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Effect of coarse particle volume fraction on the yield stress and thixotropy of cementitious materials

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Abstract

In order to help modelling the yield stress of fresh concrete, we study the behavior of suspensions of coarse particles in a thixotropic cement paste. Our aim is to relate the yield stress of these mixtures to the yield stress of the suspending cement paste, to the time passed at rest, and to the coarse particle volume fraction. We present here procedures that allow for (i) studying an homogeneous and isotropic suspension, (ii) comparing the yield stress of a given cement paste to that of the same cement paste added with particles, (iii) accounting for the thixotropy of the cement paste. We observe that the yield stress of these suspensions of cement paste with coarse particles follows the very simple Chateau-Ovarlez-Trung model [1], consistently with the experimental results of Mahaut *et al.* [2] obtained with many different particles and suspending yield stress fluids. This consistency between the results obtained in various yield stress fluids shows that the yield stress of the suspension does not depend on the physicochemical properties of the suspending yield stress fluid; it only

depends on its yield stress value. This shows that studies of suspensions in model yield stress fluids can be used as a general tool to infer the behavior of fresh concrete. Moreover, we show that the thixotropic structuration rate of the interstitial paste (its static yield stress increase rate in time) is not affected by the presence of the particles. As a consequence, it is sufficient to measure the thixotropic properties of the constitutive cement paste in order to predict the thixotropic structuration rate of a given fresh concrete. This structuration rate is predicted to have the same dependence on the coarse particle volume fraction as the yield stress.

Key words: A. Fresh Concrete, A. Rheology, D. Aggregate, D. Cement Paste, E. Modeling

1 Introduction

2 Knowing and predicting the flow properties of fresh concrete is a major issue of
3 concrete casting and concrete mix-design. Basically, fresh concretes exhibit a
4 yield stress [3] and have a solid viscoelastic behavior below this yield stress [4];
5 above the yield stress they behave as liquids, and their steady flow behavior
6 is usually well represented by a Bingham or a Herschel-Bulkley model [3,5].
7 However, fresh concrete is also known for its evolving rheological behavior.
8 Even, if its steady state flow may be described by the above models, the
9 characteristic time to reach this steady state flow may be rather long [6–9] and,
10 after a long time of rest, the stress that has to be applied to induce a flow may
11 be one or two orders higher than the dynamic yield stress measured when the

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12 material stops flowing i.e. it is thixotropic [10–12]. The static yield stress and
13 its increase rate at rest are actually the most important rheological quantities
14 in terms of potential applications in the case of SCC [13]: it has been shown
15 recently that they determine the formwork pressure [9,14–17], the stability
16 vs. sedimentation of the coarsest particles in SCC [18] and the occurrence
17 of distinct layer casting [19]. As a consequence it is of high importance to
18 understand the role of the various components of a given concrete on this yield
19 stress and its evolution at rest. Moreover, measuring directly the rheological
20 properties of fresh concrete is very difficult [20]; any model providing the yield
21 stress of concrete as a function of the suspending cement paste properties and
22 the properties and the volume fraction of sand and aggregates would then
23 prove to be very useful.

24 The link between concrete mix-design and its flow properties in the fresh state
25 may be studied in the more general framework of suspensions rheophysics
26 [12]. Actually, fresh concretes belong to the wide family of dense suspensions,
27 which often involve a broad range of particle sizes [21] and can be found in
28 many industrial processes (drilling muds, foodstuff transport...) and natural
29 phenomena (debris-flows, lava flows...). All these materials share the same
30 complex features, which originate from the great variety of interactions be-
31 tween the particles (colloidal, hydrodynamic, frictional, collisional...) and of
32 physical properties of the particles (volume fraction, sensitivity to thermal
33 agitation, shape...) affecting the material behavior [22,12]. Basically, in the
34 absence of a contact network of noncolloidal particles (i.e. for moderate non-
35 colloidal particles volume fraction), the yielding behavior originates from the
36 colloidal interactions which create a jammed network of interacting particles
37 [5,12]. Structuration at rest (which has nothing to do with setting) is observed

38 in many aggregating suspensions and colloidal glasses [12]: the evolution of the
39 behavior of aggregating suspensions at rest may be explained by a progres-
40 sive and reversible formation of a solid structure by flocculation. Within this
41 frame, the problem of the influence of coarse particles on the behavior of fresh
42 concrete may be seen more generally as the problem of the influence of non-
43 colloidal particles on the properties of yield stress fluids. It is thus of high
44 importance to clarify the cases where the rheological properties of a suspen-
45 sion of coarse particles in a yield stress fluid depend only on the rheological
46 properties of the suspending fluid and on the coarse particle volume fraction
47 and size distribution. This should provide results applicable to any particles
48 in any yield stress fluid, in particular to sand and aggregates suspended in a
49 cement paste. It would allow the use of results obtained in studies performed
50 e.g. with noncolloidal particles in clay dispersions to predict the behavior of a
51 mortar or a concrete. On the other hand, any departure from generic results
52 would be the result of specific physicochemical interactions in the suspensions
53 (or specific slippage at the paste/particle interface), as e.g. the adsorption of
54 a fraction of the superplasticizer of the cement paste on the fine aggregates
55 in SCC [23], and would justify for each material a specific study with the
56 particular particles and particular paste involved. In this paper, we test the
57 idea of fresh concrete being a suspension of particles in a yield stress fluid. We
58 compare the results obtained when suspending particles in a cement paste to
59 those recently obtained in a broad range of materials (suspensions of various
60 particles in various yield stress fluids) by Mahaut *et al.* [2].

61 The influence of the aggregates on the rheological properties of fresh concrete
62 has been studied theoretically and experimentally by de Larrard [24], de Lar-
63 rard and Sedran [25], Geiker *et al.* [26], Erdogan [27] and Toutou and Roussel

64 [28]. De Larrard [24] has proposed a model in which concrete is looked as
65 a granular mix in a water suspension. Then, the overall yield stress is the
66 macroscopic counterpart of the friction between solid particles and is inter-
67 preted as the stress one needs to apply in order to overcome the intergranular
68 contact forces. The overall yield stress can be estimated from the value of the
69 solid volume fraction and close packing density of the different components
70 of the granular mixture. However, if this model may help understanding the
71 properties of fresh concrete displaying “ordinary” rheology, it is unadapted to
72 the description of modern fluid concrete which contains less coarse particles
73 and where friction between the grains is negligible [29]. Geiker *et al.* [26] have
74 studied experimentally the effect of coarse particle volume fraction on the rhe-
75 ological properties of SCC. They have measured the steady-state flow curves of
76 various materials thanks to the procedure developed in [8]; the dynamic yield
77 stress was then extracted from a fit of the flow curve with a Bingham model.
78 It was found to increase strongly with the coarse particle volume fraction.
79 To model the behavior, they assume that the effect of aggregates on concrete
80 rheological properties can be studied by looking to concrete as a suspension of
81 coarse particles in the mortar seen as a continuum medium. Their experimen-
82 tal data are compared to a model proposed by Nielsen [30] which provides the
83 yield stress of a suspension of ellipsoids as a function of the volume fraction
84 of particles and of the aspect ratio. This model rests on heuristic rules which
85 are not rigorously justified. Nevertheless, the theory can be calibrated in order
86 to accurately describe the data of Geiker *et al.* [26]. Erdogan [27] have stud-
87 ied the effect of aggregate particle shape and surface texture on rheological
88 properties of fresh concrete. Artificial aggregate particles of regular geometric
89 shapes (spheres, cubes and rectangular prisms) with similar centimeter size
90 and volume were prepared. A Couette-vane rheometer (ICAR) was used to

91 measure the dynamic yield stress as the low shear rate limit of a flow curve.
92 In addition, slump tests were performed. Erdogan has observed that the yield
93 stress increases slightly when the coarse particle volume fraction increases.
94 This trend is confirmed by slump experiments: the slump value was clearly a
95 decreasing function of the coarse particle content, whatever the shape of the
96 particles is. Toutou and Roussel [28] have studied the flow behavior of mortars,
97 considered as suspensions of sand in a cement paste, and the flow behavior of
98 concretes, considered as suspensions of gravel in a mortar. In both cases, the
99 influence of the coarsest inclusions volume fraction on the suspending paste
100 properties was investigated. The dynamic yield stress was extrapolated from
101 the measured flow-curves. The yield stress of the mortar was found to increase
102 with the sand volume fraction. However, at low volume fraction (below 20%)
103 yield stresses of mortars were found to be lower than the yield stress of the
104 suspending cement paste. Toutou and Roussel [28] attributed this feature to
105 the increased deflocculation of the cement paste due to the presence of the
106 inclusions during mixing of the suspension, in agreement with Williams *et al.*
107 [31]. The yield stress of concrete was also found to increase with the gravel
108 volume fraction. However, Toutou and Roussel [28] found that adding gravel
109 at a given volume fraction to a mortar yields a much larger increase of the
110 yield stress than adding sand at the same volume fraction to a cement paste.

