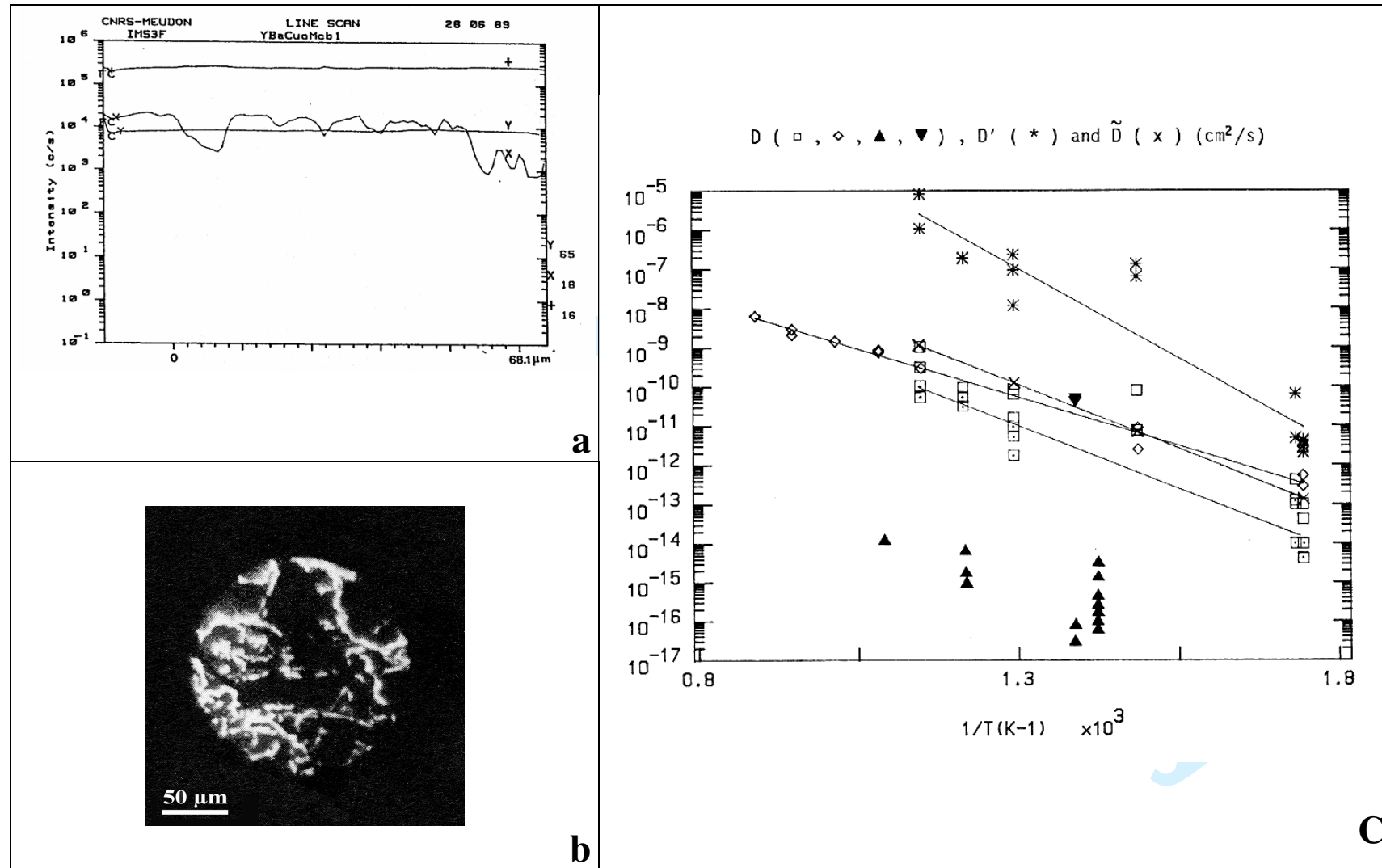


Figure 7

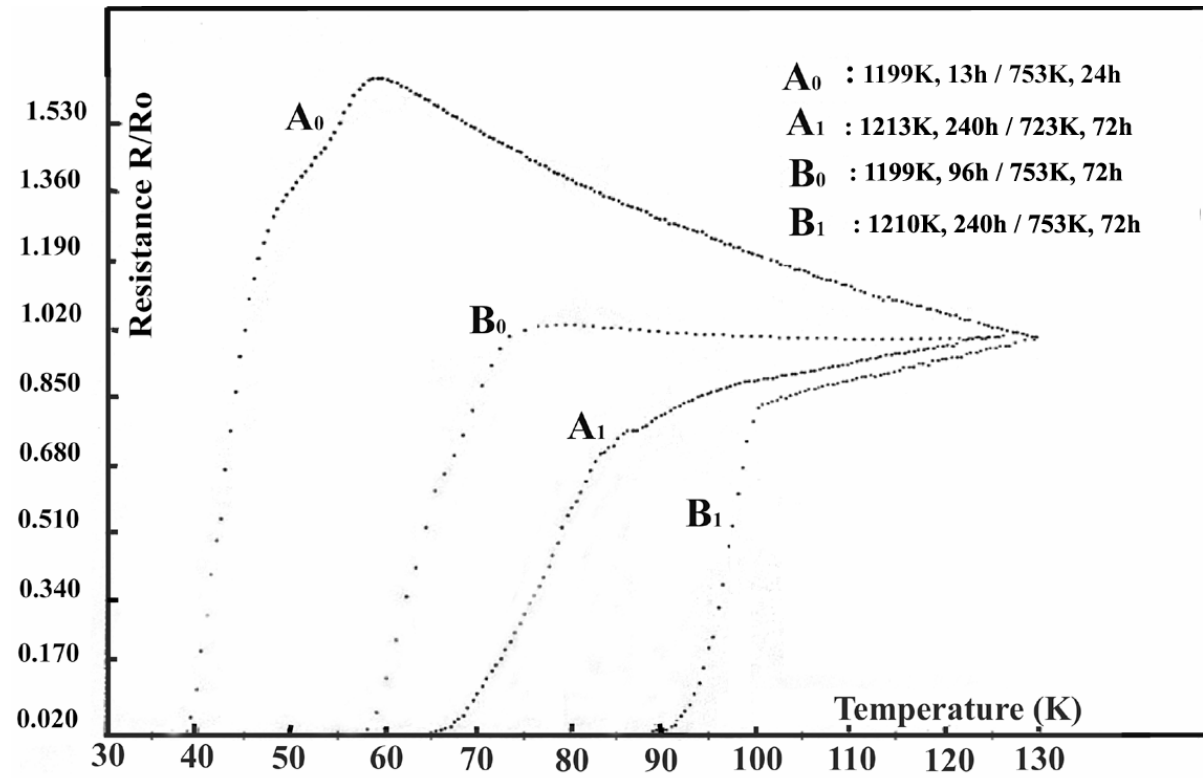
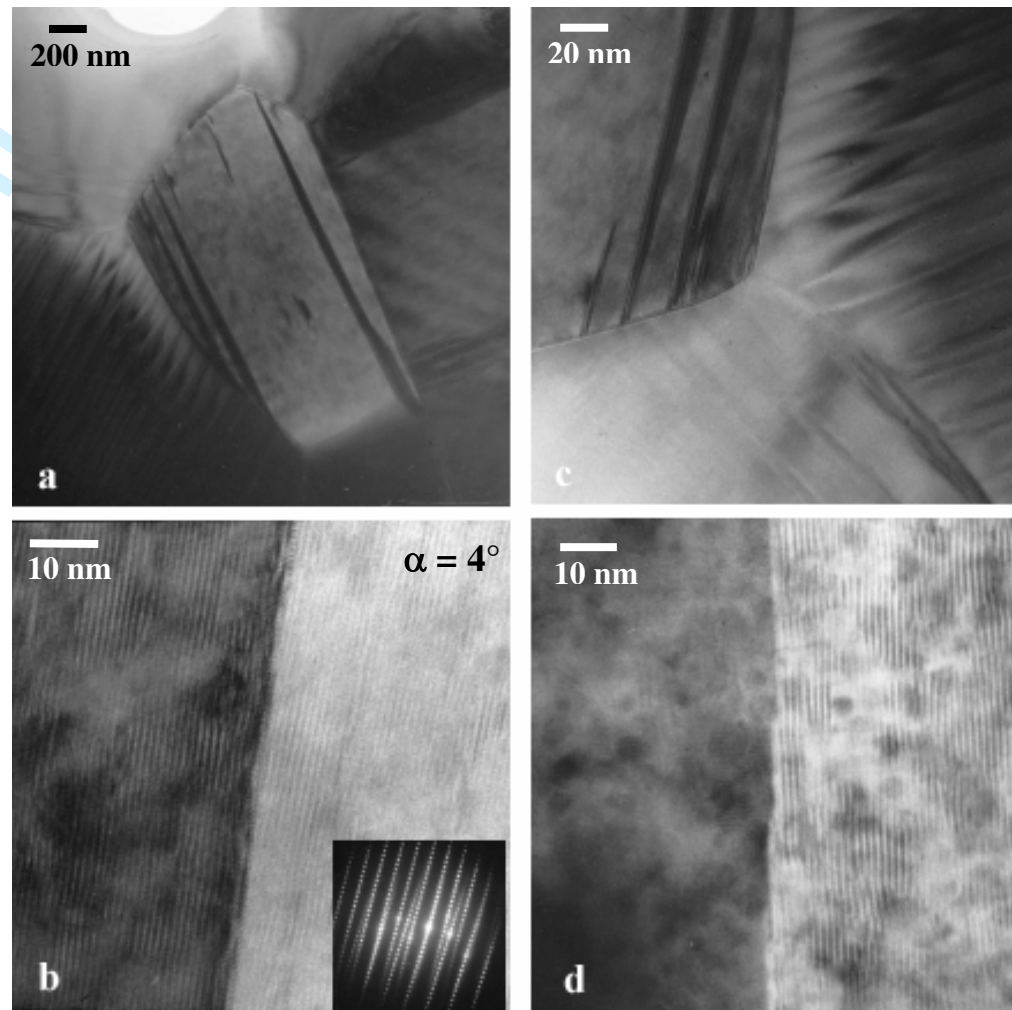


