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 **α -Cd₁₃-xSb₁₀ – the devil is in the details**

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Abstract

A detailed study of the structure of α -Cd₁₃Sb₁₀ was performed using a high quality single crystal obtained from a Cd-rich melt. The study clearly shows that this sample is Cd-deficient, and should more properly be labelled α -Cd_{13-x}Sb₁₀, but whether this is true in general for this phase, or if it is an effect of the precise conditions of synthesis remains unclear. Like for the similar Zn based compound, small differences in the Cd (Zn) content may be crucial in determining the electronic transport properties of the material.

Introduction

The discovery that the compound Zn_4Sb_3 displays thermal transport properties akin to those of Perspex sparked a lot of interest in this unusual compoundⁱ, since bad transport properties is a good thing in a thermoelectric material. That interstitial zinc was responsible for the extreme transport behaviour was first suggested by Snyder *et al.*ⁱⁱ and in a sequence of studies Häußermann *et al.* have conclusively proven the presence of interstitials in this system, as well as a number of different ordering schemes for these^{iii,iv,v}. The importance of subtle changes in composition for the physical properties of the material has been pointed out by several authors^{vi, vii, viii, ix}. While the phase diagram of Zn-Sb is relatively rich, the Cd-Sb system contains only one stable phase, the equimolar CdSb, but on the Cd rich side of the phase diagram a number of phases may be formed with relative facility either from by undercooling the binary melt or from ternary fluxes with Bi, Sn or In. At least two distinct compounds can be made this way, Cd_4Sb_3 and Cd_3Sb_2 , both showing temperature dependent polymorphism. We recently reported on the synthesis, structural elucidation and properties measurements of the two polymorphs of Cd_4Sb_3 , the high temperature phase $\beta\text{-Cd}_4\text{Sb}_3$ and the room temperature phase $\alpha\text{-Cd}_4\text{Sb}_3$ ^x. The phase transition temperature depends significantly on the flux, for a quenched binary sample the $\alpha \rightarrow \beta$ transformation temperature was 375 K, for a Sn flux grown sample the transition temperature was depressed to just above 360 K and for a Bi flux grown sample the transition took place below 360 K. The hysteresis was also quite different for the three samples, for the binary melt quenched sample and the Bi flux grown sample the heating and cooling transitions differed by about 5 K in temperature, but for the Sn grown sample, the difference is more than 25 K, even though the Sn content as measured by electron microprobe analysis is less than 0.1 %. The Cd/Sb balance in the samples shows small differences, but lie close to the crystallographic composition of the α phase, $\text{Cd}_{13}\text{Sb}_{10}$.

The phase transition is caused by the ordering of interstitial Cd positions. This ordering causes some regular Cd sites (corresponding to Wyckoff position 36f in the trigonal β phase cell) to be vacated. In the corresponding Zn based system, we have found that the α -phase is not fully ordered, but that the ordered Zn interstitials are partially unoccupied, and the vacation of the corresponding regular sites is also incomplete.

The single crystal structural study of the melt quenched sample allowed for the solution of the $\alpha\text{-Cd}_4\text{Sb}_3$ phase super structure, but all attempts to locate residual electron density corresponding to incomplete vacation of regular sites were unsuccessful. The quality of the single crystal refinement was however limited by the quality of the single crystal specimen, and in order to further investigate possible occupational disorder in $\alpha\text{-Cd}_4\text{Sb}_3$ we therefore pursued a number of different synthetic procedures in order to grow better quality single crystals that might allow a high quality refinement.

Experimental

Synthesis

A single crystal of the title compound was obtained from a Cd rich melt. A mixture of approximately 1 g of the elements (Cd, 99.9% and Sb, 99.5%; all purchased from Sigma-Aldrich) with the weight ratio Cd:Sb = 0.65:0.40 was loaded in a steel ampoule which was weld-sealed at both ends under argon atmosphere. The sample was first placed vertically in a muffle oven and heated at 923 K. Then, the ampoule was turned to a horizontal position and the oven temperature was cooled down to 673 K where the sample was subsequently annealed

for about 48 hours. Finally, the sample was removed from the furnace and allowed to cool down to room temperature.

