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MAXIMUM CURVATURES OF 0/90 PLATES UNDER THERMAL STRESS: MODELLING AND EXPERIMENTAL VALIDATION

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ABSTRACT

In this paper, special attention is paid to the maximum curvatures induced by *uniform* thermal fields in $0_m/90_n$ laminated square plates. The effects of the relative thickness of the 90° ply e_{90} and of the elastic and thermoelastic anisotropy on the curvature tensor are then studied. The conditions for which the curvatures are maximum are established by adopting the polar method within the context of the classical lamination theory. It is found that the location of the maximum curvatures is influenced by the level of *elastic* anisotropy, defined by the polar parameter R_I , while the magnitude of the maximum curvatures is driven by the *thermoelastic* properties, that is, the coefficients of thermal expansion. The capabilities of a geometrical non-linear model are explored and experimental evidence of maximum curvatures of glass/epoxy composite materials are provided.

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KEYWORDS : A. POLIMER-MATRIX COMPOSITES, C. LAMINATE THEORY, RESIDUAL STRESS

1 INTRODUCTION

$0_m/90_n$ unsymmetric composite plates under thermal stress deform because of the thermoelastic coupling. Indeed, the curing temperature of such plates is different from the service ambient temperature, therefore the temperature differential ($T_{\text{cure}} - T_{\text{room}}$) produces consistent thermal loads (thermal forces and moments) and curvatures. Curvature measurements are utilized to determine curing stresses ([1-2]). The basic idea is to identify the laminate stacking sequences allowing to perform optimal experiments due to their high sensitivity to external loads. Also, it would be desirable in preliminary design of structures to design plates that have a desired deformed shape when subjected to thermal solicitations.

Vannucci [3-4] studied in detail the phenomenon of elastic and thermoelastic coupling, that is, the structure of \mathbf{B} and \mathbf{V} tensors of the classical laminated plate theory (CLPT, [5]). He employed the polar method, making use of invariant quantities of such tensors; in particular, by this analytical method he was able to determine explicit expressions for their maximum norms.

In the present paper, the approach already employed by Vannucci is extended to the curvature tensors k , whose components are maximised

for plates belonging to the $0_m/90_n$ family. A geometrical nonlinear model of plates is then used to verify the applicability range of the simple linear theory. The paper is divided as follows : first, the employed models are briefly recalled, then the results of some simulations are presented and, finally, experimental results validating the models are provided.

2 MODEL DESCRIPTION

2.1 Recall of the polar method and conditions of maximum coupling

The Cartesian components of the anisotropic stiffness tensor, \mathbf{Q} , of a composite ply may be expressed in their polar form [3] by employing the 6 parameters T_0 , T_1 , R_0 , R_1 , Φ_0 and Φ_1 as follows:

$$\begin{aligned}
 Q_{xx} &= T_0 + 2T_1 + R_0 \cos 4\Phi_0 + 4R_1 \cos 2\Phi_1 \\
 Q_{yy} &= -T_0 + 2T_1 - R_0 \cos 4\Phi_0 \\
 Q_{xy} &= T_0 + 2T_1 + R_0 \cos 4\Phi_0 - 4R_1 \cos 2\Phi_1 \\
 Q_{ss} &= T_0 - R_0 \cos 4\Phi_0 \\
 Q_{xs} &= R_0 \sin 4\Phi_0 + 2R_1 \sin 2\Phi_1 \\
 Q_{ys} &= -R_0 \sin 4\Phi_0 + 2R_1 \sin 2\Phi_1
 \end{aligned} \tag{1}$$

with,

$$\begin{aligned}
 8T_0 &= Q_{xx} - 2Q_{xy} + 4Q_{xs} + Q_{yy} \\
 8T_1 &= Q_{xx} + 2Q_{xy} + Q_{yy} \\
 8R_0 e^{4i\Phi_0} &= Q_{xx} - 2Q_{xy} - 4Q_{ss} + Q_{yy} + 4i(Q_{xs} - Q_{ss}) \\
 8R_1 e^{2i\Phi_1} &= Q_{xx} - Q_{yy} + 2i(Q_{xs} + Q_{ss})
 \end{aligned} \tag{2}$$

The following statements can be formulated:

- T_0, T_1, R_0, R_1 and $\Phi_0 - \Phi_1$ are invariant under a rotation θ with respect to the reference frame,
- a material is isotropic if $R_0 = R_1 = 0$. T_0 and T_1 constitute the isotropic parts of \mathbf{Q} , while R_0, R_1, Φ_0, Φ_1 constitute its anisotropic part,
- \mathbf{Q} is orthotropic if and only if $(\Phi_0 - \Phi_1) = k\pi/4$ with k integer.