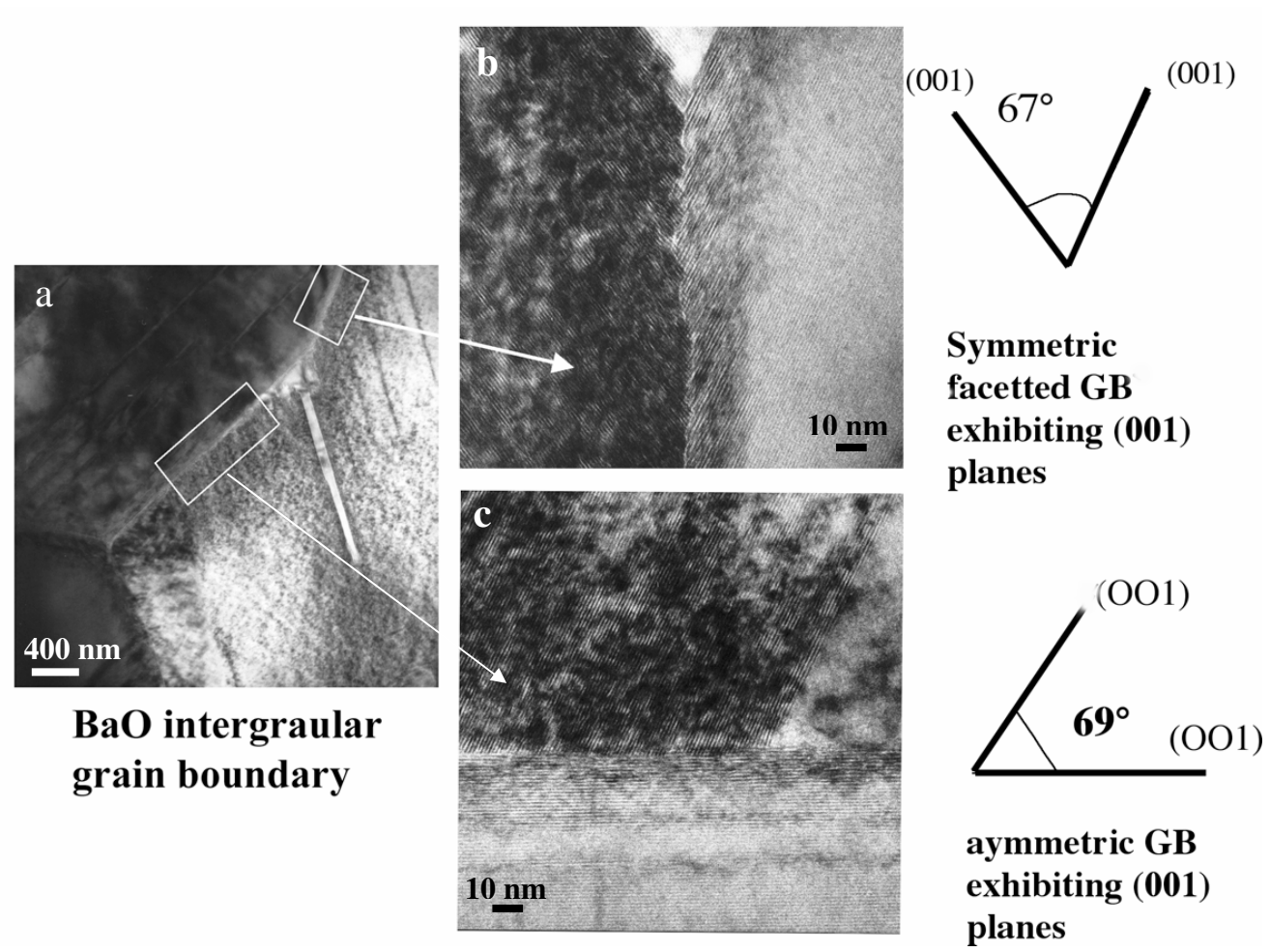
Figure 8

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**Figure 9**



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**Figure 10**

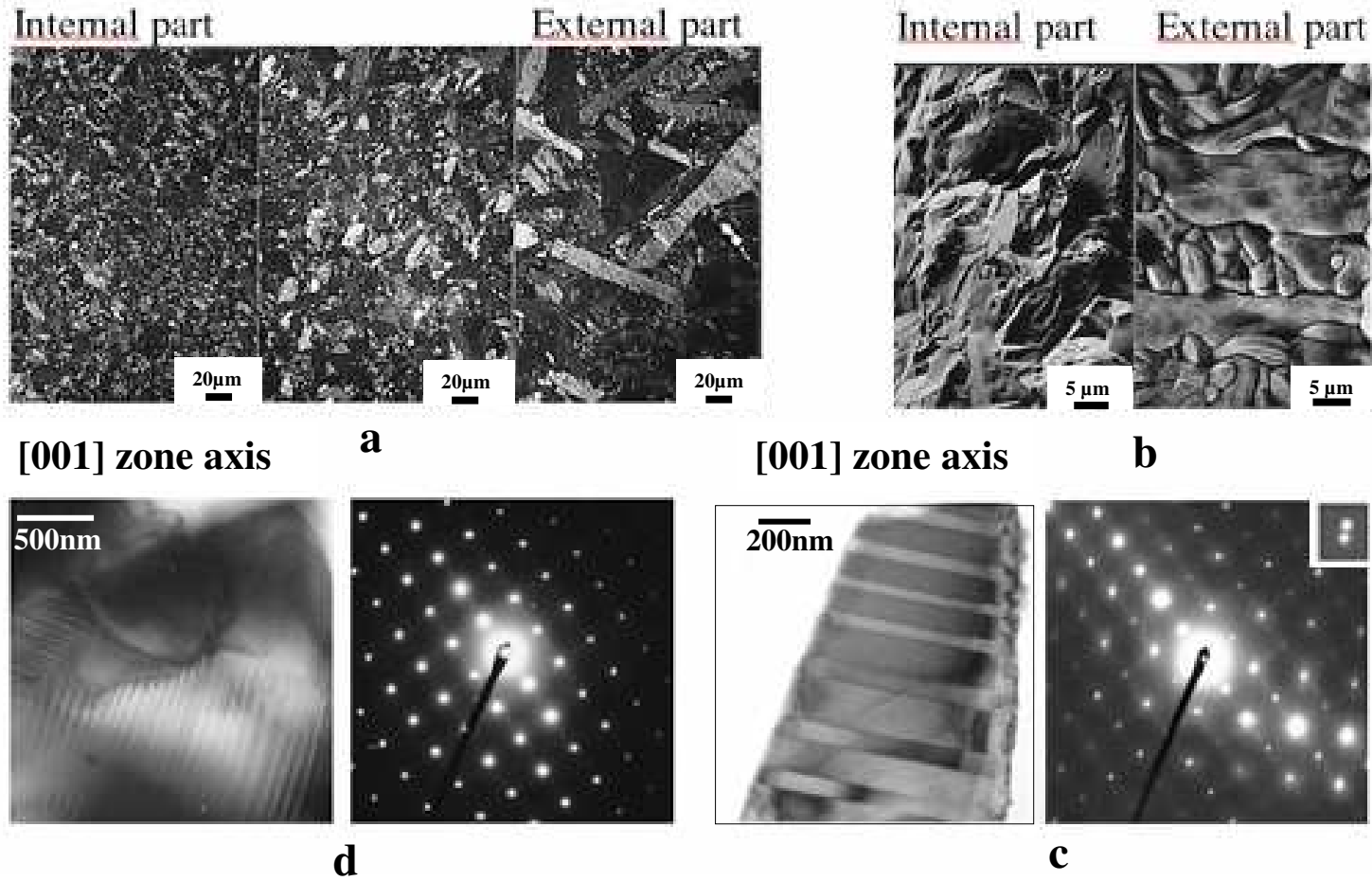