Single crystal X-ray diffraction

A suitable crystal was picked from the crushed sample, mounted on a glass fibre and diffraction data was measured on an Oxford Diffraction XCalibur 3 CCD diffractometer with MoK α radiation ($\lambda=0.71073\text{\AA}$, 50kV, 40mA). Two data sets were acquired at room temperature 295 K and at 100 K using an Oxford cryostream system. The data reduction was performed using the Oxford diffraction CrysAlis system, and the refinement was carried out using the JANA2000 program^{xi}. All details of the measurements are given in tables 1 and 2. The monoclinic super structure cell is obvious in the diffraction pattern, but the small crystal chosen exhibits less obvious twinning than expected, and picking out a dominant domain was straight-forward. In figure 1 the twinning pattern is indicated. As indicated, the diffraction pattern consists of two distinct sets. The basic reflections of the β -phase are common to all individuals, while the satellites are unique to each of the three domain orientations in the twinned structure. The data is therefore readily deconvoluted, although absolute intensity information is available only after the structure is solved and refined. In practise, as explained in previous work, to solve the structure a model featuring the β -phase in the setting of the monoclinic unit cell and embellished with a number of interstitial positions identified as noticeable in the electron density map of the solution from the β -phase was used as a starting set. This model was then refined by allowing partial occupancy for any atoms that had neighbours at unphysically short distances. After a number of least squares refinement cycles, positions with an occupancy below a threshold value were discarded, the difference electron density map was evaluated to identify new possible interstitial positions, and the distance map was re-evaluated to identify which positions that should be refined in terms of occupancy. The threshold value was adjusted during the refinement to yield increasingly hard conditions for considering a position as empty. This solution strategy was used in the maximal monoclinic subgroups to $R-3c$, $P2_1/n$, and subsequently in the three subgroups Pn , $P2_1$, and $P-1$. A satisfactory convergence was achievable only in Pn . The structure in space group Pn from previous work was used as a starting model with 60 independent Sb positions and 78 independent Cd positions. The Sb atoms were grouped in two sets (A and B) according to their positions in the β phase structure. The Cd positions were also grouped in two sets, a first, larger, set of 64 Cd positions (A) corresponding to the 36f position in the β phase, and one grouping consisting of the 14 ordered interstitial Cd positions (B). Within these groups each set was modelled using a single, isotropic, thermal displacement parameter. After convergence of this refinement, the difference electron density map was examined for prominent residuals, and the positions of these were compared to, and found to correspond to, those of the vacated regular Cd positions. A new set (C) of these 8 positions were included as partially occupied in a modified model, and the occupancy of the 14 Cd positions in group B corresponding to the ordered interstitials was reduced by the same amount. In the ensuing cycles of refinement the occupancies of these two groups were coupled complementarily. Since the 8 new positions correspond to the 36f position in the β phase, the isotropic thermal displacement parameter of group CdC was set equal to that of set CdA. All pertinent parameters for the x ray study are given in table 1 and 2. Final positional and occupational parameters are given in tables 3 and 4.

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Results and discussion

The results of the refinements, both for the data collected at ambient temperature and for the data from 100 K largely agree with the results previously published, but with two important exceptions. First, the quality of the crystal, and hence the data is far superior in this measurement compared to that of the crystals used earlier, and this is also clear from the final agreement between model and data. The number of observed reflections is lower, as a result of the smaller sample size, but the parameter-to-data ratio is still close to 10 even for the observed ($F^2 > 3\sigma(F^2)$) set. The volumes of the minor twin constituents were about 1/8 each, adding up to 1/4 of the total crystal volume. The twinning matrices were as reported earlier

0.5000	-1.0000	1.5000
0.2500	-0.5000	-0.7500
0.3333	0.6667	0.0000
0.4971	1.0000	1.5000
-0.2500	-0.5000	0.7500
0.3333	-0.6667	0.0000

As shown earlier, the ordered interstitials form chains along the monoclinic a-axis. In figure 2a, the relative positions of these chains are shown in a projection parallel to **a**. Sb atoms are shown in blue, set A of the Cd atoms is shown in yellow, set B in red and set C in green. It is evident that the chains are well separated and that the deformation of the surrounding structure is negligible. A view down the monoclinic c-axis (fig 2b) is ideal for displaying the structure of the chain of interstitials. In this view, the atomic positions of set SbA and SbB and set CdA have been removed from the top of the image to display the chain of interstitials of group CdB and the alternative positions of group CdC more clearly. Finally, in the image 2c, where the structure is projected down the b-axis, the lamellar nature of the structure is shown. An alternation between two filled and one empty lamella is obvious, and this is clearly the reason for the 3-fold superstructure along c.

