



# Design of complex safety-related systems in accordance with IEC 61508

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# Overview

## I. Introduction & IEC 61508

- safety systems & IEC 61508 framework
- introduction to design & development of complex systems

## II. Design of complex systems

- reliability issues for complex systems
- fault tree based approach to deal with complex systems

## III. Application

- case study on infrared gas transmitter
- reliability and uncertainty analyses

## IV. Discussion & conclusion

# I. Introduction & IEC 61508

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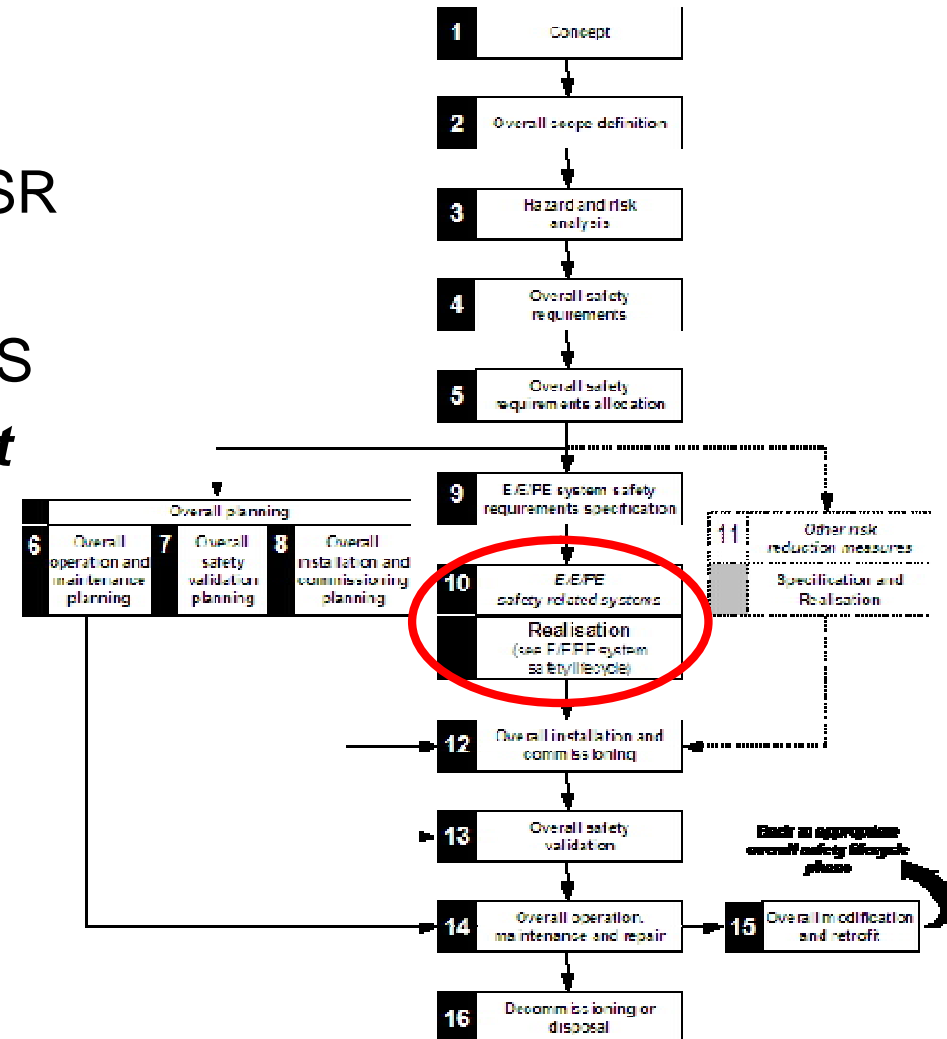
- **Safety instrumented systems (SIS)**
  - play a major part in industrial risk management
- **IEC 61508**
  - generic functional safety standard for SIS design
  - considers the overall system and software life cycle
  - introduces safety requirements (SR)
    - **safety function**: to achieve a safe state of equipment under control
    - **safety integrity**: probability of a SIS performing the safety function
  - **safety integrity level (SIL)**

SIL	Average probability of SIS failure to perform its safety function on demand ( $PFD_{avg}$ )
SIL 4	$10^{-5} \leq PFD_{avg} < 10^{-4}$
SIL 3	$10^{-4} \leq PFD_{avg} < 10^{-3}$
SIL 2	$10^{-3} \leq PFD_{avg} < 10^{-2}$
SIL 1	$10^{-2} \leq PFD_{avg} < 10^{-1}$