The equations of the classical plate lamination theory state that

[5]:

$$\begin{aligned} \mathbf{N} &= \mathbf{A}\boldsymbol{\varepsilon}_0 + \mathbf{B}k - \mathbf{U}\Delta T \\ \mathbf{M} &= \mathbf{B}\boldsymbol{\varepsilon}_0 + \mathbf{D}k - \mathbf{V}\Delta T \end{aligned} \quad (3)$$

Invariant quantities analogous to those defined in equation (2) can be introduced tensors for \mathbf{A} , \mathbf{B} , \mathbf{D} , \mathbf{U} , \mathbf{V} , respectively $\bar{T}_0, \bar{T}_1, \bar{R}_0, \bar{R}_1, \bar{\Phi}_0, \bar{\Phi}_1$ for \mathbf{A} , $\hat{T}_0, \hat{T}_1, \hat{R}_0, \hat{R}_1, \hat{\Phi}_0, \hat{\Phi}_1$ for \mathbf{B} , $\tilde{T}_0, \tilde{T}_1, \tilde{R}_0, \tilde{R}_1, \tilde{\Phi}_0, \tilde{\Phi}_1$ for \mathbf{D} , $\bar{T}, \bar{R}, \bar{\Phi}$ for \mathbf{U} and $\hat{T}, \hat{R}, \hat{\Phi}$ for \mathbf{V} . The reader can refer to the work by Vannucci et al. [3] for more detail about the exact definition of such quantities. Here, we simply note that tensors \mathbf{B} and \mathbf{V} represent, respectively elastic and thermoelastic coupling.

Finally the norm of a fourth order tensor (\mathbf{A} for instance) can be defined by the following expression:

$$A = \sqrt{\bar{T}_0^2 + 2\bar{T}_1^2 + \bar{R}_0^2 + 4\bar{R}_1^2} \quad (4)$$

In the following sections we will consider laminates with identical plies, for which:

$$\hat{T}_0 = \hat{T}_1 = \hat{T} = 0 \quad (5)$$

According to Vannucci [4], a laminate is *decoupled* if the tensor norms B and V (pertaining, respectively to tensors \mathbf{B} and \mathbf{V}) are equal to zero: it is important to note that – for laminates with identical plies – the condition $\mathbf{B} = 0$ implies $\mathbf{V} = 0$, while the inverse is not true.

Vannucci [4], by using the polar method, established explicitly the conditions of maximum coupling, that can be read as follows:

- the thermoelastic coupling is maximum (max. V) when all plies belonging to each half of the stacking sequence, with respect to the middle plane, have the same orientation differing by an angle equal to $\pi/2$: this result is not influenced by the material properties,
- the conditions of maximum elastic coupling (max. B) are the same as for V only if $\rho = R_0/R_1 \leq 1$; on the contrary, max. B is reached with plates whose halves differ by an angle δ equal to:

$$\delta = \frac{1}{2} \arccos\left(-\frac{1}{\rho^2}\right) \quad (6)$$

This time, material properties have an important influence on the maximum coupling. In fact, for laminates with $\rho > 1$, B and V are not maximised by the same stacking sequence.

2.2 Maximum curvatures of $0_m/90_n$ plates

By re-writing the constitutive equation (3) using the polar formalism and by employing invariant quantities for the thermal forces and moments we obtain, for a laminate belonging to the $0_m/90_n$ family:

$$\begin{pmatrix} T_N \\ R_N \\ T_M \\ R_M \end{pmatrix} = \begin{pmatrix} 4\bar{T}_1 & 4\bar{R}_1 & 0 & 4\hat{R}_1 \\ 4\bar{R}_1 & 2(\bar{T}_0 + \bar{R}_0) & 4\hat{R}_1 & 0 \\ 0 & 4\hat{R}_1 & 4\tilde{T}_1 & 4\tilde{R}_1 \\ 4\hat{R}_1 & 0 & 4\tilde{R}_1 & 2(\tilde{T}_0 + \tilde{R}_0) \end{pmatrix} \begin{pmatrix} T_\varepsilon \\ R_\varepsilon \\ T_k \\ R_k \end{pmatrix} \quad (7)$$