111 The influence of coarse particles on the rheological properties of other yield
112 stress fluids has been studied by Coussot [32] and Ancey and Jorrot [33]. An-
113 ceay and Jorrot [33] have suspended coarse particles within a clay dispersion.
114 They measured the yield stress of the suspension by means of a slump test.
115 They showed that for well-graded particles, the suspension yield stress does not
116 depend on the particle characteristics (diameter, material) and that the yield

117 stress diverges when the solid volume fraction value tends toward the maxi-
118 mum packing fraction. Of course, when the coarse particles are polydisperse,
119 the value of the maximum packing fraction depends on the size distribution of
120 the particles, and the yield stress diverges for values of the solid volume frac-
121 tion depending on this distribution. They observed sometimes that, for low
122 reduced solid volume fraction, the yield stress can be a decreasing function of
123 the solid volume fraction of the coarse particle. This effect was ascribed to a
124 depletion phenomena: the clay particles are supposed to be expelled from the
125 suspending fluid in the neighborhood of the coarse particles which are then
126 embedded in a shell of pure water. Then, they cannot contribute to the over-
127 all yield stress: they behave as voids. Note that this depletion mechanism is
128 specific to the suspending yield stress fluid studied by Ancy and Jorrot; thus,
129 it cannot be used to predict what happens when the particles are suspended
130 in another yield stress fluid.

131 The few existing experimental studies provide very different results; e.g., when
132 particles having the same shape (spheres) are embedded at a volume fraction
133 ϕ corresponding to 70% of the maximum packing fraction ϕ_m in a paste,
134 Geiker *et al.* [26] find that the yield stress of the paste is increased by a factor
135 50 when the paste is a mortar, whereas Erdogan [27] finds that it is increased
136 by only a factor 1.3 when the paste is also a mortar, and Ancy and Jorrot [33]
137 find that, when the paste is a clay dispersion, the yield stress is increased by a
138 factor 2. Other surprising discrepancies are shown by Toutou and Roussel [28]:
139 they find that for sand suspended at 70% of ϕ_m in a cement paste the yield
140 stress is increased by a factor 8 whereas for gravel (of comparable shape and
141 dispersity) suspended at 70% of ϕ_m in a mortar, it is increased by a factor 25.
142 As pointed out above, if rigid noncolloidal particles of a given shape and dis-

143 persity were to interact only rheologically with the suspending paste, we would
144 expect all the results to be roughly consistent as they should not depend on the
145 paste physicochemical nature. However, the discrepancy between the results
146 of Geiker *et al.* [26], Erdogan [27], and Ancey and Jorrot[33], and between the
147 mortar and the concrete case in the work of Toutou and Roussel [28], does not
148 necessarily imply that there are specific physicochemical interactions between
149 the different particles and the different pastes involved in these studies, and
150 that we would fail describing these materials as suspensions of rigid particles
151 in yield stress fluids. Such discrepancy may indeed find its origin in differences
152 and shortcomings in the experimental procedures used. Actually, the experi-
153 ments of Geiker *et al.* [26], Erdogan [27] and Toutou and Roussel [28] involve
154 a flow of the material. It is then well known that shear-induced migration
155 of particles towards low shear zones (the external cylinder in coaxial cylin-
156 ders geometries) is likely to occur [34–36], whatever the care that is taken;
157 this would cause the material to be heterogeneous inside the measurement
158 cell, and the measurement to be non-representative of the homogeneous mate-
159 rial. This is particularly true at high concentrations (above 50% for spherical
160 monodisperse particles) where it has been shown by Ovarlez *et al.* [36] that
161 radial migration occurs as an almost instantaneous and unavoidable process in
162 a Couette geometry. In this case, all the measurements performed in time are
163 likely to be performed on the same stationary heterogeneous structure: testing
164 the material at the same rotational velocity at two different times [8] may then
165 wrongly lead to conclude that there is no shear-induced migration while the
166 only correct conclusion is that the structure is stationary. Moreover, Geiker *et*
167 *al.* [26], Erdogan [27] and Toutou and Roussel [28] use a Herschel-Bulkley (or
168 Bingham) fit of the flow curve to extrapolate the value of the yield stress
169 instead of a direct measurement. Chateau *et al.* [1] have shown that such

170 an extrapolation generally provides an overestimation of the yield stress of
171 the suspension, and that this overestimation is more dramatic as the particle
172 concentration increases. The reason is that the suspension departs from the
173 Herschel-Bulkley (or Bingham) model at very low shear rate (unaccessible to
174 most concrete rheometers) and has a lower yield stress than the one extrap-
175 olated from the measurable flow curve [1]. On the other hand, as the strain
176 involved in this test is small, there should be no migration, nor extrapolation
177 problems, in the slump test used by Ancey and Jorrot [33], as long as the yield
178 stress is high enough to avoid spreading of the material and the correlation
179 between measured slump and yield stress is suitable to their experiments [37].
180 Another difference between the procedures is that the particle distribution
181 after a flow is anisotropic [38–40], whereas the particle distribution is hardly
182 changed by the slump flow and is thus isotropic in the experiments of An-
183 cey and Jorrot [33]; as a consequence, the results of Ancey and Jorrot [33] are
184 not related to the same state of the suspension as the one of Erdogan [27] and
185 Geiker *et al.* [26]. Finally, note that Ancey and Jorrot [33] and Toutou and
186 Roussel [28] found in some cases that the suspension yield stress can be lower
187 than the suspending paste yield stress; as pointed out by Chateau *et al.* [1],
188 this should not occur if the noncolloidal particles interact only mechanically
189 with the paste, i.e. these results are likely to apply only to their systems.

190 Finally, it is therefore of high importance to clarify the cases where suspen-
191 sions can actually be considered as particles in a yield stress fluid, i.e. the cases
192 where the rheological properties of the suspension depend only on the rheo-
193 logical properties of the suspending fluid and on the coarse particle volume
194 fraction, shape and size distribution. With the aim of providing such generic
195 results, Mahaut *et al.* [2] have recently performed an experimental study on

196 a broad range of materials. They have suspended beads of various sizes and
 197 made of various materials in very different pastes whose common point is to
 198 exhibit a yield stress, and they sought consistency between the results. More-
 199 over, they had a careful look at all the steps of the measurement procedure to
 200 ensure that an homogeneous and isotropic material is studied in all cases. They
 201 showed that the dimensionless elastic modulus $G'(\phi)/G'(0)$ and the dimension-
 202 less yield stress $\tau_c(\phi)/\tau_c(0)$ of such monodisperse suspensions depend on the
 203 bead volume fraction ϕ only (as expected for systems free from specific physico-
 204 chemical interactions or specific slippage at the paste/particle interface). They
 205 found that the elastic modulus/concentration relationship is well fitted to a
 206 Krieger-Dougherty model $(1 - \phi/\phi_m)^{-2.5\phi_m}$ with $\phi_m = 0.57$ for monodisperse
 207 isotropic suspensions. They showed that the yield stress/concentration rela-
 208 tionship is related to the elastic modulus/concentration relationship through
 209 a very simple law $\tau_c(\phi)/\tau_c(0) = \sqrt{(1 - \phi)G'(\phi)/G'(0)}$ in agreement with the
 210 micromechanical analysis of Chateau *et al.* [1], yielding the Chateau-Ovarlez-
 211 Trung model $\tau_c(\phi)/\tau_c(0) = \sqrt{(1 - \phi)(1 - \phi/\phi_m)^{-2.5\phi_m}}$ for the yield stress of
 212 suspensions of monodisperse beads in a yield stress fluid.