Figure 11

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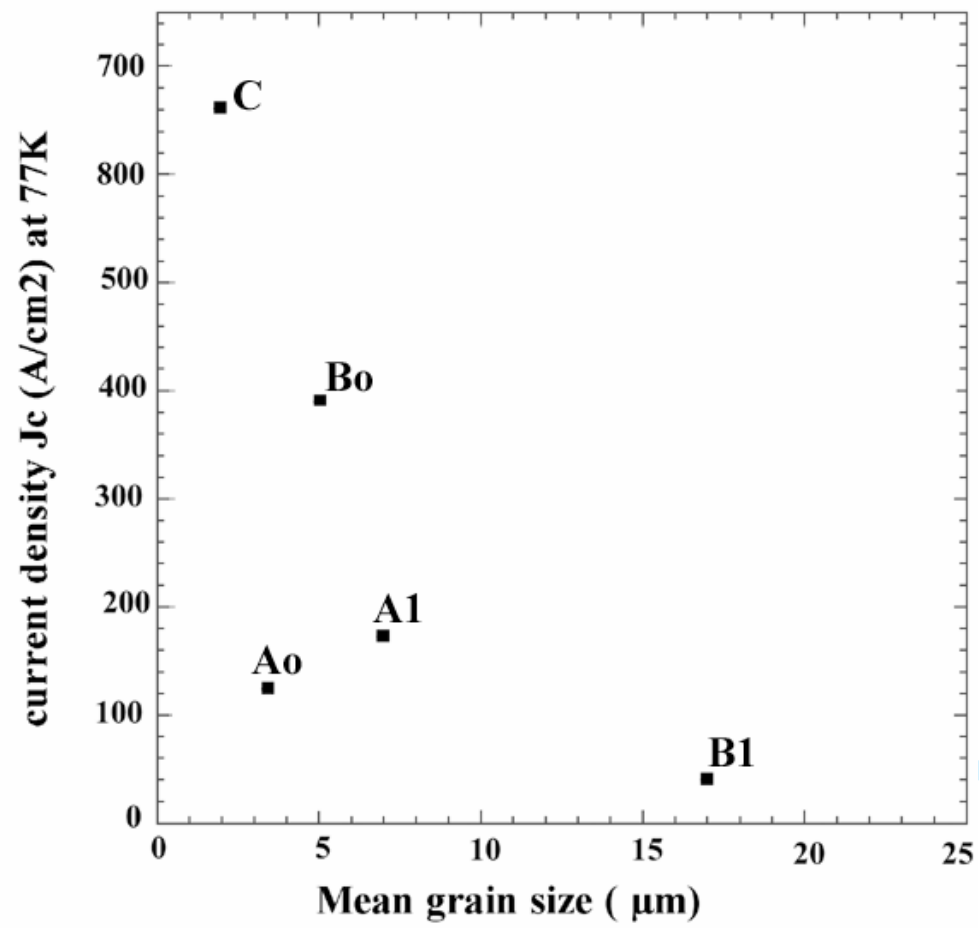
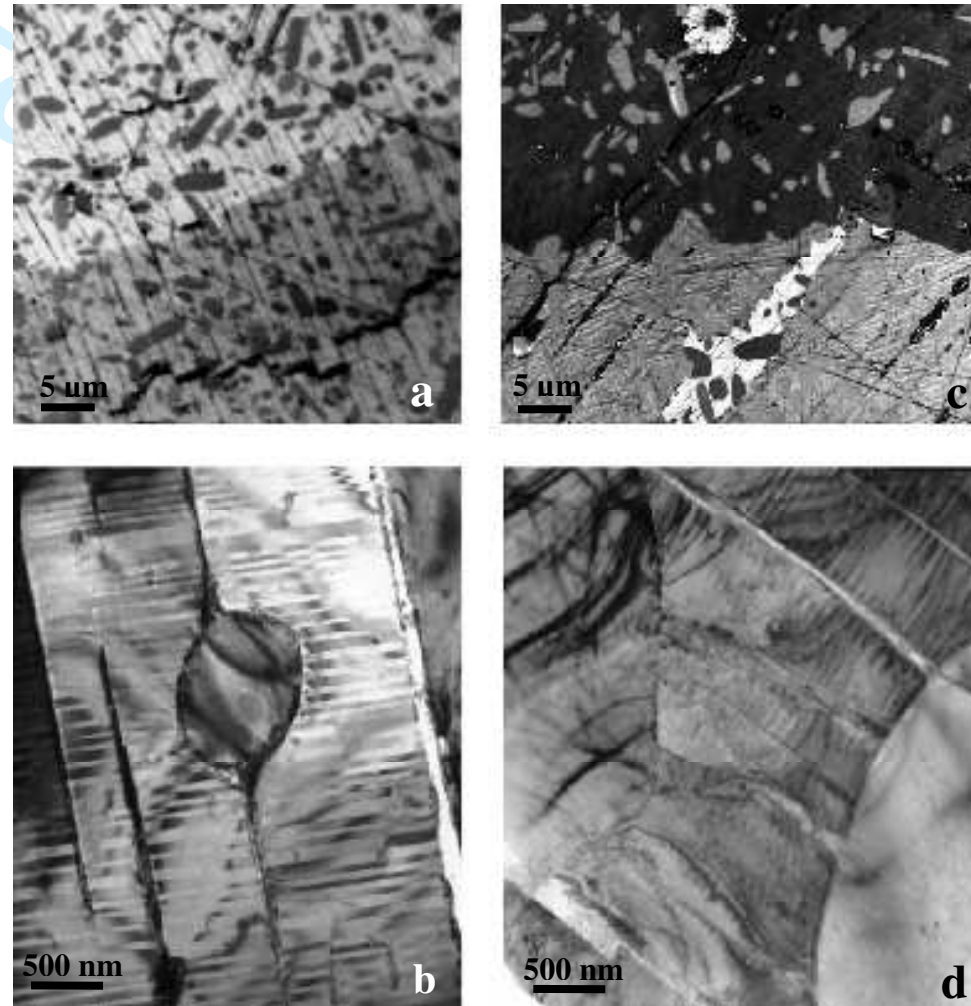
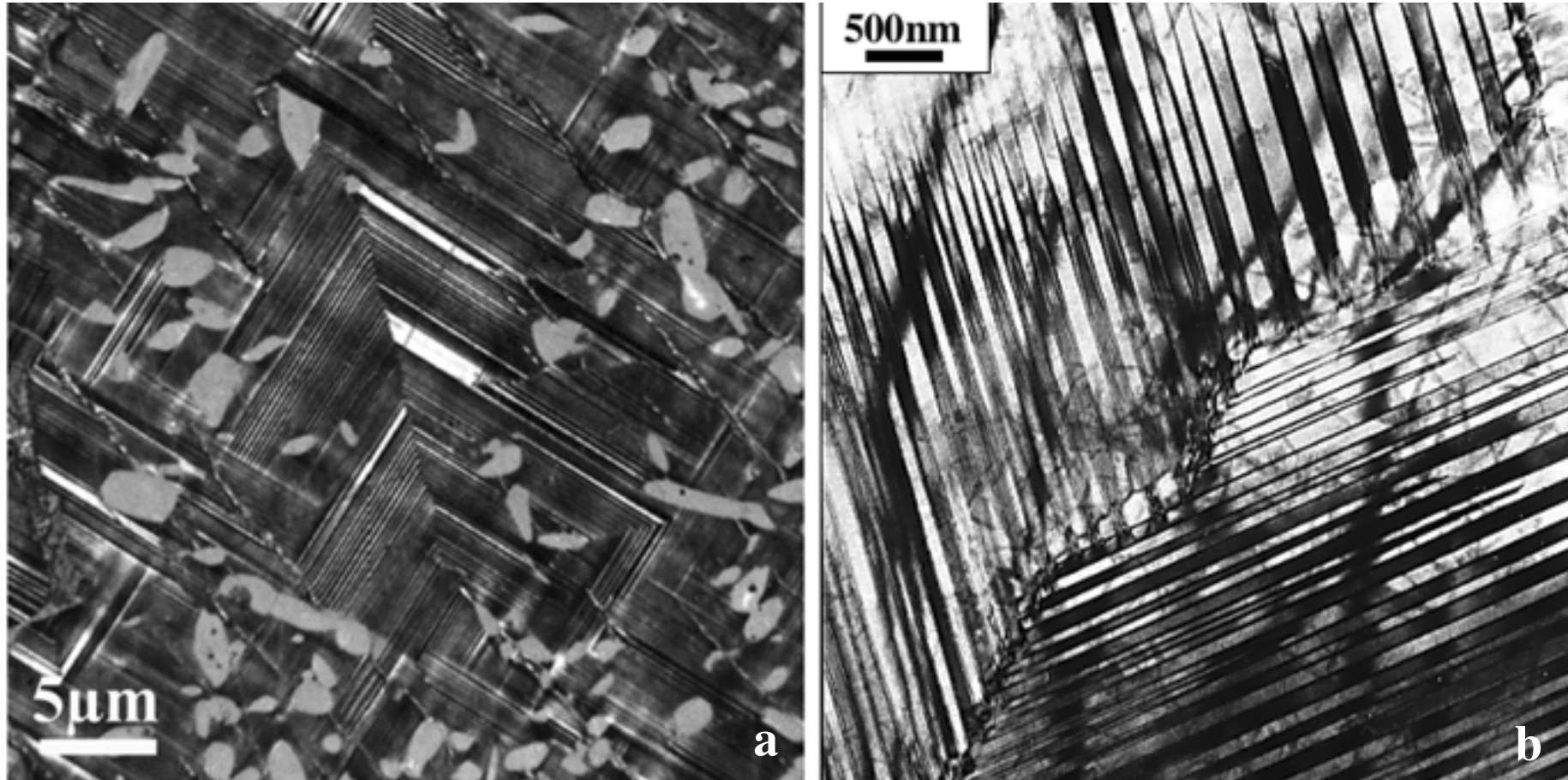