$T_\varepsilon, R_\varepsilon, T_k, R_k$ can be determined by inverting equation (7) and curvatures k_{xx} and k_{yy} can be obtained by the following equations:

$$T_k = \frac{k_{xx} + k_{yy}}{2}, \quad R_k = \frac{k_{xx} - k_{yy}}{2} \quad (8)$$

It has to be noted that, for laminates belonging to the $0_m/90_n$ family under thermal solicitations the twisting curvature k_{xy} is equal to zero, because there are no shear and twisting thermal solicitations, respectively N_{xy}^{th} and M_{xy}^{th} to activate them.

The curvatures can be studied as functions of the adimensional thickness (with respect to the total thickness of the plate, e) of the 90° plies, e_{90} , and the value of e_{90} for which curvatures are maximum can be explicitly assessed by means of analytical expressions.

For instance, the maximum k_{xx} is given by a value of e_{90} which is solution of the following equation:

$$8R_1e_{90}^2 - 2(T_0 + 2T_1 + R_0 - 4R_1)e_{90} + (T_0 + 2T_1 + R_0 - 4R_1) = 0 \quad (9)$$

One of the solutions of equation (9) does not belong to the interval $[0,1]$ within which e_{90} is varying ; the other solution is the searched value, $e_{90\max}$: it has to be noted that solutions of equation (9) are always real, whatever the material properties.

For k_{yy} an analogous equation can be established. In fact, k_{yy} is maximum for a value of e_{90} which is the solution of the following equation:

$$8R_1e_{90}^2 + 2(T_0 + 2T_1 + R_0 - 4R_1)e_{90} - (T_0 + 2T_1 + R_0 - 4R_1) = 0 \quad (10)$$

Maximum curvatures (k_{xx} or k_{yy}) depend by *elastic* invariant properties of a ply: a very important role is played by the parameter R_1 which is an indicator of the anisotropy of the material. It is evident that for $R_1 = 0$ (elastic isotropy) the problem admits only one solution, that is,

$e_{90\max} = 0.5$: in other words, for such a material the maximum curvature of $0_m/90_n$ plates is reached for $m = n$.

Figure 1 presents the evolution of the adimensional curvatures (that is, multiplied by the total thickness of the plate), k_{xx} and k_{yy} , as functions of e_{90} : the simulations are performed for a carbon-epoxy composite material, which exhibits a marked anisotropic behaviour, and whose properties are presented in table 1.

For $e_{90} = 0.5$, k_{xx} and k_{yy} have the same magnitude and opposite sign. The maximum values of k_{xx} and k_{yy} are reached for values of e_{90} which are respectively equal to 0,81 and 0,19. These values are coincident with those determined by the analytical equations (9) and (10). It has to be noted that, for the considered material (for which $\rho < 1$), the conditions of *maximum coupling* established by Vannucci do not correspond to the conditions of *maximum curvatures*.

Figure 2 shows the effect of the parameter R_1 on the location of the maximum curvature. By increasing R_1 , that is, the level of elastic anisotropy of the material, the value of $e_{90\max}$ moves towards the external limits of the $[0,1]$ interval.

Moreover, we note that the thermoelastic properties of a ply, that is, the coefficients of thermal expansion, have no role on the location of

the maximum curvatures. On the other hand, the difference $\Delta\alpha = (\alpha_2 - \alpha_1)$, between the transverse and longitudinal thermal expansion coefficients, have a consistent influence on the magnitude of the maximum curvatures.

3 EXPERIMENTAL MEASURES

The curvatures of several composite plates, made by glass-epoxy Ec13/913 materials and with several values of thickness of the 90° plies, have been measured by using the experimental technique detailed in reference [1]; measurements have been compared to numerical predictions and results are presented in figure 3. The material properties of this material have been measured at several temperatures (see table 2) and predictions by the model have employed such values. Measures do not agree - qualitatively and quantitatively – with the predictions of the linear theory. However, they are in good agreement with a plate theory that takes into account geometrical nonlinearities [6]. On the other hand, the value of $e_{90\max}$ is not affected by geometrical nonlinearities and is in good agreement with the experimental measures.