213 In this paper, we study suspensions of coarse spherical particles in a thixotropic
 214 cement paste. We measure the static yield stress of the suspensions as a func-
 215 tion of the resting time and of the particle volume fraction. We design new
 216 procedures that allow for comparing the yield stress of a given cement paste
 217 to that of the same cement paste added with particles. We also take care of
 218 designing a procedure that allows for properly accounting for thixotropy of
 219 the paste, independently of any irreversible change in the paste behaviour. In
 220 Sec. 2, we present the materials and the experimental setup. In Sec. 3, we
 221 present the procedure we developed to ensure comparing properly the yield

222 stress of the suspensions to the yield stress of the suspending cement paste, as
223 a function of the resting time. We present the results in Sec. 4 and compare
224 the yield stress obtained with particles suspended in a cement paste with this
225 procedure to the ones obtained on model materials by Mahaut *et al.* [2], and
226 to the Chateau-Ovarlez-Trung model [1].

227 **2 Materials and methods**

228 *2.1 Pastes and particles*

229 We performed our experiments with a thixotropic cement paste. White Ce-
230 ment CEM I/52.5 N CE CP2 NF “SB” from Gargenville Calcia was used
231 to prepare all the cement pastes. Its specific gravity is 3.01. Its compressive
232 strength is 62 MPa at 28 days according to NF EN 196-1 test. The size dis-
233 tribution was measured in water using a laser granulometer (according to NF
234 ISO 13320-1 test) for different amount of superplasticizer and is given in Fig. 1.
235 The specific area determined using a BLAINE permeameter, according to NF
236 EN 196-6 test, is 4117 cm²/g. The cement chemical constituents are summa-
237 rized in Tab. 1. The Water to Cement ratio W/C studied here was 0.35. A
238 Superplasticizer (Glenium 27) and a nanosilica slurry (Rhoimat CS 60 SL,
239 Rhodia) were added to the mixture with a Superplasticizer to cement mass
240 ratio of 1% and a nanosilica slurry to cement mass ratio of 2%. The fluids
241 (water + superplasticizer + nanosilica) were first mixed together to obtain an
242 homogeneous suspension, and then added to the cement powder before a 5
243 minutes mixing phase in a planetary Controlab mixer: the velocity was first
244 set to 140rpm during 2min, and then to 285rpm during 3min. All the exper-

245 iments were performed on the fresh cement paste, less than 75min since the
246 constituents were mixed together. Before any measurement, the cement paste
247 was presheared again in the mixer at 285rpm during 2min in order to always
248 start the experiments on a paste in an initially destructured state.

249 The particles suspended in the cement paste are spherical monodisperse glass
250 beads of 2 mm diameter. This ensures that the particle size is much larger
251 than the paste microstructure, so that the particles may “see” the cement
252 paste as a continuum medium.

253 We chose to compare the results obtained with the suspensions of particles in
254 a cement paste to the one obtained by Mahaut *et al* [2] where particles are
255 suspended in various other yield stress fluids: emulsions, colloidal suspensions,
256 and a physical gel (see Mahaut *et al.* [2] for details on the preparation of these
257 materials). The emulsions are water in oil emulsions, in which the origin of
258 the yield stress is the surface tension between the droplets [5]. The colloidal
259 suspensions are bentonite suspensions, made of clay particles of length of or-
260 der $1\mu\text{m}$ and thickness 10nm. The yield stress then originates from colloidal
261 interactions between the particles. The physical gel is a Carbopol dispersion.
262 Basically, the polymers arrange in roughly spherical blobs which are squeezed
263 together [41,42]; this yields a yield stress. The particles used in the Mahaut *et*
264 *al.* study are spherical monodisperse beads. They are either polystyrene beads
265 of density 1.05, or glass beads of density 2.5., of various particle diameters: 80,
266 140, $315\mu\text{m}$ in the case of the polystyrene beads, and 140, 330 and $2000\mu\text{m}$
267 in the case of the glass beads. The beads are washed in an ultrasound bath
268 during 30 minutes and then dried. This is particularly important for experi-
269 ments performed in Carbopol gels: when the unwashed beads are embedded
270 into a Carbopol gel, it actually results in a lower yield stress than when the

271 washed beads are suspended, indicating residual surface effects [2]; such resid-
272 ual surface effects may be due to colloidal impurities at the particle surface
273 (or residual surfactant at the particle surface when polystyrene particles are
274 used [2]). A single washing is enough to ensure a reproducible state. All ma-
275 terials were prepared (i) to ensure that the particle size is much larger than
276 the paste microstructure size, (ii) to check that the results depend only on
277 the mechanical properties of the paste i.e. that they are independent of the
278 physicochemical origin of the yield stress, (iii) to check that the results are
279 independent of the noncolloidal particles size (when the particles are monodis-
280 perse and have constant shape and surface texture), (iv) to check that there
281 are neither particle/particle nor particle/paste physicochemical interactions.
282 Moreover, by varying the suspending paste yield stress, it was checked that the
283 dimensionless yield stress depends only on the particle volume fraction (when
284 the particle are monodisperse). If we obtain the same behavior with suspen-
285 sions prepared with all materials, including the cement pastes, and whatever
286 the particle size, this ensures that there is no contribution from specific parti-
287 cles/material physicochemical interactions and that the results we obtain can
288 be applied to the case of any other particles in any other yield stress fluid (in
289 particular to any cement paste formulation).

290 The insertion of air is unavoidable. The effect of air on the yield stress is not
291 negligible [2], it should thus be checked that its content is negligible: it changes
292 not only the continuous phase mechanical properties [5] but also the effective
293 bead volume fraction, which is a sensitive parameter at high volume fractions.
294 However, methods such as centrifugation to remove the bubbles cannot be used
295 if we want to ensure that the materials remain homogeneous as explained in
296 Sec. 3. We thus chose to work with a constant volume of material in order to

297 check that the air content is always lower than 1%.

298 All the measurements we present in this paper were performed on suspensions
299 of coarse particles embedded in pastes at a volume fraction ϕ ranging between
300 0 and 55%, with an air content lower than 1%.

301 *2.2 Rheological tools*

302 Most rheometric experiments are performed within a vane in cup geometry
303 (inner radius $R_i = 22.5\text{mm}$, outer cylinder radius $R_e = 45\text{mm}$, height $H =$
304 45mm) on a commercial rheometer (Bohlin C-VOR 200) that imposes either
305 the torque or the rotational velocity (with a torque feedback). In order to
306 avoid wall slip [43,12], we use a six-blade vane as an inner tool, and we glue
307 sandpaper on the outer cylinder wall. For the small particles in model yield
308 stress fluids, we use another six-blade vane in cup geometry (inner radius
309 $R_i = 12.5\text{mm}$, outer cylinder radius $R_e = 18\text{mm}$, height $H = 45\text{mm}$). Working
310 within these wide-gap geometries allows for studying easily coarse particles
311 and to ensure that, for all the materials studied, there are enough particles in
312 the gap to consider that we measure the properties of a continuum medium
313 (the suspension).

314 We measure the yield stress $\tau_c(\phi)$ of the paste as a function of the volume
315 fraction ϕ of coarse particles embedded in the pastes. In a wide gap geometry,
316 the shear stress τ continuously decreases within the gap: the shear stress at
317 a radius R is $\tau(R) = \frac{T}{2\pi HR^2}$. Therefore, one has to choose a definition of
318 the shear stress that is measured in a given rheological experiment. Here,
319 we want to perform yield stress measurements; whatever the measurement

320 method we choose, yield first occurs where the stress is maximal i.e. along the
321 inner virtual cylinder. As consequence, we define the shear stress measurement
322 as $\tau(R_i) = \frac{T}{2\pi HR_i^2}$, so that the yield stress τ_c is correctly measured (any other
323 definition of the shear stress would provide an underestimation of the yield
324 stress). Anyway, we will focus on the evolution of the dimensionless yield stress
325 $\tau_c(\phi)/\tau_c(0)$ with the bead volume fraction ϕ , which should be independent of
326 the definition of τ .