# I. Introduction & IEC 61508

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- **IEC 61508 framework**
  - development of the overall SR
  - SR allocation to the SIS
  - SR specification for each SIS
  - **SIS design & development**
  - installation, validation
  - operation, maintenance
- **Other requirements**
  - documentation
  - management
  - verification
- **Informative guidelines**





# I. Introduction & IEC 61508

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- Requirements for SIS design & development
  - hardware fault tolerance (HFT)
  - safe failure fraction (SFF)
  - ***average probability of SIS failure on demand ( $PFD_{avg}$ )***
  - avoidance of the systematic faults, proven in use
  - some other specific requirements
- Complex system (IEC 61508)
  - ***not well defined failure mode*** for at least one component
  - ***or undetermined system behaviour under faulty conditions***
- “Type B” system (IEC 61508)
  - insufficient data to support claims for failure rates
  - ***or*** complex system

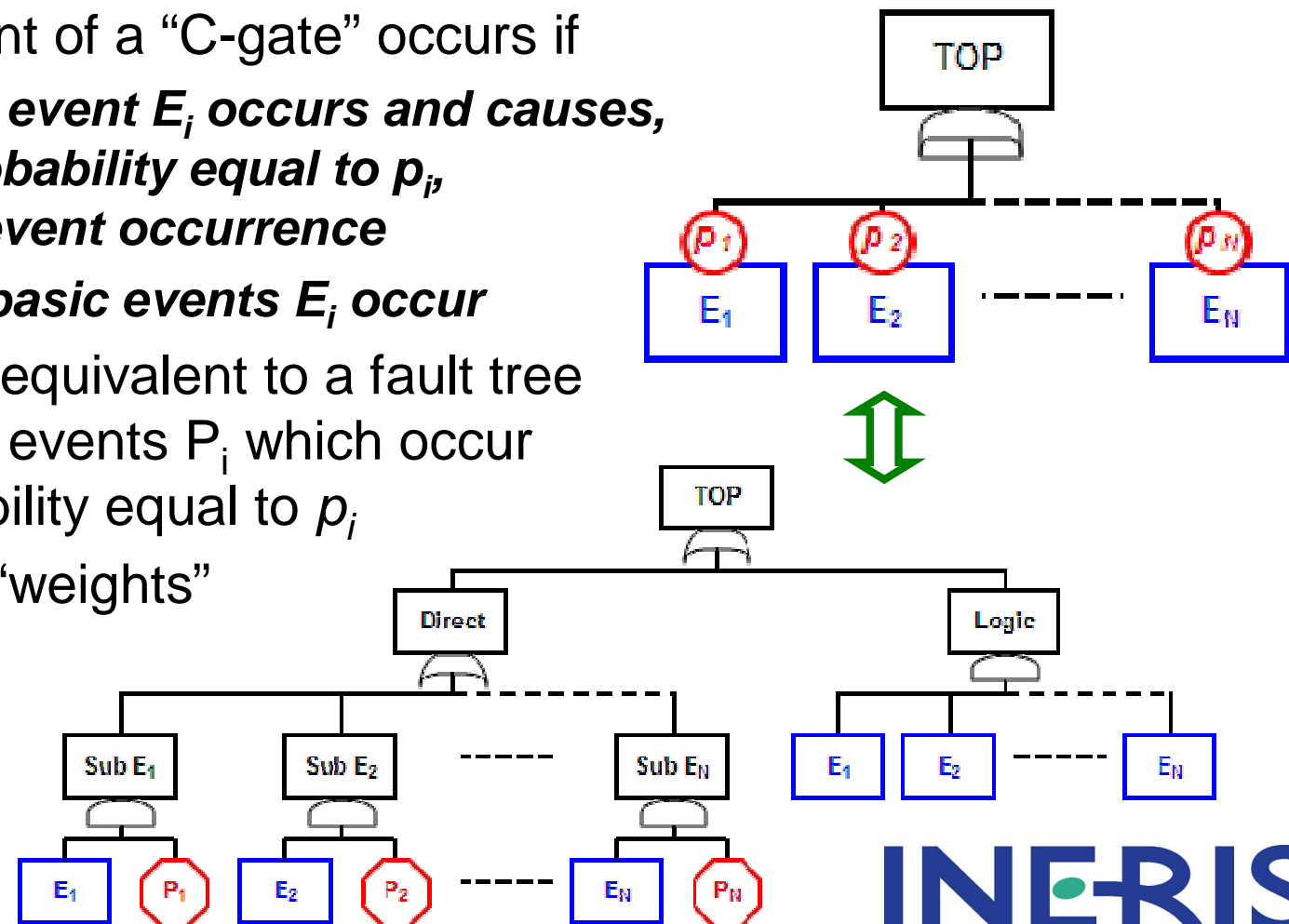
## II. Design of complex systems 1/3

- **Reliability issues for “type B” systems**
  - many references deal with uncertainty on failure rates
    - e.g. comparison of data sources, Monte Carlo, fuzzy sets, etc.
  - fewer analyses regarding ***uncertainty into system behaviour***