Figure 12

Figure 13



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**Figure 14**

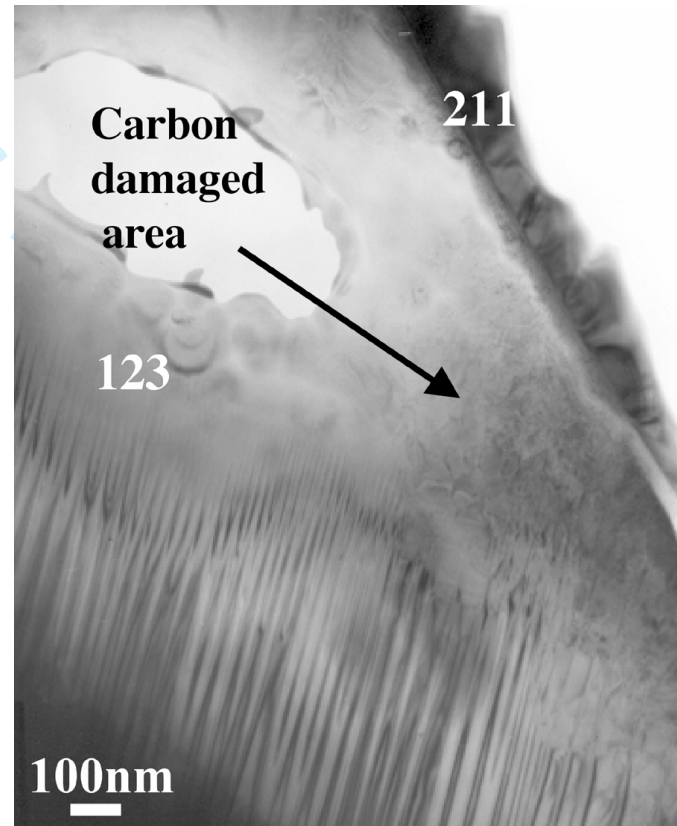


Figure 15

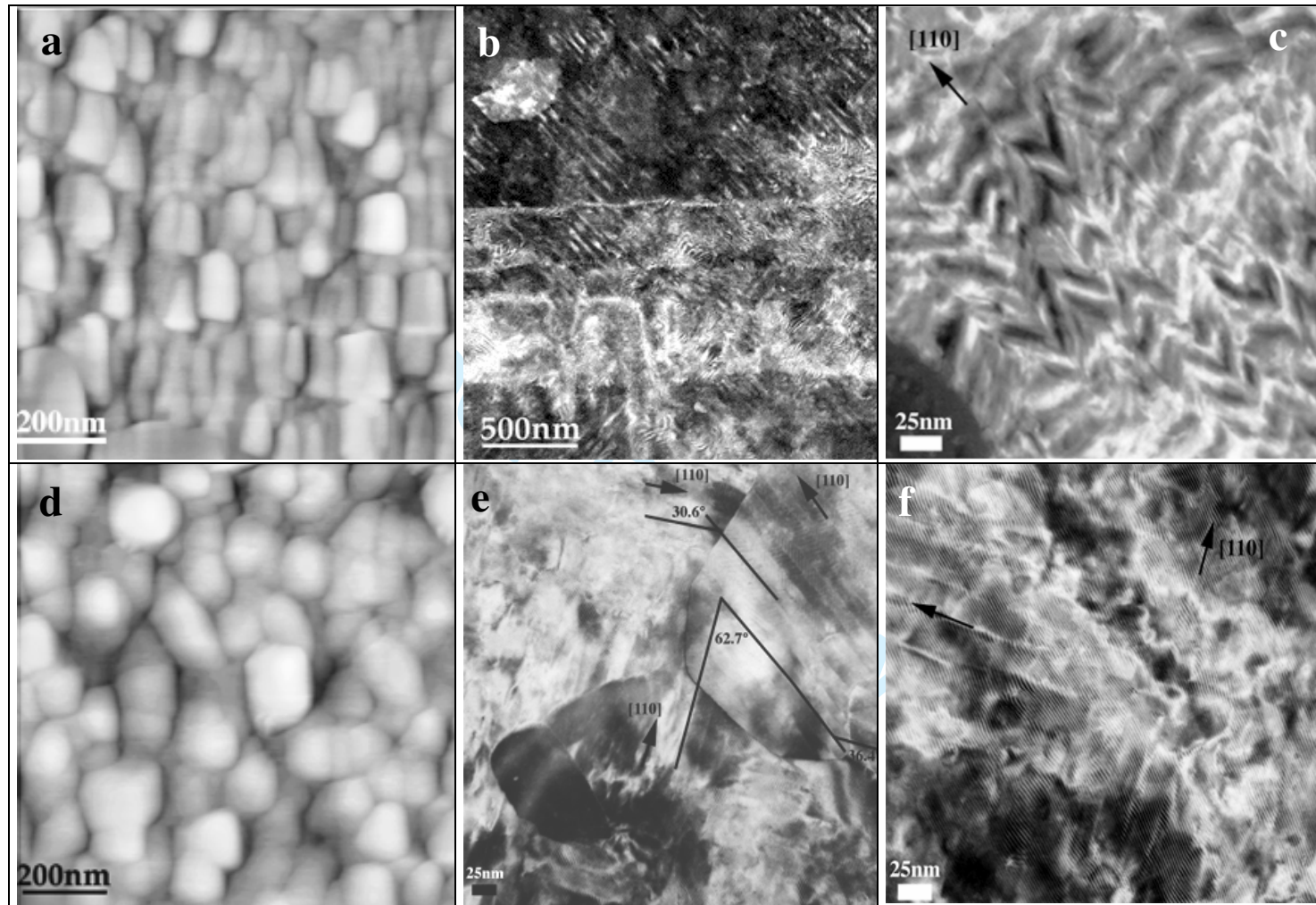


Figure 16

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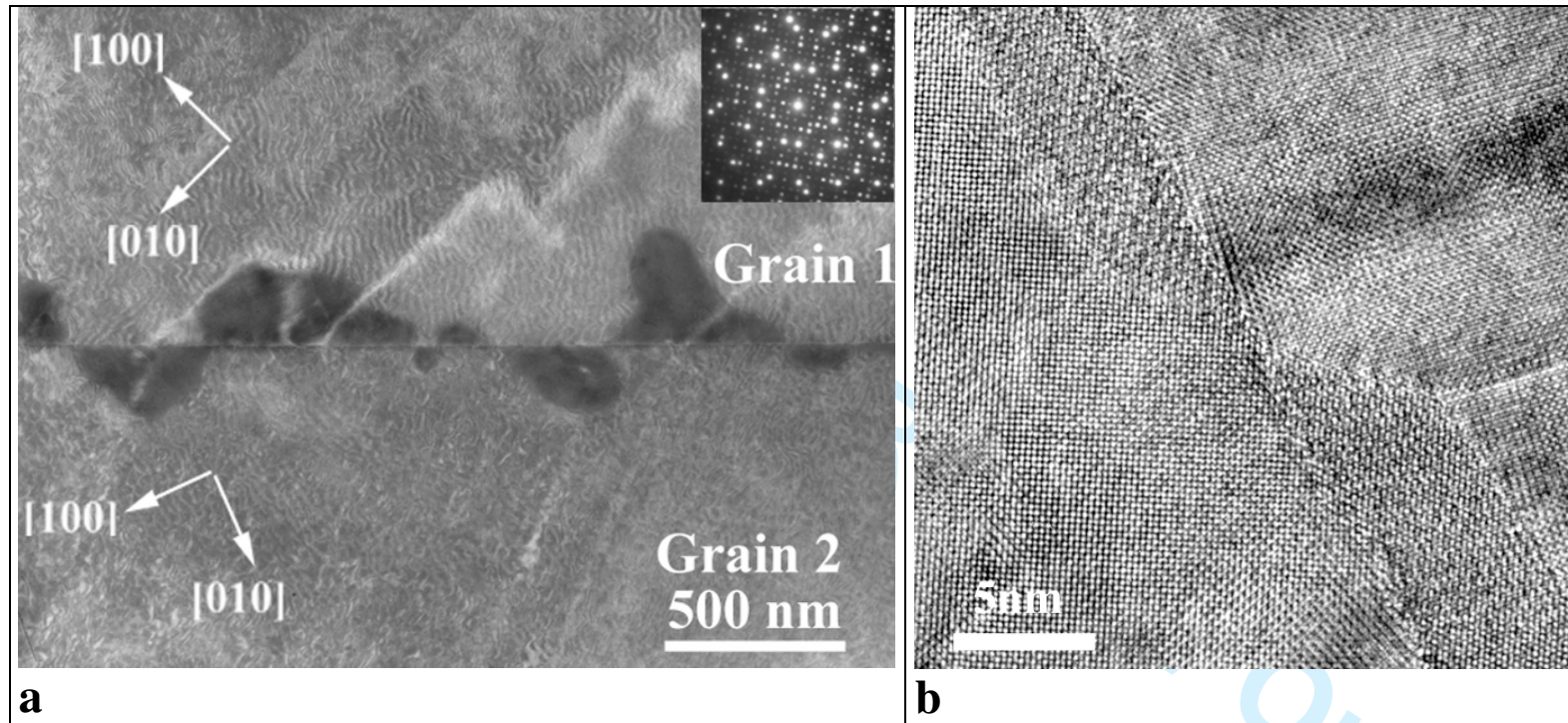


Figure 17



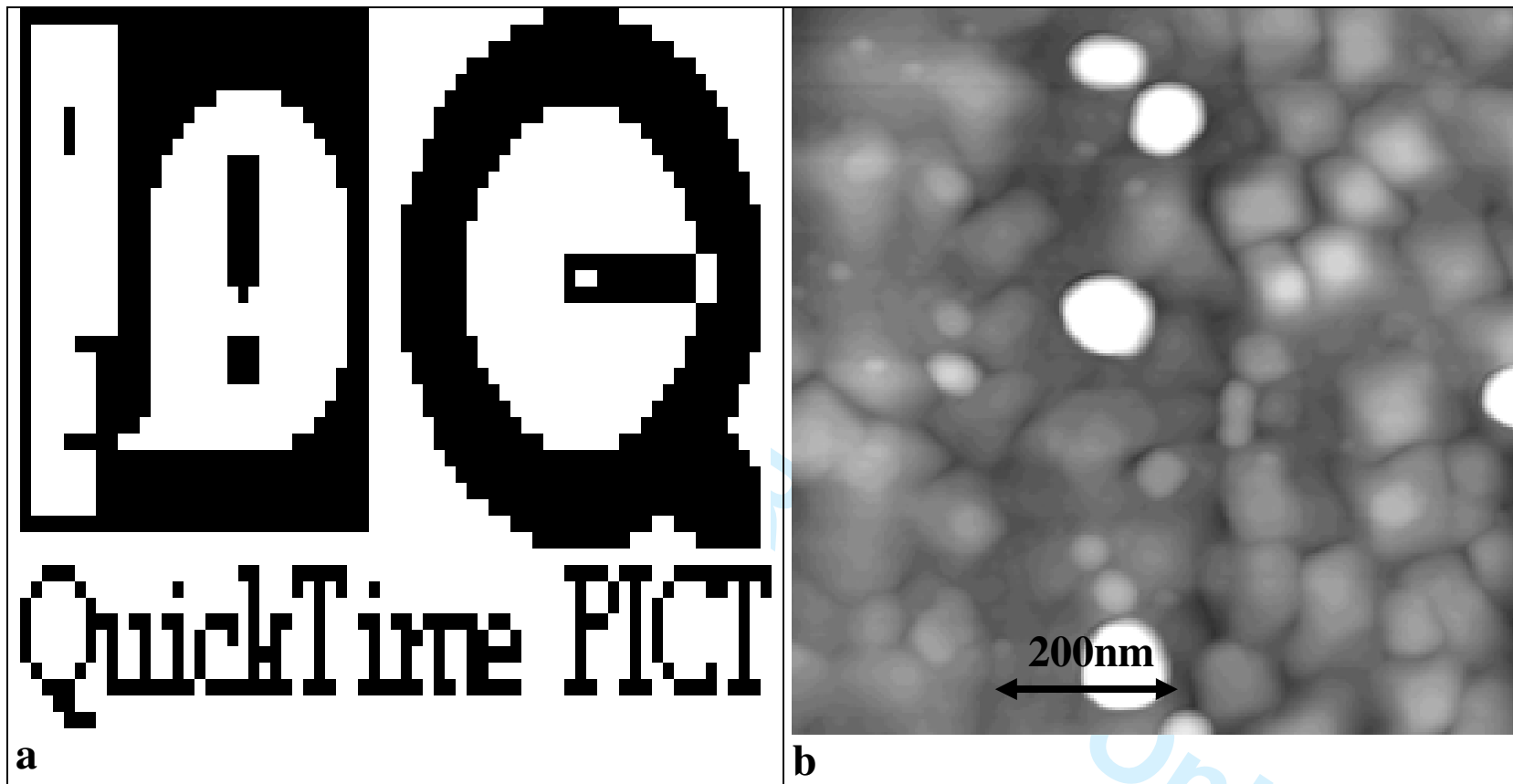
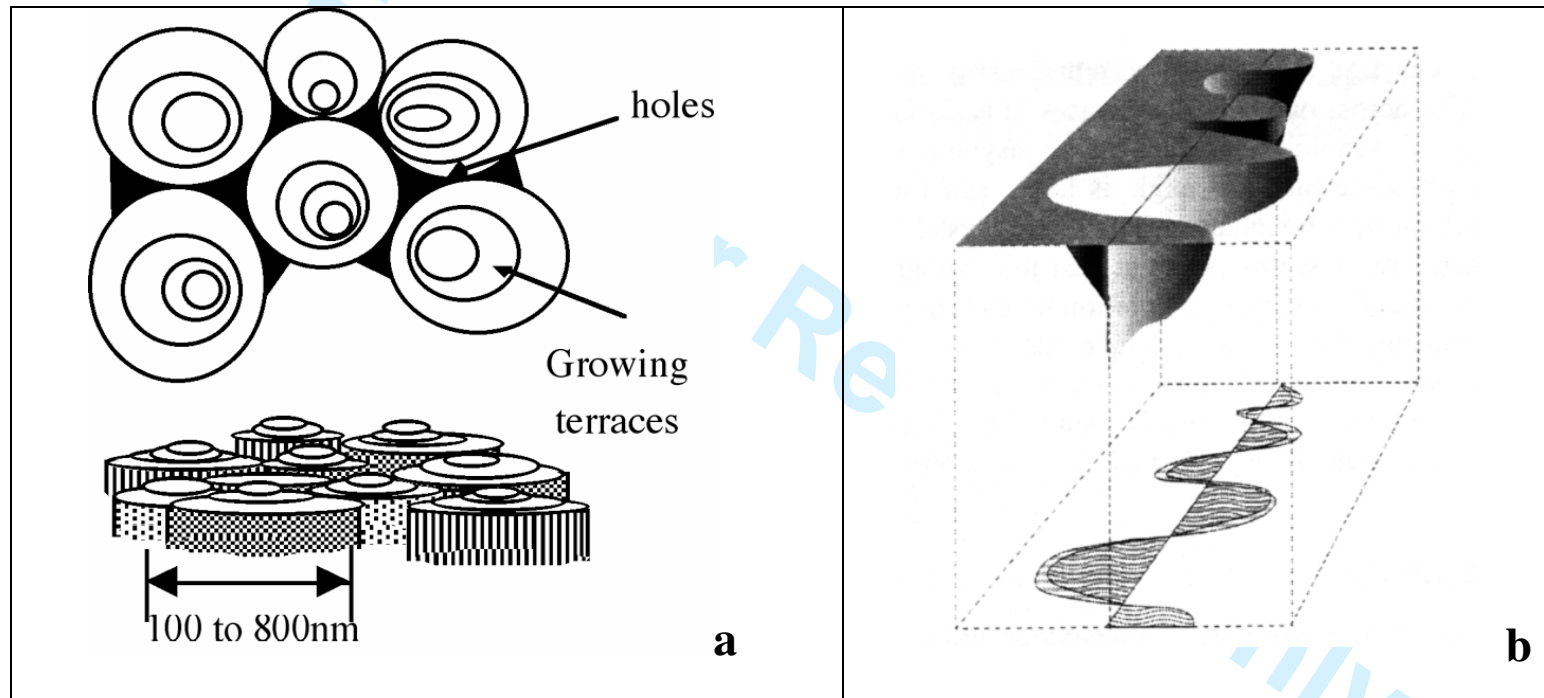