327 **3 Experimental procedure**

328 In this section, we present the procedure aiming at showing the influence
329 of the inclusion of coarse particles on the yield stress of cement pastes. We
330 first show that the choice of the sample preparation and of the yield stress
331 measurement procedure is critical to know how the particles are distributed in
332 the suspension. We then establish a new procedure to ensure a good knowledge
333 of the interstitial paste properties in the suspension.

334 *3.1 Preparation and yield stress measurement*

335 First, we need to define precisely the state of the materials we want study.
336 Three points are actually important: (i) we want to perform our yield stress
337 measurement on a homogeneous suspension, otherwise the measurement would
338 have no meaning, (ii) we want to control the microstructure of the suspen-
339 sions (i.e. the distribution of the neighbors of the coarse particles) to ensure
340 that all measurements deal with the same state of the suspension, and can
341 be compared and modelled, (iii) we need the interstitial cement paste to be

342 initially destructured in order to study thixotropy.

343 These three points impose severe restrictions about the preparation and yield
344 stress measurement procedures, as shown by Mahaut *et al.* [2]. They showed
345 that measurements involving an important flow of the material (a large strain)
346 pose several problems. First, a flow causes particle migration towards the low
347 shear zones (the outer cylinder in coaxial cylinder geometries) i.e. creation of
348 a heterogeneous structure. This migration phenomenon is well documented
349 for suspensions of noncolloidal particles in Newtonian fluids [34–36] but is
350 still badly known in yield stress fluids. As it needs a large strain to occur
351 for moderate volume fraction [34,35], it may be avoided in these cases by
352 performing only short duration experiments. However, for volume fractions
353 of the order of 50% and more, migration is a critical phenomenon: it seems
354 unavoidable as it is almost instantaneous as shown by Ovarlez *et al.* [36].
355 Another problem when suspensions flow is that an anisotropic microstructure
356 of the particles is created by the flow, as observed in suspensions of particles
357 in Newtonian fluids [38–40]. It is also a critical phenomenon: Mahaut *et al.* [2]
358 showed that suspensions of isotropic and anisotropic microstructure have very
359 different rheological properties.

360 These problems imply that we cannot preshear our materials with the rheome-
361 ter and that we cannot use a yield stress measurement method based on a shear
362 flow such as shear rate [8] or shear stress ramps [44] and creep tests [45]; we
363 then have to measure the static yield stress. On the other hand, as the static
364 yield stress of thixotropic materials depends on the time passed at rest in
365 the solid state [46], the measurements have to be performed on a well defined
366 state of the paste, i.e. the material needs to be first strongly presheared to get
367 a destructured initial state. However, as pointed out above, we cannot apply

368 a controlled preshear with the rheometer to the system after its preparation.
369 That is why, before loading the material in the measurement cup, we first pres-
370 sheared the cement paste alone during 2 minutes with the mixer at 285rpm;
371 this ensures that the cement paste is initially in a destructured state. Then,
372 the particles and the paste are mixed together in the measurement cylinder,
373 and the loaded suspension is strongly stirred by hand in random directions to
374 disperse the particles; this random stirring should ensure keeping the material
375 in a destructured state while avoiding particle migration and anisotropy. Af-
376 terwards, the vane tool is inserted in the cup, and we perform our yield stress
377 measurement after a given resting time with the vane method [47,48]: a small
378 rotational velocity, corresponding to a shear rate of 0.01s^{-1} is imposed to the
379 vane tool. Note that we checked that we observe the same effect of the parti-
380 cles on the yield stress whatever the low velocity that is chosen to drive the
381 vane tool. Fig. 2 shows the shear stress vs. strain for yield stress measurement
382 experiments performed in a cement paste. There is an overshoot, followed by
383 a slow decrease of the shear stress: the peak defines the static yield stress, the
384 decrease corresponds to destructuration of the material under the shear flow;
385 the suspension structure at yield should then be isotropic and homogeneous.
386 Then, any new yield stress measurement requires a new sample preparation
387 or a new random manual preshear in the cup: it has been shown by Mahaut *et*
388 *al.* [2] that the small strain of order 1 induced by the whole measurement
389 procedure is sufficient to change the material state (it is sufficient to change
390 the suspension microstructure or to induce migration): the suspension states
391 before and after the yield stress measurements are characterized by different
392 rheological properties.

394 As we are interested in the influence of the particles on the yield stress of
395 cement pastes, we will need to compare the suspension yield stress and the
396 cement paste yield stress. It is thus important to ensure that we have a good
397 knowledge of the properties of the interstitial paste state in the suspension.
398 The procedure developed to ensure this measurement is presented in detail in
399 the Appendix A. We present here the main steps.

400 First, we have to note that it is very difficult to achieve a good reproducibility
401 of a cement paste mechanical behavior (see Appendix A). That is why we
402 chose to work on the same batch for the measurement of the properties of the
403 paste alone and for the suspension.

404 Then, for a given cement paste batch, we observe that yield stress measure-
405 ments performed in the same conditions as regards thixotropic effects (i.e. for
406 a 2 minutes resting time after a strong stirring of the paste) provide values
407 that depend on the time t_{age} elapsed since the constituents of the cement paste
408 were mixed together (Appendix A). This means that one cannot know what
409 is the yield stress of the interstitial paste in a suspension if the yield stress of
410 the cement paste alone is not measured at exactly the same time after mixing
411 as the yield stress of the suspension. That is why we chose to measure simul-
412 taneously the yield stress of the suspension and the yield stress of the cement
413 paste alone in exactly the same conditions (same age t_{age} after mixing the
414 constituents of the cement paste, same time t_{rest} after the end of the strong
415 stirring), with the help of 2 rheometers that perform their measurements in
416 parallel.

417 We have also shown that when the same suspension sample, after a first resting
418 period and a first measurement, is stirred again in the measurement cup,
419 its interstitial cement paste is not in the same state of destructurement as
420 the cement paste alone stirred with the same procedure (Appendix A). This
421 means that the suspension and the cement paste cannot be compared anymore.
422 A solution to this problem is to perform only a single measurement on a
423 suspension, for a given resting time after its preparation.

424 A key point of the comparison between the suspension and the cement paste
425 is actually that the cement paste is initially strongly presheared in the mixer
426 for both samples: this defines an initial destructured state of the paste that is
427 the same both for the interstitial cement paste and for the cement paste alone.
428 After this preshear, the cement paste is loaded alone in one measurement cup,
429 and with the particles in another cup. Both samples are then strongly stirred
430 by hand during 30s in random directions: this ensures an homogeneous dis-
431 persion of the particles in the suspension, while keeping the cement paste in
432 a destructured state in both samples. Then, the stirring is stopped simultane-
433 ously for both samples: this defines the beginning of the resting period. With
434 this procedure, we have shown that the paste alone and the interstitial paste
435 have the same history and thus the same behavior (see Appendix A).

436 Finally, as the cement paste is thixotropic, its static yield stress increases as
437 a function of the time t_{rest} elapsed since the end of the stirring. However,
438 we showed that the yield stress value also depends on the time t_{age} elapsed
439 since the constituents were mixed together, even at short times. This would
440 mean that a characterization of thixotropy would only have a meaning for this
441 age t_{age} , and it would make the study of the impact of the coarse particles
442 on this thixotropy difficult. Nevertheless, we have shown that the irreversible

443 phenomena can be separated from the reversible phenomena. The thixotropic
444 (reversible) increase of the yield stress is actually the same whatever the paste
445 age t_{age} : it depends only on the time t_{rest} elapsed since the end of a preshear
446 (Appendix A). The increase of the yield stress of our cement paste due to
447 thixotropy is basically linear in t_{rest} : it reads $\tau_c(t_{rest}) = A_{thix} t_{rest}$ with an
448 increase rate $A_{thix} = 12\text{Pa}/\text{min}$.

449 3.3 Summary

450 As a summary we present in Fig. 3 a sketch of the whole procedure used to
451 study the influence of coarse particles on the yield stress of cement pastes.