- **Limitations of reliability models**
  - system responses to events have to be strictly defined...
  - ...according to architectural constraints of discrete nature
    - e.g. fault tree gates, Markov graph states and transitions
  - random changes in models could yield unrealistic configurations
- **Proposal**
  - ***system behaviour should be parameterised so that the system part architectures can be continuously graduated***

## II. Design of complex systems 2/3

- Continuous gate for fault tree based approach

- the TOP-event of a “C-gate” occurs if
  - any basic event  $E_i$  occurs and causes, with a probability equal to  $p_i$ , the TOP-event occurrence
  - or all the basic events  $E_i$  occur
- a “C-gate” is equivalent to a fault tree with fictitious events  $P_i$  which occur with a probability equal to  $p_i$
- $p_i$  are called “weights”



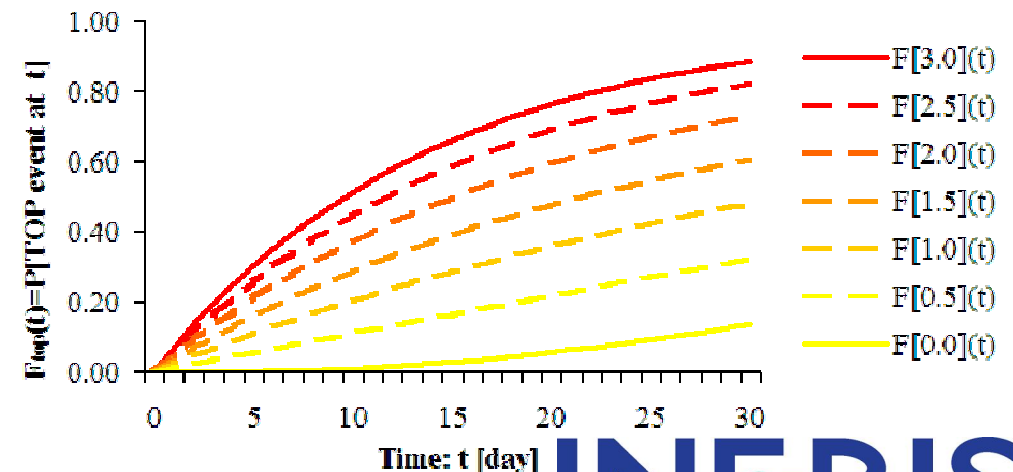
## II. Design of complex systems 3/3

- Continuous gate properties

- $F_i(t)$  probability of occurrence of basic event  $E_i$  at time  $t$
- $p_i$  constant probability of occurrence of fictitious event  $P_i$
- $F_{top}(t)$  probability of occurrence of C-gate TOP-event at time  $t$

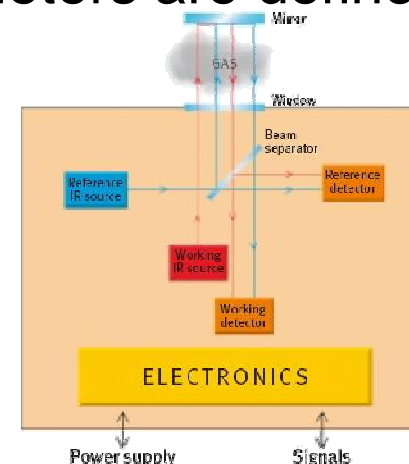
$$F_{top}(t) = 1 - \prod_{i=1}^N (1 - p_i \cdot F_i(t)) + \prod_{i=1}^N ((1 - p_i) \cdot F_i(t))$$