Figure 18

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**Figure 19**

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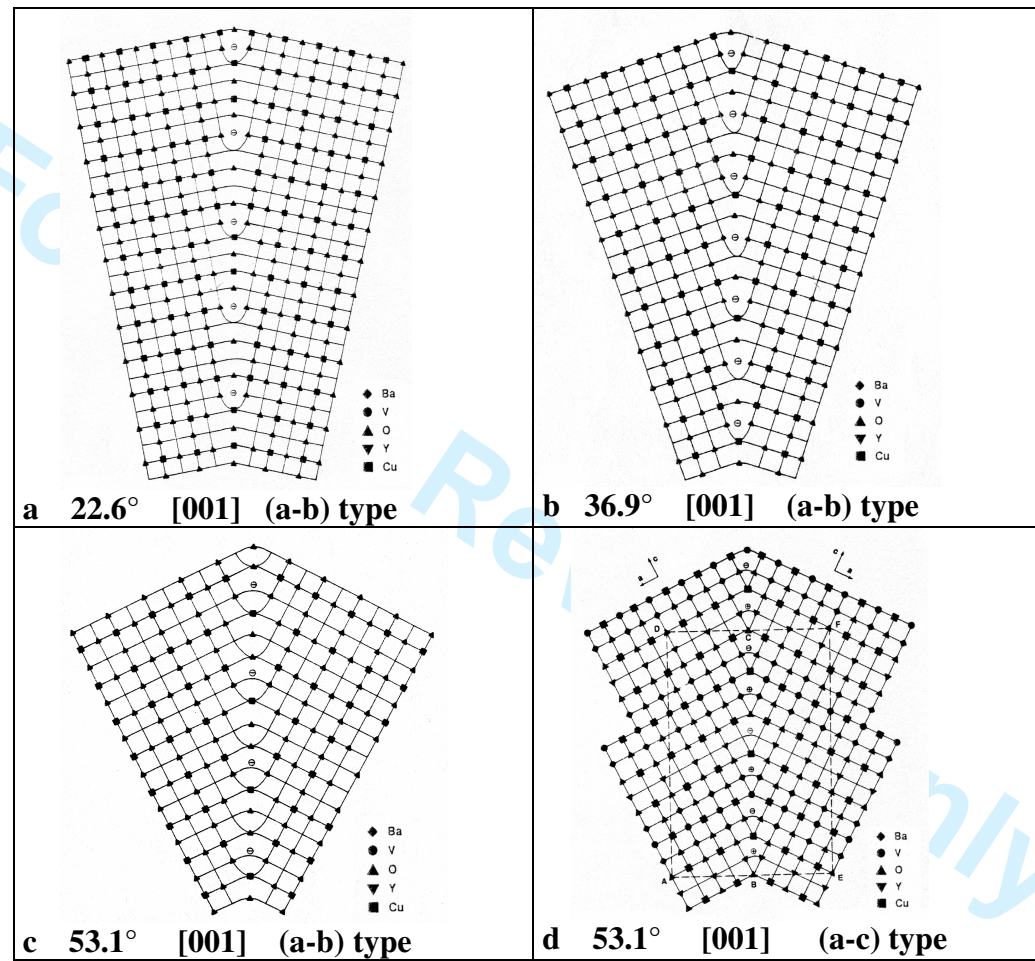