452 This procedure ensures (i) that an homogeneous material is studied; (ii) that
453 we study a well defined state of the material: we chose to study the case of
454 isotropic distributions of particles; (iii) that the interstitial cement paste is well
455 characterized; (iv) that the initial destructured state of the interstitial cement
456 paste is well defined; (v) that thixotropy is accounted for and separated from
457 irreversible phenomena; (vi) that the results obtained with cement pastes can
458 be compared to measurements performed in other yield stress fluid.

459 4 Experimental results

460 In this section, we summarize the results of the yield stress measurements per-
461 formed on the suspensions with the procedure presented above. We compare
462 the results obtained with the cement pastes to the results obtained by Mahaut
463 *et al.* [2] with various yield stress fluids, and to the Chateau-Ovarlez-Trung
464 model [1].

466 In Fig. 4 we plot the dimensionless yield stress $\tau_c(\phi)/\tau_c(0)$ vs. the volume
 467 fraction ϕ of coarse particles embedded in the cement paste, when the yield
 468 stresses are measured with the procedure developed in Sec. 3 for various times
 469 t_{rest} after the end of a strong stirring.

470 We first observe that the yield stress increases when the coarse particle volume
 471 fraction is increased. This increase is quite limited for volume fraction lower
 472 than 45%: in this case, the yield stress is increased by a factor less than 3.
 473 However, the yield stress is found to increase sharply at the approach of a
 474 60% volume fraction. E.g., the yield stress of a suspension of 55% particles is
 475 20 times higher than the yield stress of the interstitial cement paste.

476 We also observe in Fig. 4 that the same evolution of the yield stress with the
 477 particle volume fraction is found whatever the time t_{rest} passed at rest before
 478 the measurement. This means that the yield stress of suspensions of coarse
 479 particles embedded at a volume fraction ϕ in a thixotropic cement paste of
 480 time-dependent yield stress $\tau_c(0, t)$ reads

$$\tau_c(\phi, t) = \tau_c(0, t)g(\phi) \quad (1)$$

481 This feature is expected if the coarse (i.e. noncolloidal) particles have only a
 482 mechanical interaction with the cement paste [2]: in this case, they should not
 483 interfere with the physical process at the origin of thixotropy. Then, at time
 484 t the interstitial paste has naturally the same yield stress $\tau_c(0, t)$ as if it had
 485 not been in contact with the coarse particles. Finally, as the relative increase

486 of the yield stress due to the monodisperse particles should be a function
 487 of their volume fraction ϕ only, independently of the value of the interstitial
 488 fluid yield stress, the yield stress of the suspension at time t is expected to be
 489 equal to $\tau_c(0, t)$ multiplied by some function $g(\phi)$ whatever $\tau_c(0, t)$, as observed
 490 experimentally.

491 Eq. 1 has an interesting consequence: it means that it is sufficient to know
 492 how the interstitial cement paste evolves in time to predict the suspension
 493 evolution at rest. This is important for fresh concrete as their behavior is
 494 hard to measure: our results show that the knowledge of the cement paste
 495 structuration rate at rest is sufficient to predict the fresh concrete structuration
 496 rate. As found on the cement paste we studied (see Sec. 3.2) the yield stress
 497 evolution at rest after a preshear of a cement paste usually reads [19]:

$$\tau_c(0, t) = \tau_c(0) + A_{thix}t \quad (2)$$

498 where A_{thix} is the structuration rate of the paste. In this case, Eq. 1 reads:

$$\tau_c(\phi, t) = \tau_c(0)g(\phi) + A_{thix}g(\phi)t \quad (3)$$

499 As a consequence, if the mechanical impact of the coarse particles is to increase
 500 the yield stress by a factor $g(\phi)$, then their impact on the structuration rate of
 501 the paste is to increase it also by a factor $g(\phi)$. It is thus sufficient to measure
 502 the cement paste yield stress evolution in time (i.e. A_{thix}) and to measure the
 503 increase of the yield stress with the volume fraction (i.e. $g(\phi)$) for a single
 504 resting time t_{rest} to infer the value $A_{thix}g(\phi)$ of the structuration rate of the
 505 suspension (and more generally of fresh concrete).

507 In Fig. 5, we plot a summary of the dimensionless yield stress measurements
508 $\tau_c(\phi)/\tau_c(0)$ performed on all the materials by Mahaut *et al.* [2], together with
509 the results obtained with cement pastes.

510 We find that all the results are consistent: the dimensionless yield stress
511 $\tau_c(\phi)/\tau_c(0)$ is independent of the physicochemical origin of the material yield
512 stress, of the bead material and of the bead size, and of the paste yield stress;
513 it is a function of the volume fraction only. This means that the particles have
514 a purely mechanical contribution to the paste behavior, which is indepen-
515 dent of the physicochemical properties of the materials: the only important
516 matter is the value of the yield stress of the paste. This also validates our
517 approach: as long as the coarse particle size is much larger than the cement
518 paste microstructure, a suspension of coarse particles in a cement paste can
519 be considered more generally as a suspension of rigid noncolloidal particles in
520 a yield stress fluid.

521 This result helps proposing a method than can be applied to obtain quickly
522 the effect of particles of any kind (any shape, any size distribution) on the yield
523 stress of a cement paste. Actually, preparing a model yield stress fluid of stable
524 and reproducible rheological properties, showing no setting nor thixotropic
525 effects (e.g. an emulsion), is quite easy, and measurements are much easier to
526 perform on these materials. Then a great amount of accurate experiments can
527 be performed to measure the properties of suspensions of particles in this yield
528 stress fluid. Finally, the result of the measurement of the dimensionless yield
529 stress $\tau_c(\phi)/\tau_c(0) = g(\phi)$ as a function of the volume fraction ϕ of particles

530 in this yield stress fluid should hold if the interstitial paste is a cement paste.
531 Moreover, we have shown that the knowledge of the structuration rate A_{thix} of
532 a cement paste is sufficient to infer the structuration rate of the suspension of
533 particles in this cement paste (it is equal to $A_{thix}g(\phi)$). A measurement of the
534 cement paste structuration at rest plus the measurement $\tau_c(\phi)/\tau_c(0) = g(\phi)$ in
535 a model yield stress fluid then provides everything that is needed to infer the
536 behavior of mortars or concretes. Note however that these results apply only
537 as long as the particle size is much larger than the cement paste microstructure
538 typical size so that the particles see the yield stress fluid as an homogeneous
539 material. This should not be true otherwise: if the particles were to be sensitive
540 to the cement paste microstructure, then the behavior should depend on the
541 exact details of the specific microstructure of each paste. E.g., in the case of
542 particles suspended in a foam, Cohen-Addad *et al.* [49] found that the behavior
543 of the suspension depends on the particle size for particles of size lower than
544 5 times the bubble size in the foam. Note finally that another important
545 requirement is that the fraction of superplasticizer adsorbed at the surface
546 of the aggregates suspended in the paste is negligible. The study of Hammer
547 and Wallevik [23] suggests that in some cases (it may depend strongly on the
548 cement paste composition) this may be true only if the aggregates are larger
549 than 0.25 to 0.5mm; in such cases, our approach would then be valid for SCC
550 only if the suspending yield stress fluid includes the fine aggregates (of size
551 lower than 0.25 to 0.5mm in the study of Hammer and Wallevik).