Weight			Unreliability function
$P_1$	$P_2$	$P_3$	
0	0	0	$F[0.0](t)$ / parallel structure
0.5	0	0	$F[0.5](t)$
0.5	0.5	0	$F[1.0](t)$
0.5	0.5	0.5	$F[1.5](t)$
1	0.5	0.5	$F[2.0](t)$
1	1	0.5	$F[2.5](t)$
1	1	1	$F[3.0](t)$ / series structure

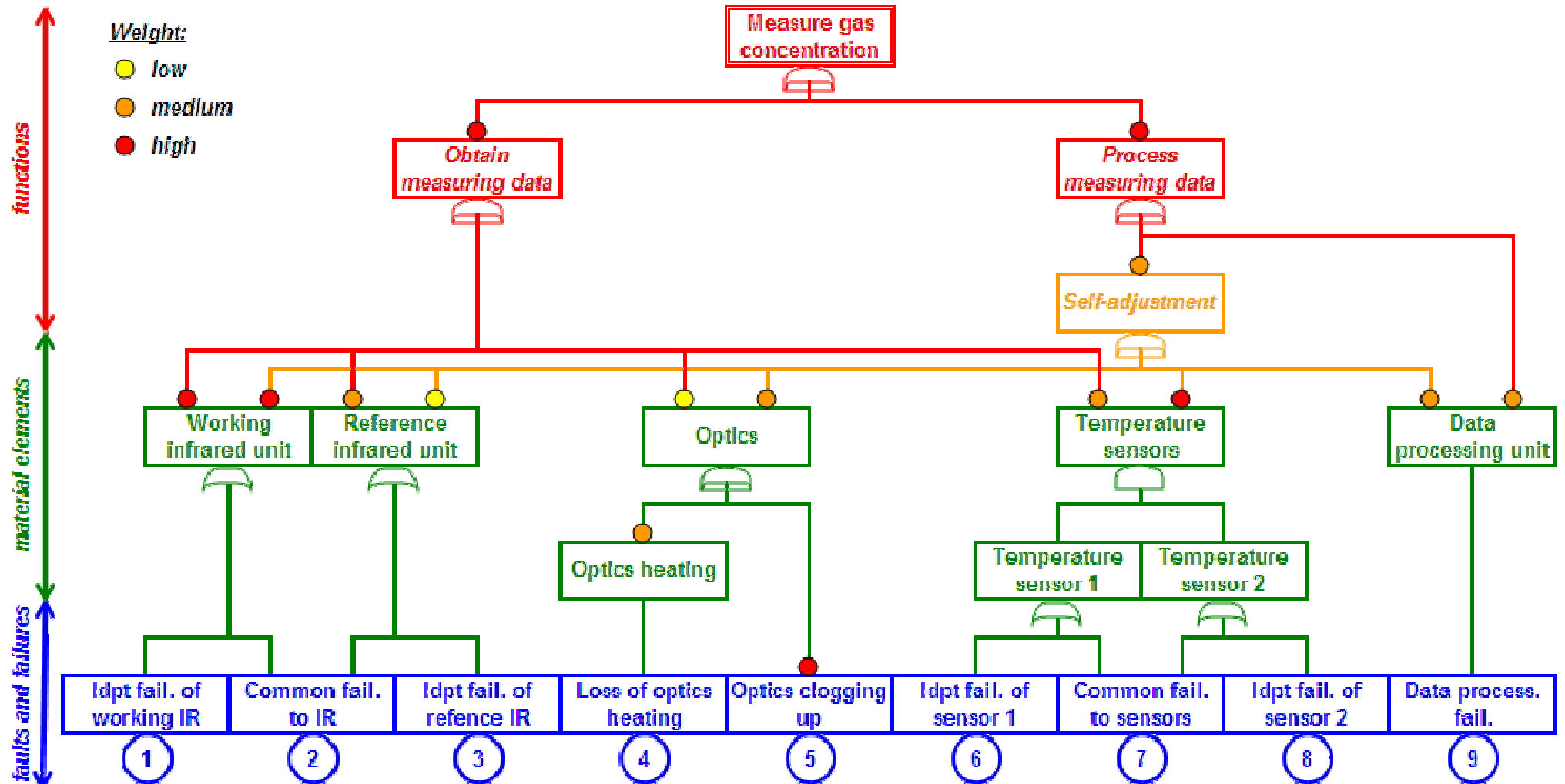


## III. Application

- **Case study on infrared gas transmitter**
  - to measure gas concentration by infrared absorption
  - the use of a working and a reference infrared units allows corrections of the optics clogging up and power fluctuations
  - heating elements aim to prevent steam from building up on optics
  - redundant temperature sensors are used for digital compensation
  - a data processing unit carries out all processing and calculations
  - off-set and gain drift parameters are defined by self-adjustments