The reduction in Cd content, x , generated by the partial exchange of the 14 atomic positions in group CdB for the 8 positions in group CdC is given by $\text{Cd}(\text{A})_{64}\text{Cd}(\text{B})_{14(1-x)}\text{Cd}(\text{C})_{8x}\text{Sb}(\text{A,B})_{60}$ which simplifies to $\text{Cd}_{13-x}\text{Sb}_{10}$. In the final refinement, the deficiency on the occupancy of set CdC converges to about 20%. This means that the Cd content is reduced to $\text{Cd}_{12.8}\text{Sb}_{10}$, or from 56.5% to 56.1%, equivalent to about two esd. in the electron microprobe analysis. The failure to locate significant electron density on positions corresponding to set CdC in our previous work may be taken as an indication that this product was in fact stoichiometric $\text{Cd}_{13}\text{Sb}_{10}$, but as mentioned in the introduction, it may equally well simply reflect the quality of the single crystal. It should be noted that weak super structure ordering combined with twinning places rather high demands on crystal quality for detailed analysis. We therefore cannot say with any certainty that the two samples really differ in composition, but there are certainly good reasons to assume that a certain composition range is permissible for Cd_4Sb_3 . The crystal used in this study has a unit cell volume that is 0.2% smaller (at ambient conditions and 0.1% at 100K) than that used in the previous study. The significance of this difference is debatable, and it is in fact larger than would be expected from the Cd deficiency alone. The fact that the phase may be grown from a rather extended region, compositionally as well as in temperature, and that the phase originally formed is the disordered β -phase certainly leaves room for compositional variations. The local structure of α - Cd_4Sb_3 comprising lamellae containing ordered interstitials interleaved with lamellae devoid of interstitial positions certainly offers a facile way to structurally accommodate a slight variation in under-occupancy of Cd. This is indeed the case for the analogous Zn_4Sb_3

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2 compound which further strengthens the suspicion. A last important indication is the report by
3 Zelinska^{xiii} of a Cd₄Sb₃ quenched from the binary melt that doesn't exhibit any super structure
4 ordering at room temperature. This would be most easily understood in terms of small
5 compositional variations determining the transition temperature between the α and β forms of
6 this phase.
7

8 Conclusion

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10 This α -phase structure of Cd₁₃Sb₁₀ from a new synthetic protocol was unambiguously shown
11 to be Cd deficient, i.e., the compound is Cd_{13-x}Sb₁₀. This does not mean that previous studies
12 by us and others indicating a stoichiometric α -phase, or even a room temperature β -phase are
13 in error. To the contrary, we think it indicates a compositional variability within certain
14 bounds that allows for a Cd-poor sample to remain in the β -phase throughout the entire
15 temperature range of the investigation, or to display various degrees of α/β -polyphasic
16 behaviour. As for the compound Zn₁₃Sb₁₀, the α -phase super structure displays a clear layer
17 structure that allows for the facile intergrowth between the two phases. The fact that the Cd
18 compound only forms as a meta stable compound from the melt make detailed investigations
19 of compositional and temporal parameters difficult. Slow cooling of a melt always results in
20 elemental Cd and the 1:1 compound.
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26 CMA European project.
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2 Figure captions
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5 Scheme of the twinned diffraction pattern. The reflections marked by red circles are main
6 reflections from the high temperature b-phase, while those marked by yellow circles generate
7 the superstructure. Every red reflection is part of three twin lattices as indicated for the set
8 along the c^* axis by the three intersection planes.
9

10 2
11 The structure of the compound $Cd_{13-x}Sb_{10}$ in axial projection. Sb positions are shown in blue,
12 regular Zn positions in yellow, ordered interstitial Zn positions are shown in red and finally
13 partially occupied regular Zn in green. a) view down a-axis, b) view down c-axis, c) view
14 down b-axis
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Table 1

Crystal data

$\text{Cd}_{153.662}\text{Sb}_{120}$	$V = 7643.2 (5) \text{ \AA}^3$
$M_r = 31883.1$	$Z = 1$
<u>Monoclinic, Pn</u>	<u>Mo $K\alpha$</u>
$a = 11.4478 (4) \text{ \AA}$	$\mu = 20.81 \text{ mm}^{-1}$
$b = 26.0793 (7) \text{ \AA}$	$T = 293 \text{ K}$
$c = 26.0691 (10) \text{ \AA}$	$0.10 \times 0.05 \times 0.03 \text{ mm}$
$\beta = 100.872 (4)^\circ$	

Data collection

XCalibur 3 diffractometer	<u>42170</u> independent reflections
Absorption correction: <u>Gaussian</u> <u>CrysAlis RED, Oxford Diffraction Ltd.,</u> <u>Version 1.171.32.9 (release 17-07-2007</u> <u>CrysAlis171 .NET) (compiled Aug 17</u> <u>2007,17:36:27) Numerical absorption</u> <u>correction based on Gaussian integration over</u> <u>a multifaceted crystal model</u>	<u>2407</u> reflections with $I > 3\sigma(I)$
$T_{\min} = 0.288, T_{\max} = 0.656$	$R_{\text{int}} = 0.175$
<u>72678</u> measured reflections	