553 Proposing a theoretical value for the dimensionless yield stress is challenging.
 554 However, it has been shown by Chateau *et al.* [1] that it is possible to give
 555 a general relationship between the linear response of the materials (e.g. its
 556 dimensionless elastic modulus $G'(\phi)/G'(0)$ as probed under the yield stress)
 557 and the dimensionless yield stress $\tau_c(\phi)/\tau_c(0)$ of a suspension of rigid parti-
 558 cles in a yield stress fluid. This estimate is based on the following hypotheses:
 559 the particles are rigid and noncolloidal; there are no physicochemical interac-
 560 tions between the particles and the paste; the distribution of the particles is
 561 isotropic. This is what we have managed to perform experimentally, therefore,
 562 our experiments are fitted to provide a test of these theoretical predictions.
 563 Chateau *et al.* [1] find

$$\tau_c(\phi)/\tau_c(0) = \sqrt{(1 - \phi)G'(\phi)/G'(0)} \quad (4)$$

564 Mahaut *et al.* [2] have measured the elastic modulus of all the suspensions
 565 studied above, and found a Krieger-Dougherty model to apply $G'(\phi)/G'(0) =$
 566 $(1 - \phi/\phi_m)^{-2.5\phi_m}$ for the dimensionless elastic modulus. Combining this equa-
 567 tion and the theoretical expression Eq. 4 thus yields for the yield stress the
 568 Chateau-Ovarlez-Trung model [1]

$$\frac{\tau_c(\phi)}{\tau_c(0)} = \sqrt{\frac{1 - \phi}{(1 - \phi/\phi_m)^{2.5\phi_m}}} \quad (5)$$

569 which should be valid for any isotropic suspension of rigid spherical noncol-
 570 loidal particles in yield stress fluids with no physicochemical interactions be-
 571 tween the particles and the paste.

572 Our experimental data are compared to Eq. 5 on Fig. 5. We find a remarkable
573 agreement between our data and this model with a best fit for $\phi_m = 0.56$;
574 note that this value of 0.56 is valid only for the case of monodisperse spherical
575 particles we studied.

576 Note however that Eq. 5 can *a priori* be easily modified to account for polydis-
577 persity and for complex shapes of the particles when studying more complex
578 suspensions. Actually, Eq. 4 should hold in all cases. It is then sufficient to
579 know what is the linear response of a suspension made with the studied parti-
580 cles to infer the yield stress value. This linear response can be measured with
581 the method presented in this paper (it is the dimensionless elastic modulus
582 $G'(\phi)/G'(0)$); it can also be inferred from the huge amount of dimension-
583 less viscosity data from the literature dealing with suspensions of particles in
584 Newtonian fluids (with the same particles): the problem of the elasticity of
585 a suspension of rigid particles in a linear elastic material is actually formally
586 similar to the problem of the viscosity a suspension of rigid particles in a
587 Newtonian (thus linear) material.

588 4.4 Comments

589 Our results are naturally close to the Ancy and Jorrot [33] ones, as they have
590 chosen to measure the yield stress of the suspension by means of a slump test
591 which ensures avoiding migration of particles and anisotropy of the material.
592 On the other hand, we find very different values from Geiker *et al.* [26], Erdo-
593 gan [27], and Toutou and Roussel [28]. As pointed out in Sec. 1 and Sec. 3, this
594 is due to the shortcomings of their experimental procedure which is based on a
595 flow and an extrapolation of the dynamic yield stress from a flow curve. Their

596 materials are then likely to be heterogeneous and anisotropic. Moreover, an
597 extrapolation from a flow curve provides an overestimation of the yield stress
598 of the suspension [1] because the suspension departs from a Herschel-Bulkley
599 (or Bingham) model at very low shear rate (unaccessible to most concrete
600 rheometers) and has a lower yield stress than the one extrapolated from the
601 accessible flow curve, even if the suspending yield stress fluid has a Herschel-
602 Bulkley (or Bingham) behavior.

603 Finally, note that in most papers the results are presented vs. ϕ/ϕ_{max} where
604 ϕ_{max} is the maximum packing fraction (taken at about 0.65 for monodisperse
605 particles) and the yield stress divergence is expected to occur for $\phi/\phi_{max} = 1$.
606 This is not correct: the maximum volume fraction ϕ_m for the yield stress sharp
607 increase should not be taken as the maximum volume fraction one can reach
608 by packing particles together (which is the definition of the maximum pack-
609 ing fraction ϕ_{max}). The maximum volume fraction for the yield stress sharp
610 increase is rather the one at which direct contacts become important, which
611 is the limit of application of models including only hydrodynamic interactions
612 between the particles, and also the limit between SCC and ordinary rheology
613 concretes [29]. This explains why we find the yield stress to diverge at around
614 56% while the maximum packing fraction is of about 65% for spheres.

615 **5 Conclusion**

616 We have studied the behavior of suspensions of coarse particles in a thixotropic
617 cement paste. We managed to design procedures that allow for (i) studying
618 an homogeneous and isotropic suspension, (ii) comparing the yield stress of
619 a given cement paste to that of the same cement paste added with particles,

620 (iii) accounting properly for the thixotropy of the cement paste. We observed
 621 that the yield stress of these pastes follows the very simple Chateau-Ovarlez-
 622 Trung model [1] $\tau_c(\phi)/\tau_c(0) = \sqrt{(1 - \phi)(1 - \phi/\phi_m)^{-2.5\phi_m}}$, with $\phi_m = 0.56$ for
 623 monodisperse spherical particles, consistently with the experimental results
 624 of Mahaut *et al.* [2] obtained with many different suspensions. This supports
 625 the fact that the yield stress of the suspension is independent of the physic-
 626 ochemical properties of the yield stress fluid, and depends only on its yield
 627 stress value. This shows that studies of suspensions in model yield stress fluids
 628 can be used as a general tool to infer the behavior of fresh concrete. More-
 629 over, we showed that the thixotropic structuration rate of these pastes (their
 630 static yield stress increase rate in time) is not changed by the presence of the
 631 particles. This shows that it is sufficient to measure the cement paste yield
 632 stress evolution in time and to measure the increase of the yield stress with
 633 the volume fraction of coarse particles for a single resting time to predict the
 634 value of the structuration rate of fresh concrete. For a linear increase of the
 635 cement paste yield stress with a rate A_{thix} , we predict a linear increase of the
 636 suspension with a rate $A_{thix}\sqrt{(1 - \phi)(1 - \phi/\phi_m)^{-2.5\phi_m}}$.

637 **A Characterization of the interstitial paste**

638 In this appendix, we detail the arguments that have led to develop the pro-
 639 cedure presented in Sec. 3. This new procedure is built to ensure a good
 640 knowledge of the mechanical properties and of the state of structuration of
 641 the interstitial cement paste in the suspension.

642 First, we have to note that it is very difficult to achieve a good reproducibility
 643 of a fresh cement paste mechanical behavior. In Fig. A.1a we show the result

644 of the yield stress measurements performed (apparently) exactly in the same
645 conditions in 2 cement pastes having the same composition. We observe that
646 the uncertainty on the yield stress of the cement paste we get is of order 25%.
647 This means that, if we want to measure accurately the ratio of the suspension
648 yield stress to the interstitial cement paste yield stress, we cannot compare the
649 properties of suspensions of particles in a cement paste to the properties of a
650 cement paste having the same composition but being from a different batch.
651 That is why we chose to work on the same batch for the measurement of the
652 properties of the paste alone and for the suspension.

653 Then, for a given cement paste batch, we could propose to first measure the
654 cement paste yield stress and then the suspension yield stress. For the results
655 to be comparable, one would then just have to perform the experiment in the
656 same conditions as regards thixotropy (i.e. for the same resting time after a
657 strong preshear). In order to check the validity of this method, we performed
658 yield stress measurements several times in the same conditions (i.e. for a 2
659 minutes resting time after a strong stirring of the paste) on a single cement
660 paste batch. The results of this experiment are depicted in Fig. A.2 as a
661 function of the time t_{age} elapsed since the constituents of the cement paste
662 were mixed together. We observe that due to various irreversible chemical
663 interactions in the material, the cement paste yield stress, measured in the
664 same conditions as regards thixotropic effects, evolves (non-monotonously) as
665 a function of the time t_{age} elapsed since the constituents of the cement paste
666 were mixed together. This means that one cannot know what is the yield
667 stress of the interstitial paste in a suspension if the yield stress of the cement
668 paste alone is not measured at exactly the same time after mixing as the yield
669 stress of the suspension. That is why we chose to measure simultaneously the

670 yield stress of the suspension and the yield stress of the cement paste alone
671 in exactly the same conditions (same age t_{age} after mixing the constituents of
672 the cement paste, same time t_{rest} after the end of the strong stirring), with
673 the help of 2 rheometers that perform their measurements in parallel. We
674 show in Fig. A.1b that, as expected, this method yields a very low uncertainty
675 when the measurements are performed on the same cement paste (without
676 particles).