# III. Application



## III. Application

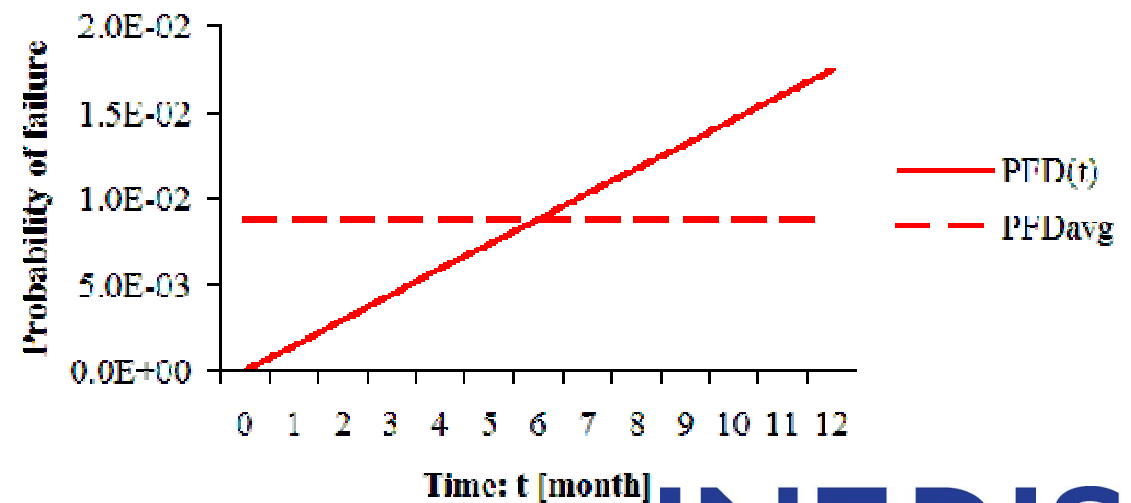
- Fault tree analyses

- input data:

- $\{p_L, p_M, p_H\}$  weigh value according to type
- $F_i(t) = \exp(-\lambda_i \cdot t)$  probability of fault or failure occurrence  $i$  at time  $t$

- analyses are performed using equivalent fault trees and SimTree from Aralia WorkShop software tool

Type	Name	Base value	Name	Base value [hour <sup>-1</sup> ]
low	p <sub>L</sub>	0.10	λ <sub>1</sub>	4.0·10 <sup>-7</sup>
medium	p <sub>M</sub>	0.50	λ <sub>2</sub>	1.0·10 <sup>-7</sup>
high	p <sub>H</sub>	0.90	λ <sub>3</sub>	4.0·10 <sup>-7</sup>
			λ <sub>4</sub>	1.0·10 <sup>-6</sup>
			λ <sub>5</sub>	3.0·10 <sup>-6</sup>
			λ <sub>6</sub>	5.0·10 <sup>-7</sup>
			λ <sub>7</sub>	1.5·10 <sup>-7</sup>
			λ <sub>8</sub>	5.0·10 <sup>-7</sup>
			λ <sub>9</sub>	5.0·10 <sup>-7</sup>





# III. Application

- **Uncertainty analyses: input data**
  - failure rate uncertainties are represented by lognormal distributions with error factors equal to 5
  - system behaviour uncertainties are translated into weight value uncertainties and are represented by uniform distributions
  - ***variances are greater for weight values than for failure rates***

Name	Uncertainty analysis		
	law	mean	variance
$\lambda_1$	log-Normal	$4.0 \cdot 10^{-7}$	$3.2 \cdot 10^{-14}$
$\lambda_2$	log-Normal	$1.0 \cdot 10^{-7}$	$2.0 \cdot 10^{-15}$
$\lambda_3$	log-Normal	$4.0 \cdot 10^{-7}$	$3.2 \cdot 10^{-14}$
$\lambda_4$	log-Normal	$1.0 \cdot 10^{-6}$	$2.0 \cdot 10^{-13}$
$\lambda_5$	log-Normal	$3.0 \cdot 10^{-6}$	$1.8 \cdot 10^{-12}$
$\lambda_6$	log-Normal	$5.0 \cdot 10^{-7}$	$4.9 \cdot 10^{-14}$
$\lambda_7$	log-Normal	$1.5 \cdot 10^{-7}$	$4.5 \cdot 10^{-15}$
$\lambda_8$	log-Normal	$5.0 \cdot 10^{-7}$	$4.9 \cdot 10^{-14}$
$\lambda_9$	log-Normal	$5.0 \cdot 10^{-7}$	$4.9 \cdot 10^{-14}$