Figure 3 shows the typical behaviour of this kind of plates; the deformed shapes are not saddle-like, as predicted by the linear theory, but cylindrical. Actually two cylindrical deformed shapes, the first one along the x direction and the other one along the y direction may exist: in fact, at

a given temperature, for the same total potential energy, the two cylindrical deformed shapes are both allowed to exist. The prevalence of one solution with respect to the other is dictated by imperfections: the range of existence of the two cylindrical solutions is clearly indicated in figure 3.

4 CONCLUSIONS

The behaviour of composite laminated plates belonging to the $0_m/90_n$ family under thermal loads has been studied with the aim of determining their maximum thermally induced curvatures. The classical plate lamination theory (a linear theory) and the polar method were employed. These methods allowed us to find explicitly the conditions of maximum curvature. In particular, the thickness of the 90° plies, e_{90} , for which curvatures are maximum were determined. The location of maximum curvature (i.e. e_{90MAX}) depends on the elastic properties of a ply while their magnitude is driven by the thermal expansion coefficients, that is, by the thermoelastic properties.

The existence of maximum curvatures has been experimentally proven through measures of curvatures of laminated plates made by glass-epoxy Ec13/913 composite materials. The location of maximum

curvatures is correctly predicted by the linear models; on the other hand, the magnitude of the measured curvatures agree with a model of plates which takes into account the effect of geometrical nonlinearities. This result is plausible, since these plates exhibit large displacements, even at small strain.

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Table 2 : Thermomechanical properties (at T_{amb}) of the glass-epoxy Ec13/913 composite material.

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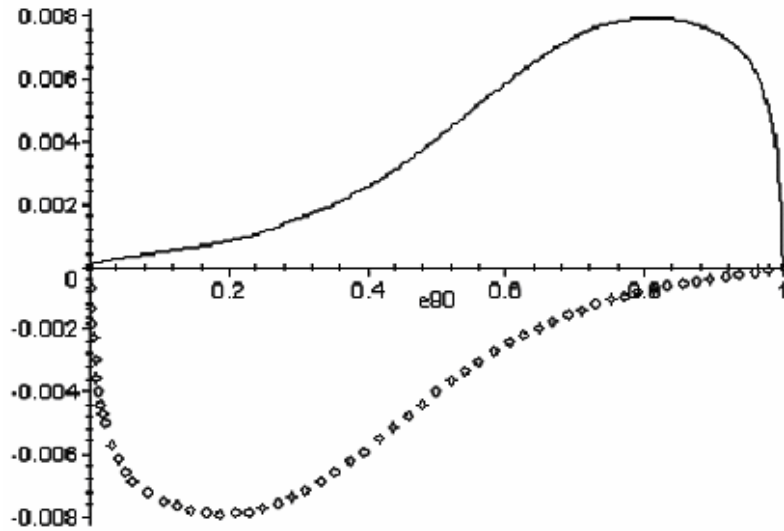


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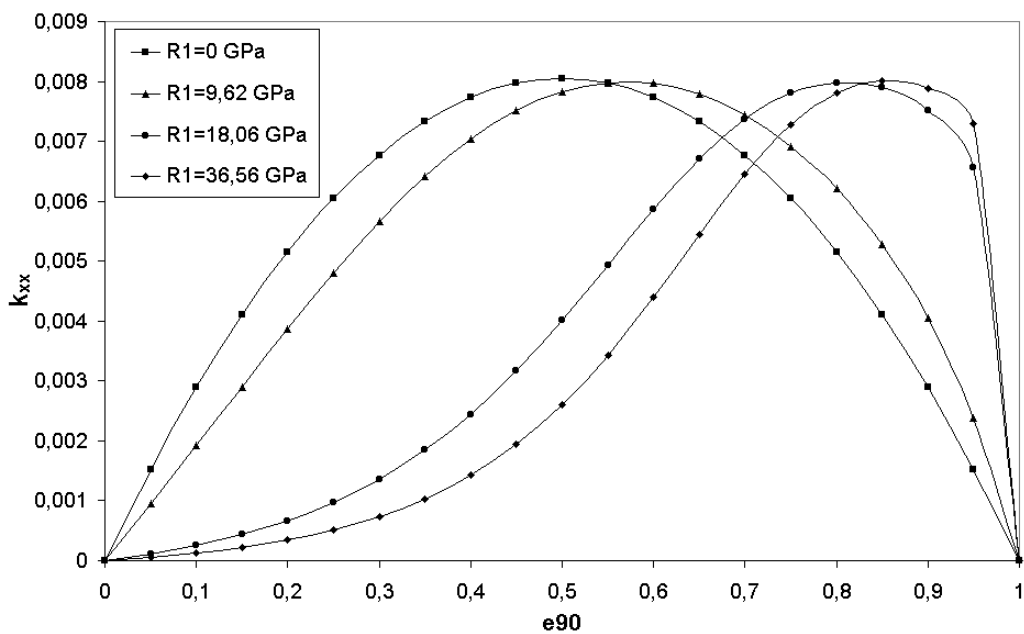