677 Now, by performing these simultaneous measurements of the suspension yield
678 stress $\tau_c(\phi)$ and of the cement paste yield stress $\tau_c(0)$ several times, at various
679 ages t_{age} after mixing the constituents of the cement paste, we should observe
680 the same effect of the particles on the yield stress whatever the age of the
681 cement paste. In Fig. A.3 we present the dimensionless yield stress $\tau_c(\phi)/\tau_c(0)$
682 as a function of the time t_{age} elapsed since the constituents of the cement paste
683 were mixed together. We observe that $\tau_c(\phi)/\tau_c(0)$ is not constant in time. This
684 means that the interstitial paste is not in the same mechanical state as the
685 paste alone although they have apparently the same history. The only differ-
686 ence stands in the preshear procedure: before performing each measurement,
687 the paste and the suspension are presheared to ensure a reproducible destruc-
688 tured initial state. As pointed out above, the preshear has to be manual to
689 avoid migration and anisotropy. Our results show that this preshear is not as
690 efficient in the suspension as in the cement paste. It is harder to shear the sus-
691 pension, thus an experimentalist cannot shear the suspension the same way as
692 the paste alone. It can be noted that, in the case of a strong mechanical pres-
693 hear in a mixer, an opposite result has been obtained by Toutou and Roussel
694 [28] due to the mixing effect of the particles. As a result of these imperfect
695 and perturbing preshears, the differences between the structuration state of

696 the paste alone and of the interstitial paste in the suspension increases with
697 time. The suspension and the cement paste cannot be compared anymore, and
698 the function $\tau_c(\phi)/\tau_c(0)$ is no more correctly measured by this means. A solu-
699 tion to this problem is to perform only a single measurement on a suspension,
700 for a given resting time after its preparation. As pointed out in Sec. 3.2, a
701 key point of the comparison between the suspension and the cement paste is
702 then that the cement paste alone is first initially strongly presheared in the
703 mixer for both samples before being loaded (and eventually mixed with the
704 particles) in the measurement cups: this defines an initial destructured state
705 of the paste that is the same both for the interstitial cement paste and for
706 the cement paste alone. The manual stirring in the measurement cup then
707 ensures an homogeneous dispersion of the particles in the suspension, while
708 keeping the cement paste in a destructured state in both samples. With this
709 procedure, one ensures that the paste alone and the interstitial paste have the
710 same history and thus the same behavior. We show actually in Fig. A.3 that,
711 in these conditions, the same value of $\tau_c(\phi)/\tau_c(0)$ is found within the measure-
712 ment uncertainty whatever the time t_{age} elapsed since the constituents of the
713 cement paste were mixed together.

714 Finally, as the cement paste is thixotropic, its static yield stress increases as
715 a function of the time t_{rest} elapsed since the end of the stirring. However,
716 if we want to account properly for the (reversible) thixotropic behavior of
717 the cement paste, and to check what the influence of the particles on this
718 thixotropic behavior is, we face a problem. We showed that the value of the
719 yield stress measured 2 minutes after a strong stirring evolves as a function
720 of the time t_{age} elapsed since the constituents were mixed together, even at
721 short times. This would mean that in order to characterize the increase of

722 the yield stress of cement pastes due to structuration at rest, as a function
723 of the resting time t_{rest} after a strong stirring, we would need to perform
724 all the yield stress measurements only at a same given age t_{age} after mixing
725 the constituents of the cement paste. And this characterization of thixotropy
726 would only have a meaning for this age t_{age} . However, we show in the following
727 that the thixotropic increase of the yield stress is actually the same whatever
728 the paste age. In Fig. A.4a, we plot the yield stress of a cement paste as a
729 function of the age t_{age} of the paste for 3 different times t_{rest} after a strong
730 stirring; note that as we have only 2 rheometers, these measurements had to
731 be performed on 2 batches, so that the uncertainties may be rather large (as
732 in Fig. A.1a).

733 We observe the same evolution of the paste behavior as a function of t_{age}
734 whatever t_{rest} . An important consequence is that the irreversible effects can
735 be separated from the reversible effects by writing

$$\tau_c(t_{rest}, t_{age}) = \tau_c(t_{age}) + \tau_c(t_{rest}) \quad (\text{A.1})$$

736 where $\tau_c(t_{age})$ is the yield stress that would be measured just after a preshear,
737 which depends on the time t_{age} elapsed since the constituents were
738 mixed together, and $\tau_c(t_{rest})$ represents the increase of the yield stress due
739 to thixotropic effects, which depends only on the time elapsed since the end of
740 a preshear. This is shown in Fig. A.4b: all data are superposed when shifted
741 by a constant value that depends only on t_{rest} . From the superposition of
742 data in Fig. A.4b, we find that $\tau_c(t_{rest} = 4\text{min}) - \tau_c(t_{rest} = 2\text{min}) = 24\text{Pa}$ and
743 $\tau_c(t_{rest} = 6\text{min}) - \tau_c(t_{rest} = 2\text{min}) = 48\text{Pa}$. This is consistent with the simple law
744 proposed by Roussel [19] i.e. the increase of the yield stress due to thixotropy

745 is basically linear in t_{rest} : it reads $\tau_c(t_{rest}) = A_{thix} t_{rest}$ with an increase rate
746 $A_{thix} = 12\text{Pa}/\text{min}$. Finally, as the absolute increase of the yield stress due to
747 thixotropic effects is the same at any time t_{age} (lower than 90 min) since the
748 constituents were mixed together, this shows that studies of thixotropy and
749 of the effect of the coarse particles on this thixotropy performed at different
750 times t_{age} can be compared together and provide relevant information on the
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Constituents	% by mass
SiO ₂	20.95
Al ₂ O ₃	4.08
TiO ₂	0.14
Fe ₂ O ₃	0.22
CaO	65.55
MgO	0.49
Na ₂ O	0.12
K ₂ O	0.20
SO ₃	2.60
RI	1.47
PAF	3.36

Table 1

Cement chemical constituents.

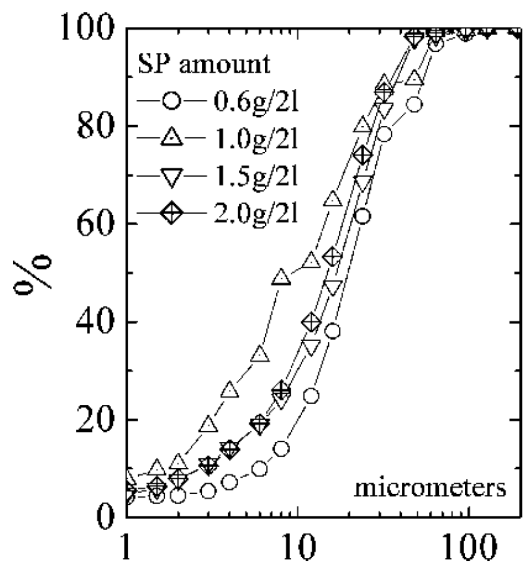


Fig. 1. Cement size distribution curve for various superplasticizer (SP) amount.

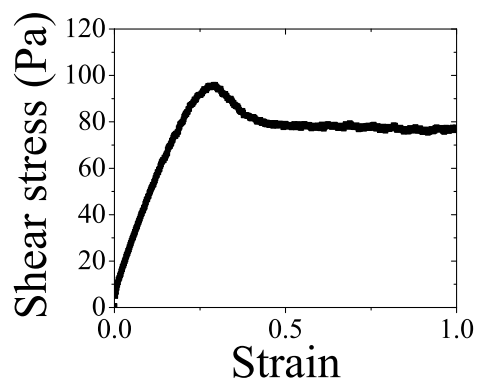


Fig. 2. Shear stress vs. strain when slowly shearing a cement paste at 10^{-2}s^{-1} 2 minutes after a strong stirring of the paste.