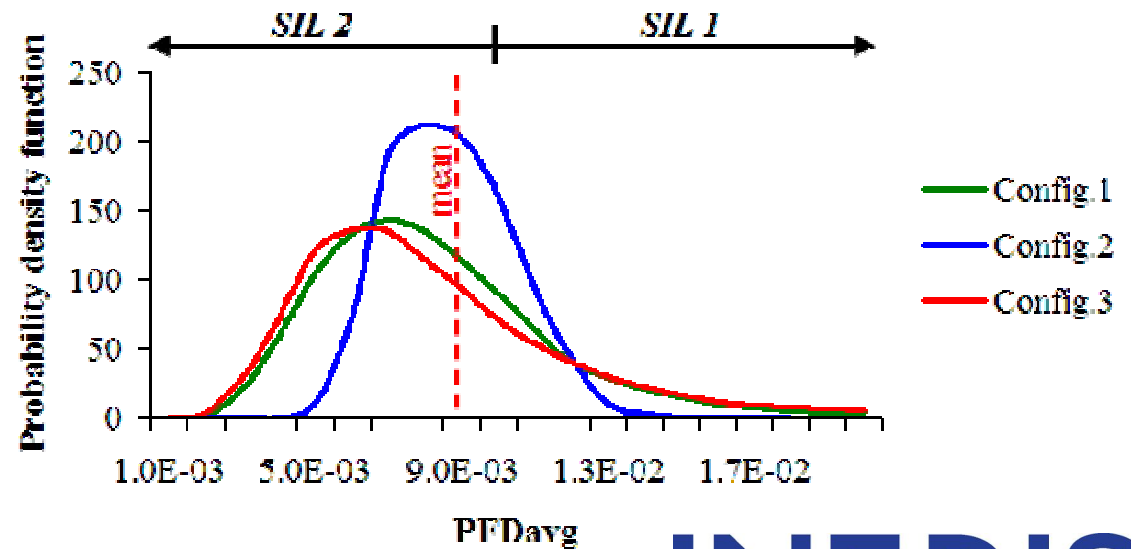
Type	Name	Uncertainty analysis		
		law	mean	variance
low	p <sub>L</sub>	U[0.0, 0.2]	0.10	$3.3 \cdot 10^{-3}$
medium	p <sub>M</sub>	U[0.2, 0.8]	0.50	$3.0 \cdot 10^{-2}$
high	p <sub>H</sub>	U[0.8, 1.0]	0.90	$3.3 \cdot 10^{-3}$

# III. Application

- **Uncertainty analyses: results**
  - three configurations are compared
  - each analysis is performed by 1,000,000 Monte Carlo simulations
  - ***variances are much lower for results than for any input***
  - ***uncertainties into system behaviour are not significant***

Configuration	Uncertainty analysis on
Config.1	Failure rates only
Config.2	System behaviour (i.e. weight values) only
Config.3	Failure rates and system behaviour

Configuration	Mean	Variance	P[SIL2]	P[SIL1]
Config.1	$8.69 \cdot 10^{-3}$	$1.5 \cdot 10^{-5}$	0.74	0.26
Config.2	$8.73 \cdot 10^{-3}$	$2.9 \cdot 10^{-6}$	0.78	0.22
Config.3	$8.68 \cdot 10^{-3}$	$2.0 \cdot 10^{-5}$	0.74	0.26



## IV. Discussion & conclusion 1/1

- **Uncertainties into system behaviour**
  - can be taken into account by continuous fault tree gates
  - can be translated into equivalent fault trees using fictitious events
- **Discussion of results**
  - taking the system behaviour uncertainties into account leads to  $PFD_{avg}$  evaluation with a relatively small variance
  - uncertainties into inputs, especially for weight values, are partially mitigated through the proposed model
  - assuming uncertainties into failure rates, the addition of system behaviour uncertainties does not have a significant effect
- **the lack of knowledge in system behaviour can be accounted for and partially compensated for by the proposed approach to evaluate  $PFD_{avg}$**



**Thanks for your attention**

**Questions & Comments are Welcome**

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