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Refinement

$R[F^2 > 2\sigma(F^2)] =$ <u>0.038</u>	$\Delta\rho_{\max} = 5.10 \text{ e \AA}^{-3}$
$wR(F^2) = 0.070$	$\Delta\rho_{\min} = -3.82 \text{ e \AA}^{-3}$
$S = 0.50$	
<u>42170</u> reflections	<u>445</u> parameters

Table 2

Crystal data

$\text{Cd}_{154.036}\text{Sb}_{120}$	$V = 7636.3 (5) \text{ \AA}^3$
$M_r = 31925.2$	$Z = 1$
<u>Monoclinic, Pn</u>	<u>Mo $K\alpha$</u>
$a = 11.4469 (4) \text{ \AA}$	$\mu = 20.85 \text{ mm}^{-1}$
$b = 26.0624 (9) \text{ \AA}$	$T = 100 \text{ K}$
$c = 26.0579 (10) \text{ \AA}$	$0.10 \times 0.05 \times 0.03 \text{ mm}$
$\beta = 100.797 (3)^\circ$	

Data collection

<u>XCalibur 3</u> diffractometer diffractometer	<u>42010</u> independent reflections
Absorption correction: <u>Gaussian</u> <u>CrysAlis RED, Oxford Diffraction Ltd.,</u> <u>Version 1.171.32.9 (release 17-07-2007</u> <u>CrysAlis171 .NET) (compiled Aug 17</u> <u>2007,17:36:27) Numerical absorption</u> <u>correction based on Gaussian integration over</u> <u>a multifaceted crystal model</u>	<u>3243</u> reflections with $I > 3\sigma(I)$
$T_{\min} = 0.288, T_{\max} = 0.656$	$R_{\text{int}} = 0.144$
<u>72229</u> measured reflections	

Refinement

$R[F^2 > 2\sigma(F^2)] = 0.037$	$\Delta\rho_{\max} = 5.46 \text{ e \AA}^{-3}$
$wR(F^2) = 0.069$	$\Delta\rho_{\min} = -4.78 \text{ e \AA}^{-3}$
$S = 0.56$	
<u>42010</u> reflections	<u>445</u> parameters

Table 3

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (Å²) at T=293K

	<i>x</i>	<i>y</i>	<i>z</i>	<i>U</i> _{iso} */ <i>U</i> _{eq}	Occ. (<1)
Sba1	1.600263	0.8777 (3)	0.692587	0.02009 (10)*	
Sba2	2.0982 (12)	0.6292 (3)	0.6974 (4)	0.02009 (10)*	
Sba3	1.5962 (11)	0.8729 (3)	0.3664 (4)	0.02009 (10)*	
Sba4	1.6062 (12)	0.6167 (3)	0.8571 (5)	0.02009 (10)*	
Sba5	2.0964 (11)	0.8745 (3)	0.5277 (4)	0.02009 (10)*	
Sba6	2.1017 (13)	1.1259 (3)	0.3592 (5)	0.02009 (10)*	
Sba7	1.1013 (13)	0.6213 (3)	1.0323 (5)	0.02009 (10)*	
Sba8	1.5956 (13)	1.1247 (3)	0.5280 (5)	0.02009 (10)*	
Sba9	1.1033 (11)	1.3728 (3)	0.5282 (4)	0.02009 (10)*	
Sba10	1.5982 (10)	1.3637 (3)	0.3606 (4)	0.02009 (10)*	
Sba11	1.0973 (13)	1.1193 (3)	0.6947 (5)	0.02009 (10)*	
Sba12	1.3807 (12)	0.6231 (3)	0.7893 (4)	0.02009 (10)*	
Sba13	1.3813 (11)	1.1247 (3)	0.4551 (4)	0.02009 (10)*	
Sba14	1.3831 (12)	0.8791 (3)	0.6245 (4)	0.02009 (10)*	
Sba15	1.3800 (12)	1.3705 (3)	0.2873 (4)	0.02009 (10)*	
Sba16	1.8832 (11)	0.6267 (3)	0.6249 (4)	0.02009 (10)*	
Sba17	1.8843 (9)	0.8745 (3)	0.4535 (3)	0.02009 (10)*	
Sba18	0.8834 (12)	1.1220 (3)	0.6172 (4)	0.02009 (10)*	
Sba19	0.8837 (11)	0.6151 (3)	0.9580 (4)	0.02009 (10)*	
Sba20	1.3816 (12)	0.8706 (3)	0.2885 (4)	0.02009 (10)*	
Sba21	0.8806 (12)	1.3733 (3)	0.4593 (4)	0.02009 (10)*	
Sba22	1.3815 (12)	0.3759 (3)	0.6222 (4)	0.02009 (10)*	
Sba23	1.8804 (11)	1.1250 (3)	0.2872 (4)	0.02009 (10)*	
Sba24	1.6003 (11)	0.3807 (3)	0.6941 (4)	0.02009 (10)*	
Sbb25	1.8167 (11)	0.5377 (3)	0.7736 (4)	0.01987 (9)*	
Sbb26	1.6743 (11)	0.7129 (3)	0.7077 (4)	0.01987 (9)*	