Figure 20

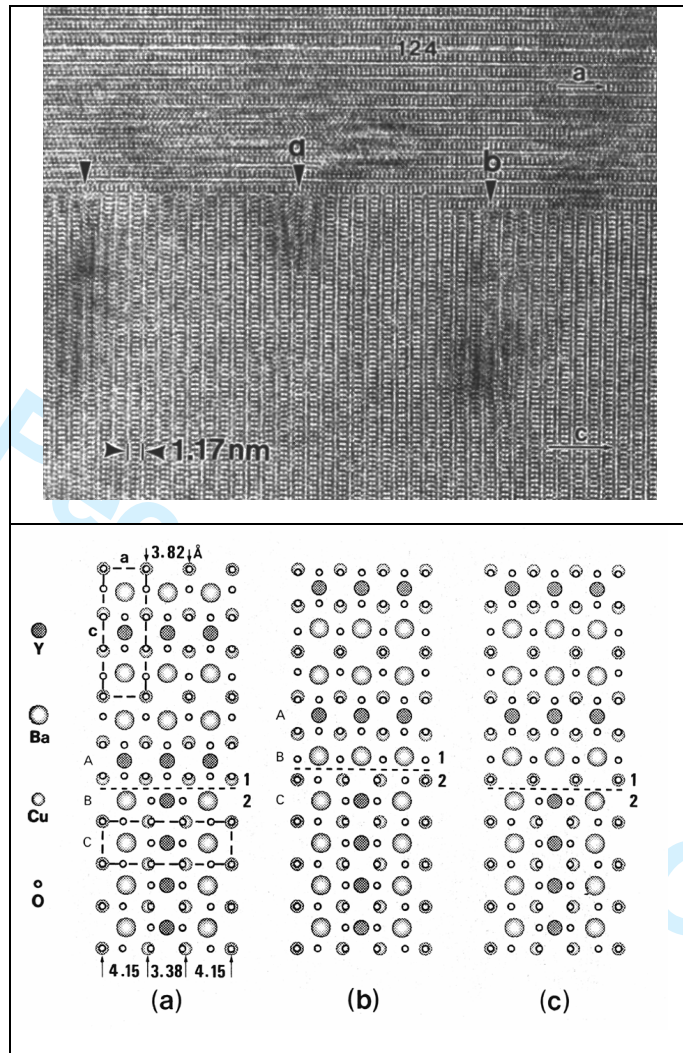


Figure 21

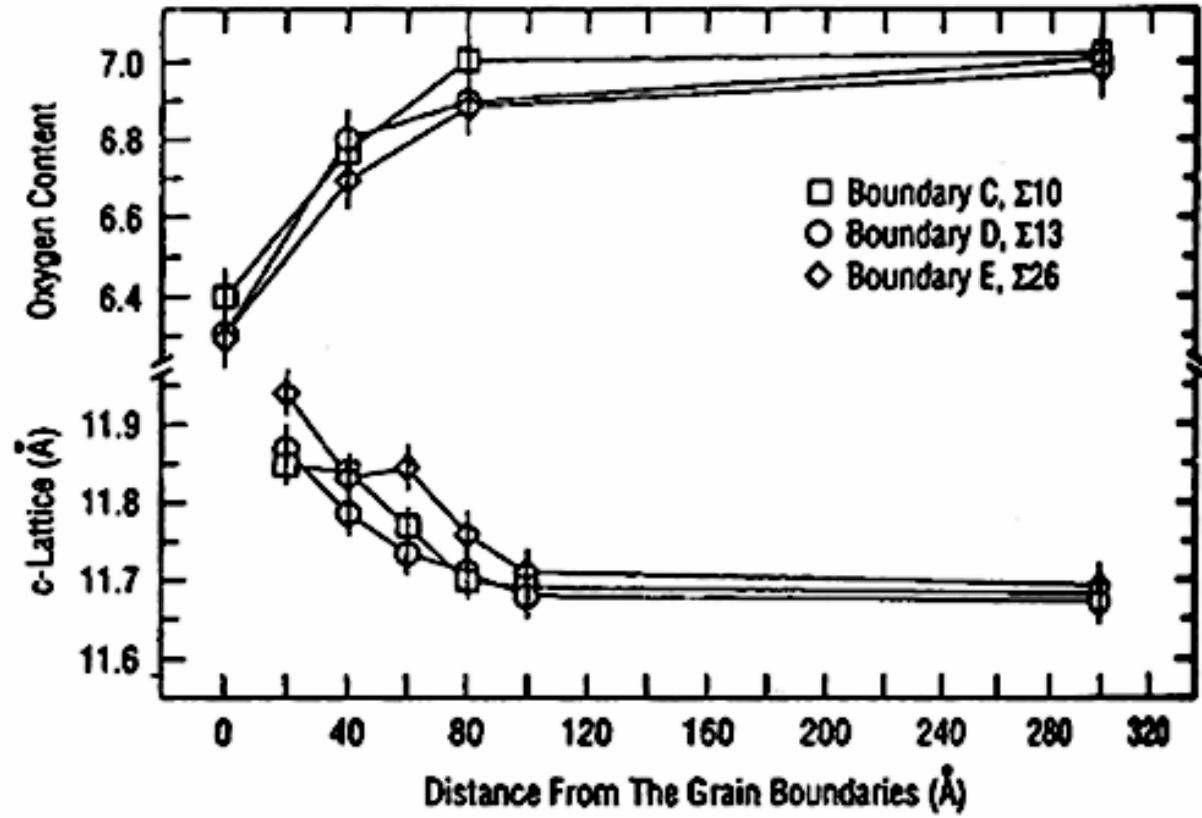


Figure 22

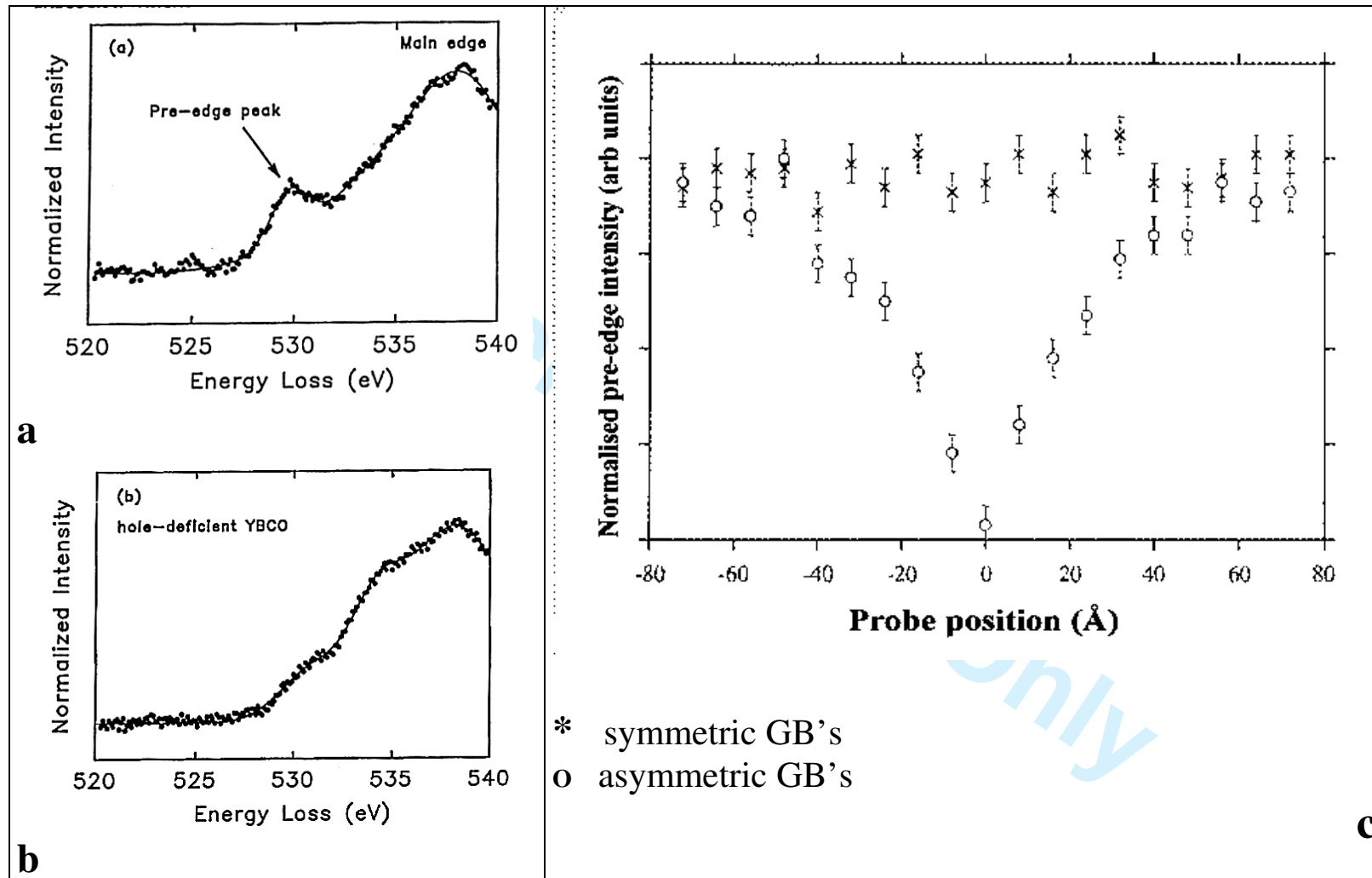


Figure 23

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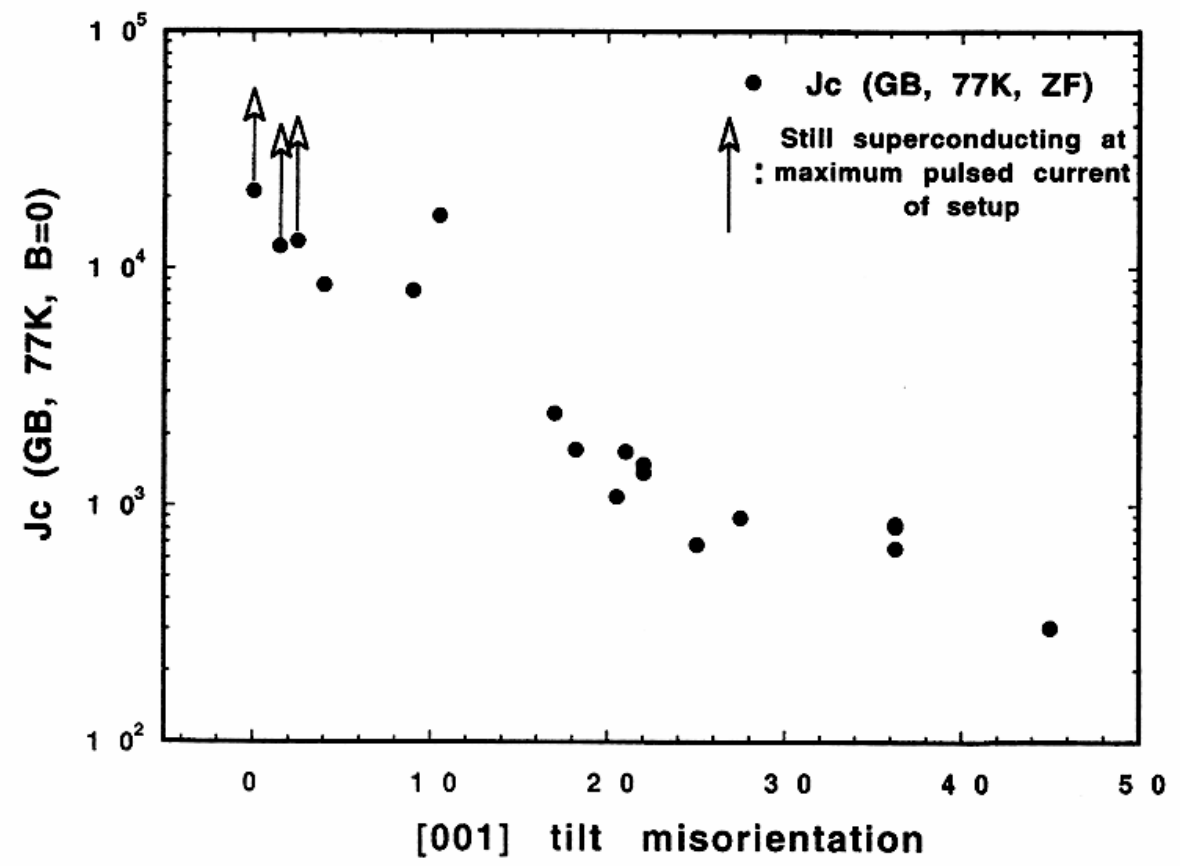
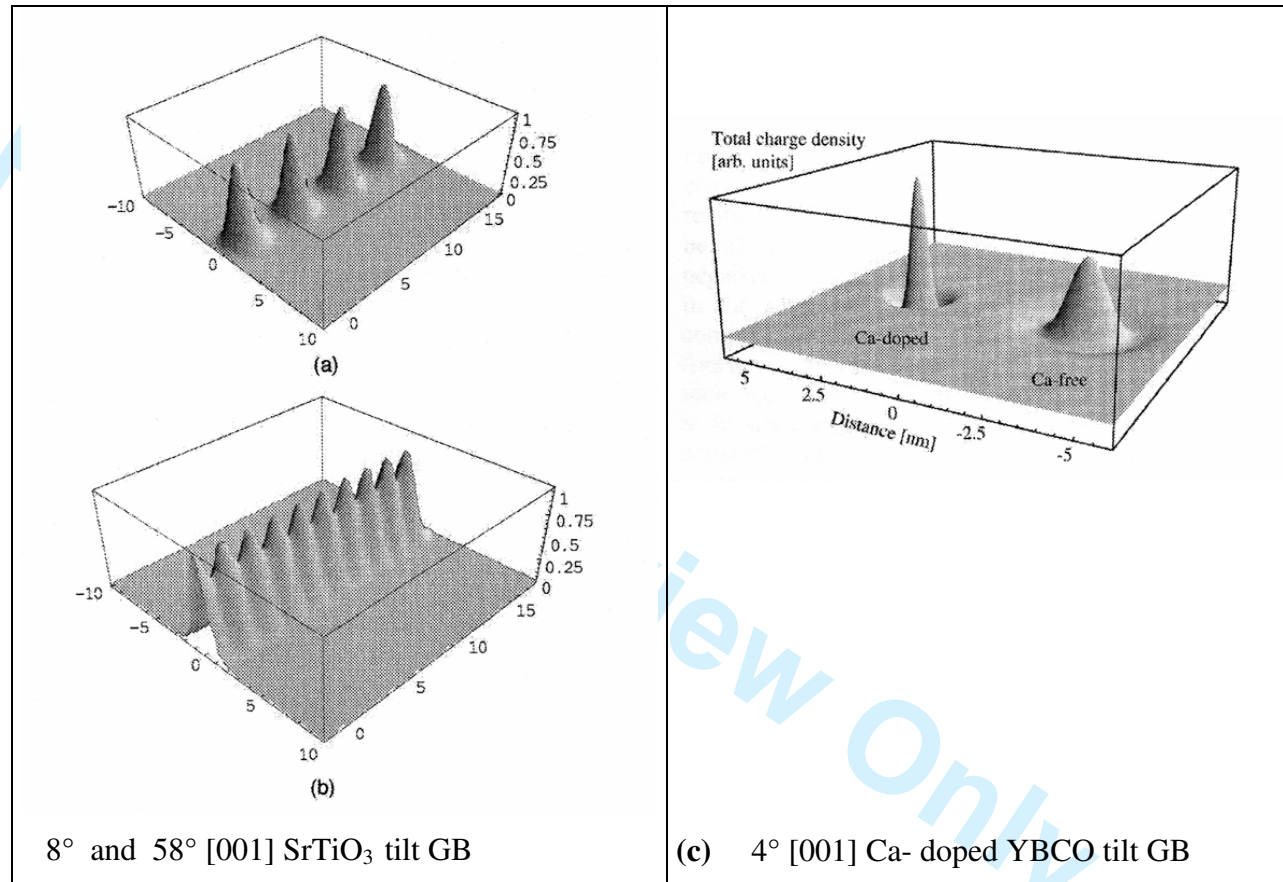