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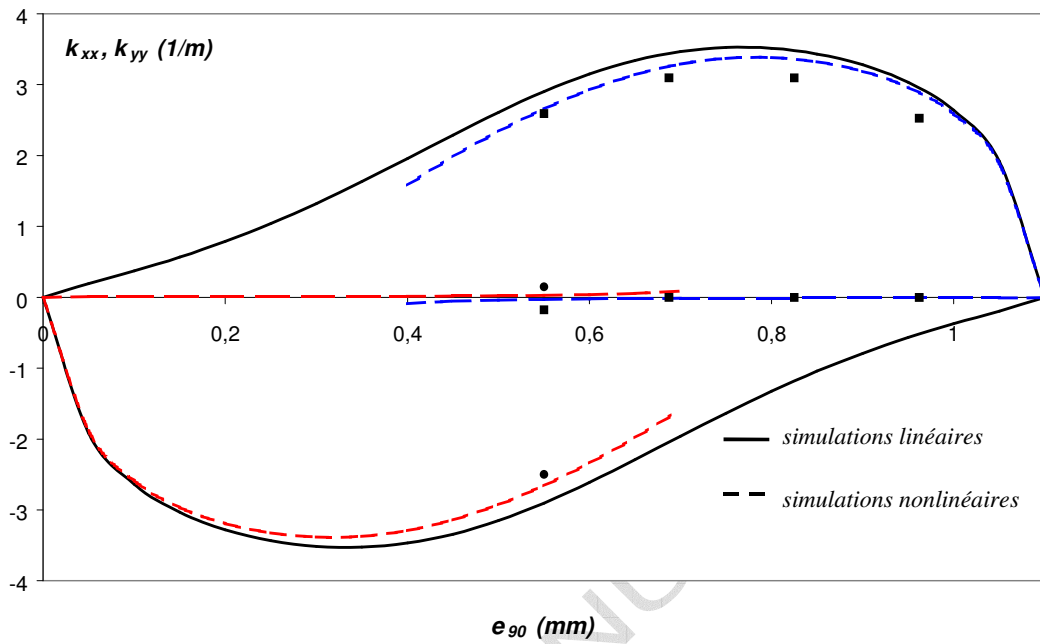


Figure 3: Comparison between model predictions and experimental measurements (Ec13/913 glass-epoxy material).

E_1 (GPa)	E_2 (GPa)	G_{12} (GPa)	ν_{12}	α_1 ($^{\circ}\text{C}^{-1}$)	α_2 ($^{\circ}\text{C}^{-1}$)
152	8.4	4.2	0.35	0.09 E-6	28.8 E-6
T_0	T_1	R_0	R_1	Φ_0	Φ_1
21.5	20.9	17.3	18	0	0

Table 1: Thermomechanical properties used in the simulations.

E_1 (GPa)	E_2 (GPa)	G_{12} (GPa)	ν_{12}	α_1 ($^{\circ}\text{C}^{-1}$)	α_2 ($^{\circ}\text{C}^{-1}$)
45.8	8.1	-	-	7.12 E-6	29.7 E-6
T_0	T_1	R_0	R_1	Φ_0	Φ_1
8.4	7.3	4.2	4.7	0	0

Table 2 : Thermomechanical properties (at T_{amb}) of the glass-epoxy Ec13/913 composite material.