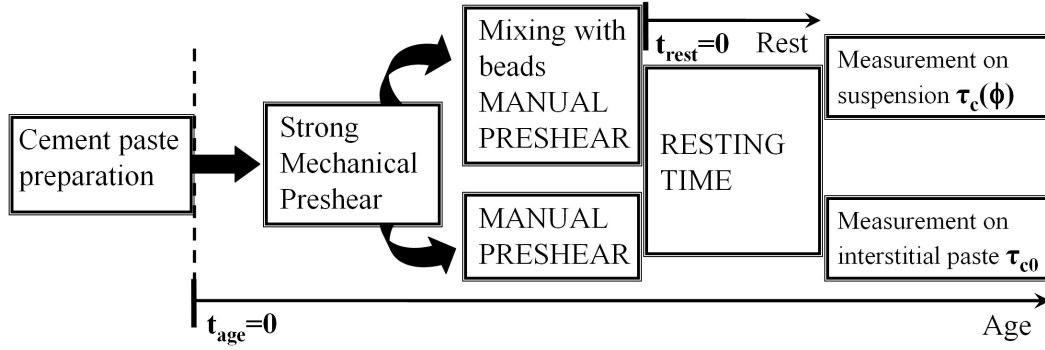


Fig. 3. Sketch of the procedure designed to study the evolution of the dimensionless yield stress $\tau_c(\phi)/\tau_c(0)$ with the volume fraction ϕ of particles in the suspension.

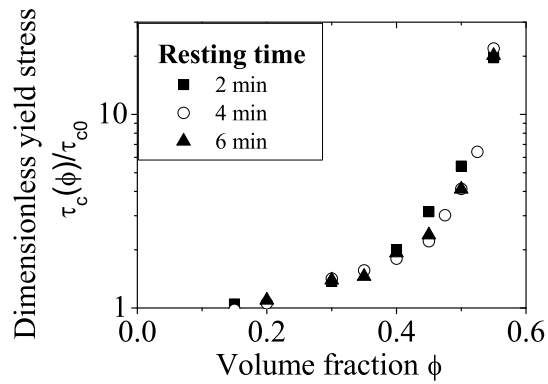


Fig. 4. Dimensionless yield stress $\tau_c(\phi)/\tau_c(0)$ vs. the bead volume fraction ϕ for suspensions of 2mm glass beads in a cement paste, measured with the procedure developed in Sec. 3 for various times t_{rest} after a strong stirring of the suspension.

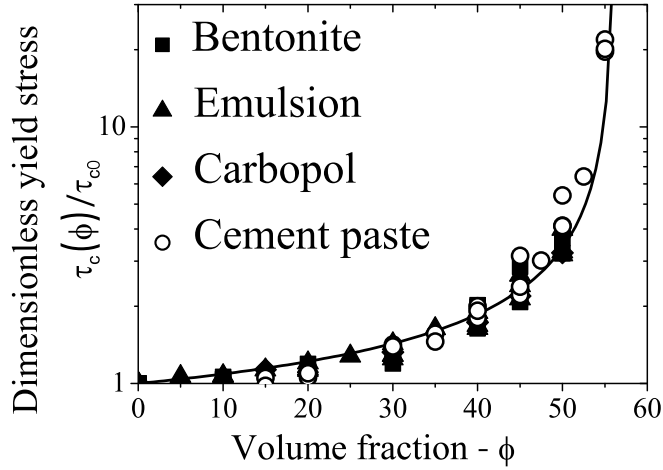


Fig. 5. Dimensionless yield stress $\tau_c(\phi)/\tau_c(0)$ vs. the bead volume fraction ϕ for suspensions of 80, 140, and 315 μm polystyrene beads and 140 μm , 330 μm and 2mm glass beads in various bentonite suspensions, emulsions and Carbopol gels (results from Mahaut *et al.* [2]), and for 2mm glass beads suspended in a cement paste. The solid line is the Chateau-Ovarlez-Trung model $\sqrt{(1-\phi) \times (1-\phi/\phi_m)^{-2.5\phi_m}}$ with $\phi_m = 0.56$.

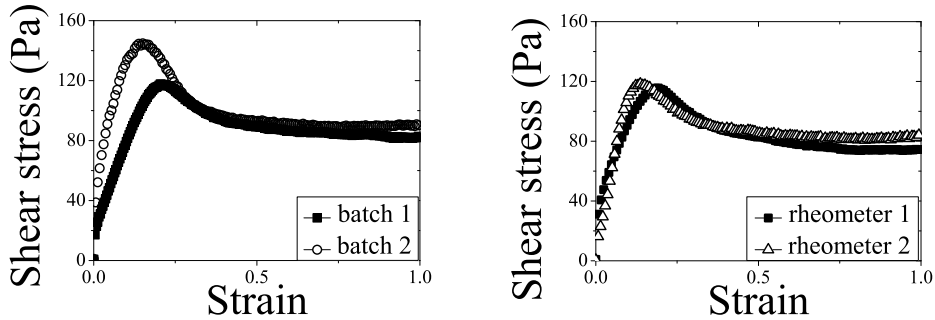


Fig. A.1. a) Shear stress vs. strain when slowly shearing two batches of a cement paste at 10^{-2} s^{-1} 2 minutes after a strong stirring of the paste. b) Shear stress vs. strain when slowly shearing simultaneously on 2 rheometers a cement paste from a single batch at 10^{-2} s^{-1} 2 minutes after a strong stirring of the paste.

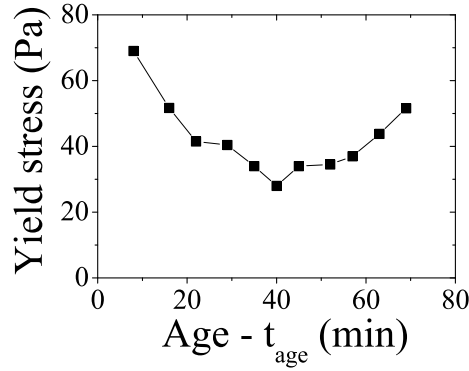


Fig. A.2. Yield stress of a cement paste measured 2 minutes after a strong stirring of the paste vs. the time t_{age} elapsed since the constituents of the cement paste were mixed together.

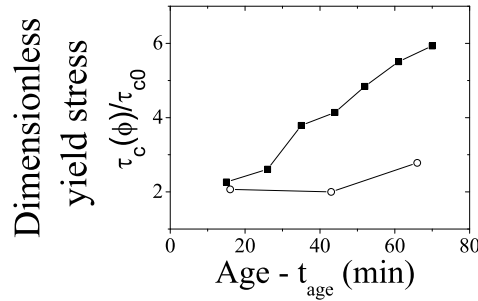


Fig. A.3. Dimensionless yield stress $\tau_c(\phi)/\tau_c(0)$ measured 2 minutes after a strong stirring of the suspension vs. the time t_{age} elapsed since the constituents of the cement paste were mixed together (with a volume fraction of coarse particles $\phi = 40\%$), in two cases: when the same suspension of particles is used for all measurements (squares); when the particles are mixed with the cement paste just before each measurement (open circles).

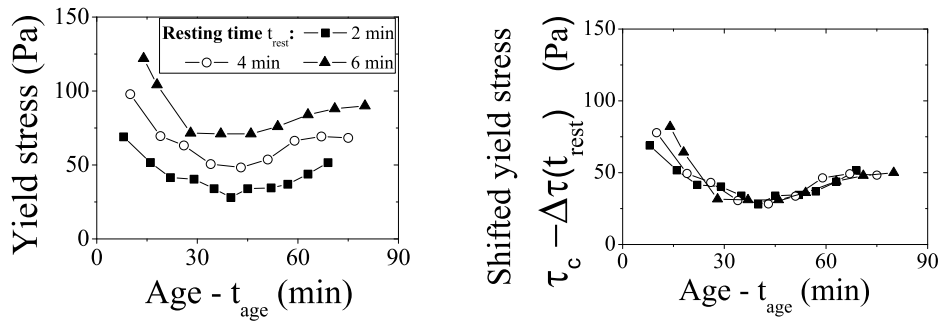


Fig. A.4. a) Yield stress of a cement paste measured 2, 4 and 6 minutes after a strong stirring of the paste vs. time t_{age} elapsed since the constituents of the cement paste were mixed together. b) Data of Fig. A.4a rescaled by shifting the yield stress values by a function $\Delta\tau_c(t_{rest})$ of the time t_{rest} elapsed since the end of the strong stirring.