Figure 24

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**Figure 25**



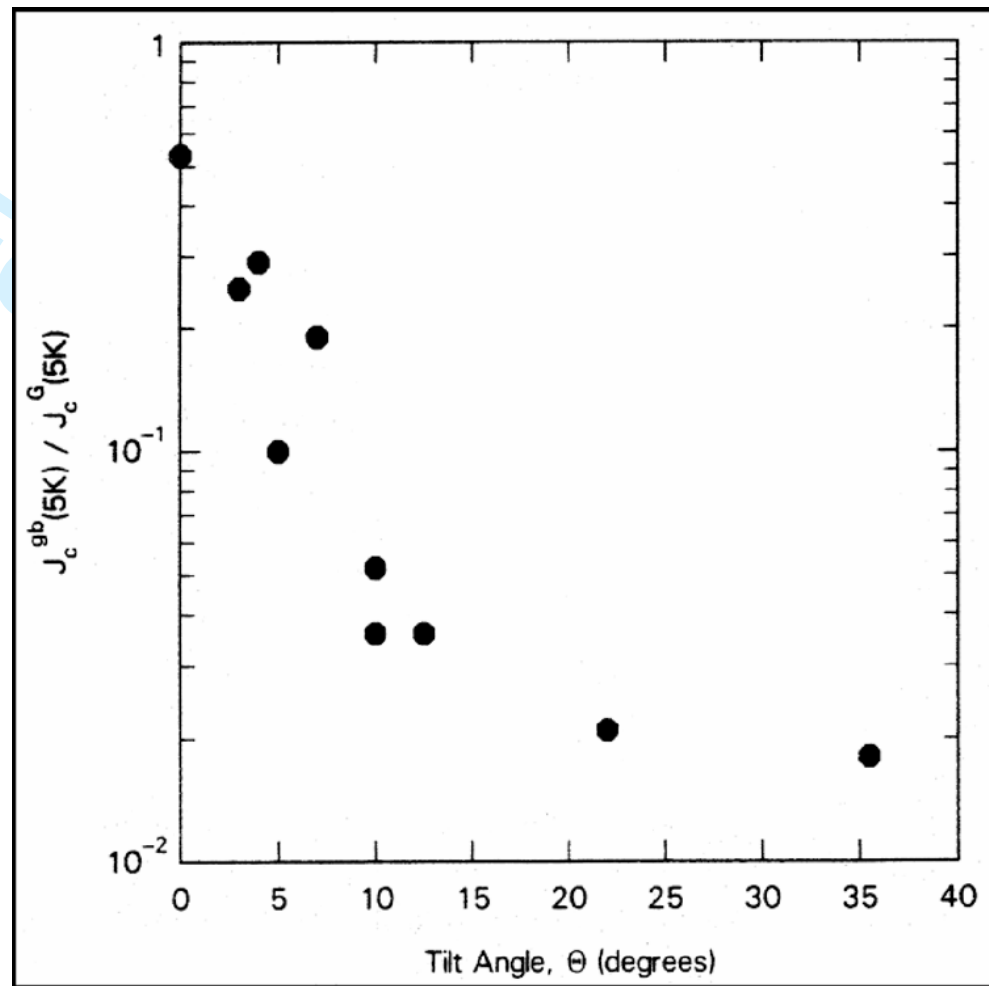


Figure 26

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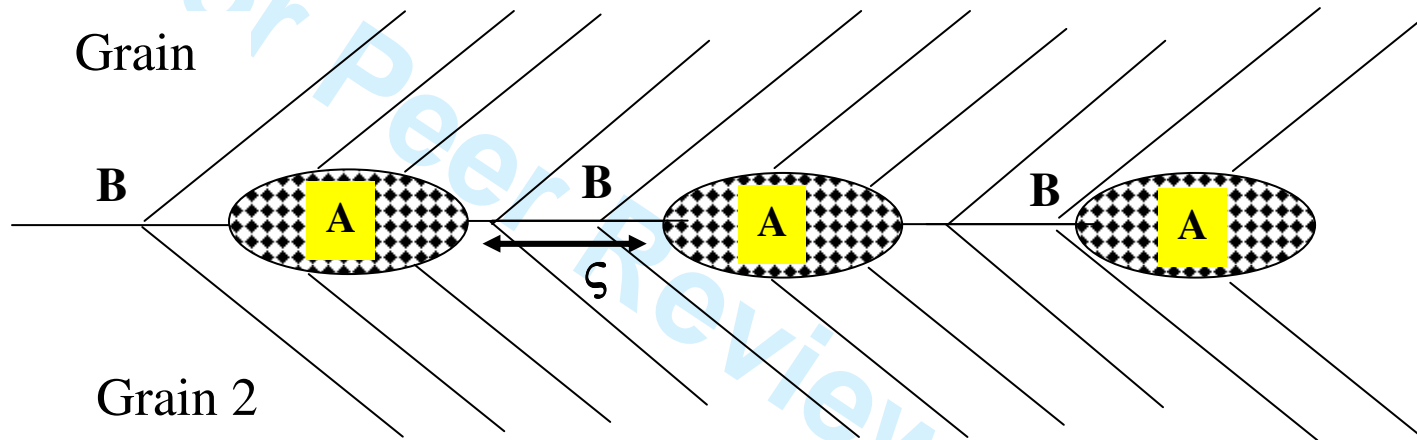


Figure 27

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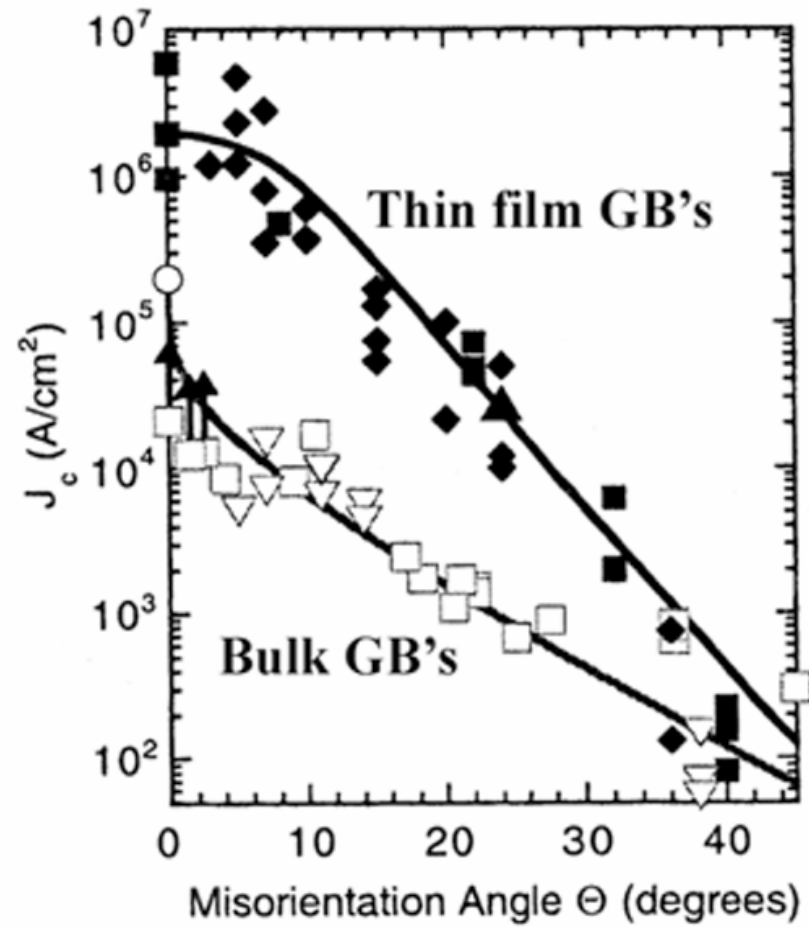
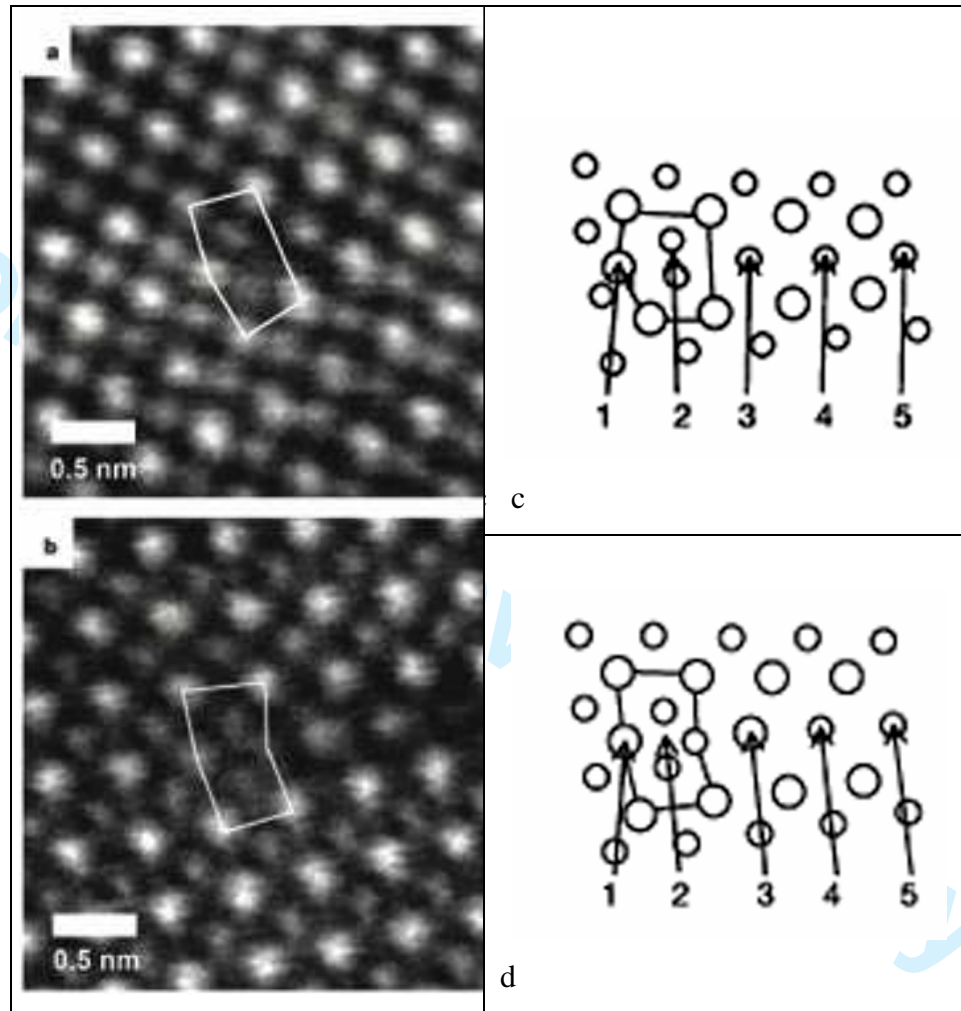


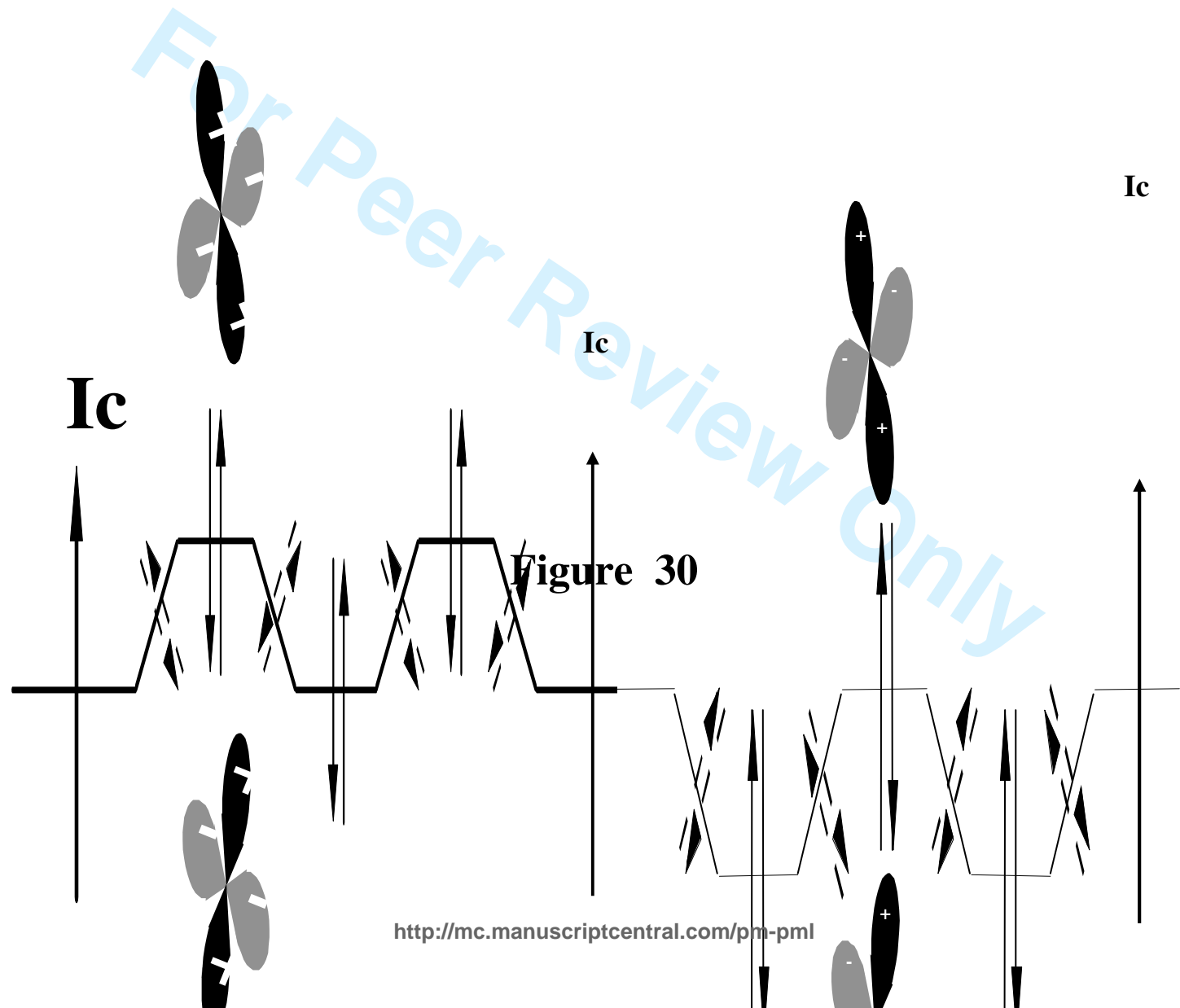
Figure 28

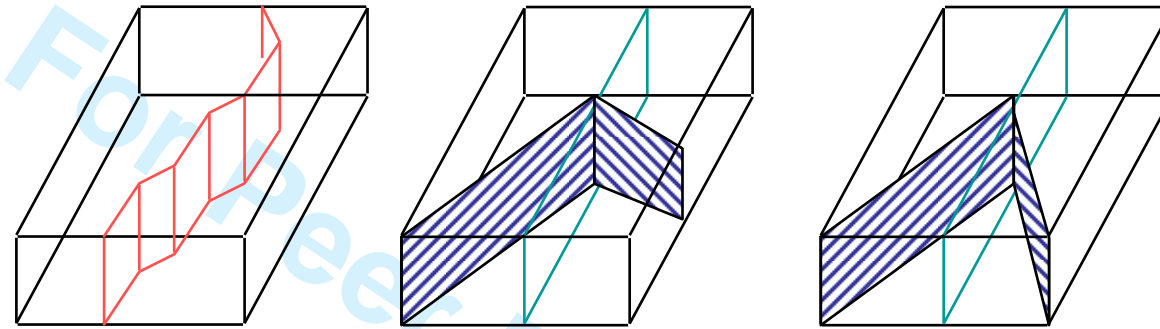


**Figure 29**

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**Facetted  
GB plane**

**Asymmetric GB**

**Symmetric GB**

**Figure 31a**

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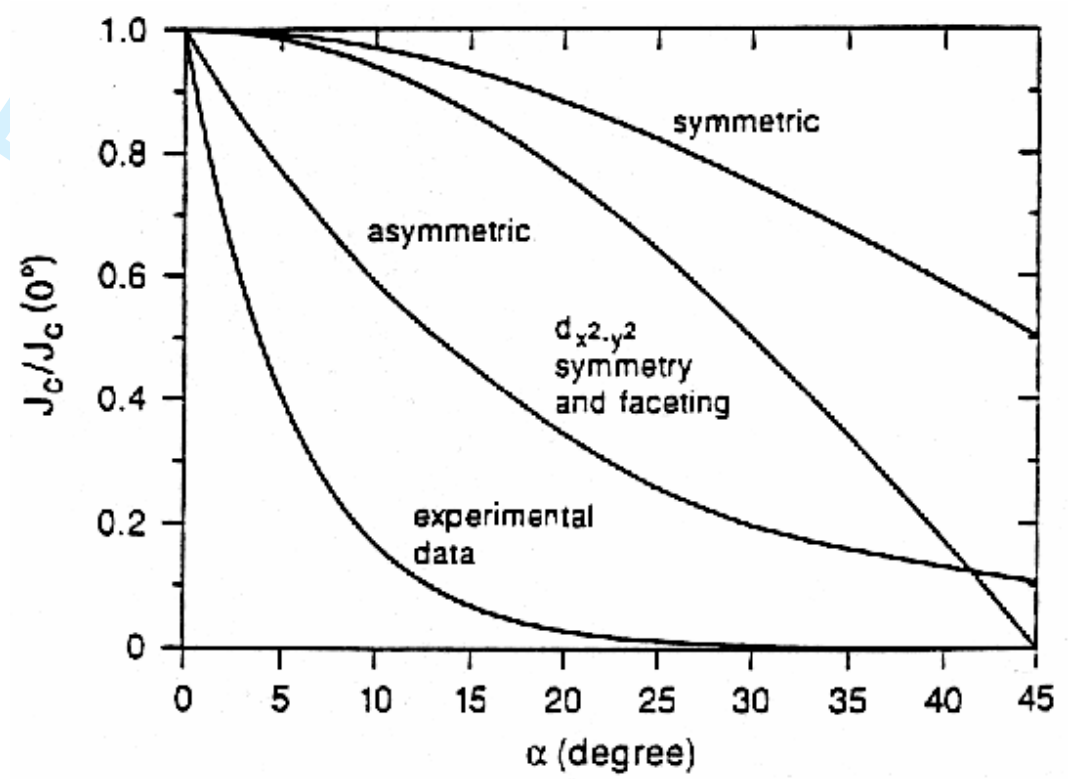


Figure 31b

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<b>YBCO Structures</b>	<b>Oxygen contents</b>	<b>T<sub>c</sub> (K)</b>	<b>Lattice Parameters (nm)</b>
<b>Ortho I</b>	<b>O<sub>7</sub> - O<sub>6.9</sub></b>	<b>91</b>	<b>a=0.382</b> <b>b=0.388</b> <b>c=1.168</b> <b>+ oxygen ordering*</b>
<b>Ortho II</b>	<b>O<sub>6.97</sub></b>	<b>maximum T<sub>c</sub>=92</b>	
<b>Ortho II</b>	<b>O<sub>6.6</sub> - O<sub>6.7</sub></b>	<b>60</b>	<b>+ oxygen ordering*</b>
<b>Tetragonal</b>	<b>O<sub>6.5</sub> - O<sub>6.4</sub></b>	<b>0</b>	<b>a=b=0.386</b> <b>c=1.171</b> <b>+ oxygen ordering*</b>
<b>*oxygen ordering occurs between O<sub>6.85</sub> and O<sub>6.4</sub></b>			

**Table 1**



SAMPLES	SUBSTRATES	211 GRAIN SIZES	T <sub>c</sub> (K)	Δ T <sub>c</sub> (K)	J <sub>c</sub> A/cm <sup>2</sup> at 77K
<b>D</b>	<b>MgO</b>	<1μm to 5μm	<b>82</b>	<b>13</b>	<b>0</b> (H//c) ~0
<b>E</b>	<b>Y<sub>2</sub>O<sub>3</sub></b>	2μm to >25μm	<b>91,5</b>	<b>1</b>	1.4 10 <sup>4</sup> (H//c= 1T) 3.5 10 <sup>4</sup> (H//c = 0)

Table 2

YBCO	Type of material	Low angle GB	Large angle GB	Special Σ GB	J <sub>c</sub> A/cm <sup>2</sup>
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system			<10°		10°<θ< 90°		20°<θ< 90°		
			Clean	Degradated	Clean	Degradated	Clean	Degradated	
Solid-solid diffusion reaction	Bulk classic Ceramic		Yes	No	Some	Some	Some	Some	$J_c < 10^3$
	Thin films grown on single crystal substrate SrTiO <sub>3</sub> , MgO		Yes	No	Yes	No	Yes	No	$10^6 < J_c < 10^7$
	GB thin film grown on bicrystal SrTiO <sub>3</sub>		Yes	No	Yes	No	Yes	No	$J_c = f(\alpha)$
Solid-liquid diffusion reaction	Single crystal : Twins (110)		-----	-----	-----	-----	Yes	-----	$10^5 < J_c < 10^6$
	Bulk bicrystals		Yes	-----	Yes	-----	Yes	-----	$J_c = f(\alpha)$
	Melt-textured Without substrate	under magnetic field	Some	Some	Some	Some	-----	-----	$10^4 < J_c < 10^5$
	Melt-textured with substrate	Y <sub>2</sub> O <sub>3</sub> ceramic	-----	-----	Some	Some	-----	-----	$10^4 < J_c < 10^5$
Y <sub>2</sub> BaCuO <sub>5</sub> Ceramic (211)		-----	-----	Some	Some	-----	-----	$10^4 < J_c < 10^5$	
	Single crystal MgO	Some	Some	No	Yes	-----	-----	$J_c \cong 0$	

**Table 3**

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