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Sbb27	1.4969 (11)	0.9485 (3)	0.4895 (4)	0.01987 (9)*	
Sbb28	1.3117 (11)	1.2791 (3)	0.4480 (4)	0.01987 (9)*	
Sbb29	1.3223 (11)	0.7184 (3)	0.6133 (4)	0.01987 (9)*	
Sbb30	1.8090 (11)	0.9618 (3)	0.6062 (4)	0.01987 (9)*	
Sbb31	1.4919 (11)	0.5469 (3)	0.9904 (4)	0.01987 (9)*	
Sbb32	2.1671 (12)	0.5360 (3)	0.8715 (4)	0.01987 (9)*	
Sbb33	1.9907 (11)	0.8012 (3)	0.6580 (4)	0.01987 (9)*	
Sbb34	1.3112 (11)	0.7900 (3)	0.7744 (4)	0.01987 (9)*	
Sbb35	1.3192 (11)	1.2096 (3)	0.6036 (4)	0.01987 (9)*	
Sbb36	1.9919 (11)	0.6965 (3)	0.8241 (4)	0.01987 (9)*	
Sbb37	1.9891 (12)	1.2953 (3)	0.3255 (4)	0.01987 (9)*	
Sbb38	1.4955 (11)	0.5579 (3)	0.6544 (4)	0.01987 (9)*	
Sbb39	0.9938 (11)	1.1950 (3)	0.4913 (4)	0.01987 (9)*	
Sbb40	2.1658 (11)	0.5420 (3)	0.5434 (4)	0.01987 (9)*	
Sbb41	1.6738 (11)	0.7818 (3)	0.5409 (4)	0.01987 (9)*	
Sbb42	1.2950 (10)	0.7154 (3)	0.9510 (4)	0.01987 (9)*	
Sbb43	1.4909 (11)	1.0487 (3)	0.6549 (4)	0.01987 (9)*	
Sbb44	1.4951 (11)	0.4545 (3)	0.8217 (4)	0.01987 (9)*	
Sbb45	1.8183 (11)	1.0380 (3)	0.4372 (4)	0.01987 (9)*	
Sbb46	1.6787 (11)	0.7815 (3)	0.8702 (4)	0.01987 (9)*	
Sbb47	1.4909 (11)	1.0550 (3)	0.3223 (4)	0.01987 (9)*	
Sbb48	2.1601 (11)	0.9688 (3)	0.7012 (4)	0.01987 (9)*	
Sbb49	1.6683 (11)	1.2887 (3)	0.5417 (4)	0.01987 (9)*	
Sbb50	1.7974 (11)	0.9584 (3)	0.2783 (4)	0.01987 (9)*	
Sbb51	1.8153 (11)	0.4652 (3)	0.9497 (4)	0.01987 (9)*	
Sbb52	0.9932 (12)	1.3038 (3)	0.6564 (4)	0.01987 (9)*	
Sbb53	1.4917 (12)	1.4504 (3)	0.4913 (4)	0.01987 (9)*	
Sbb54	2.1655 (11)	0.9591 (3)	0.3790 (4)	0.01987 (9)*	
Sbb55	1.8089 (11)	0.4615 (3)	0.6094 (4)	0.01987 (9)*	
Sbb56	2.1619 (11)	0.4642 (3)	0.7057 (4)	0.01987 (9)*	

Sbb57	2.1638 (11)	1.0324 (3)	0.5334 (4)	0.01987 (9)*	
Sbb58	1.6753 (11)	1.2133 (3)	0.7063 (4)	0.01987 (9)*	
Sbb59	1.6725 (11)	1.2115 (3)	0.3716 (4)	0.01987 (9)*	
Sbb60	1.8147 (12)	1.0348 (3)	0.7778 (4)	0.01987 (9)*	
Cda1	1.5679 (13)	0.7974 (4)	0.7613 (5)	0.02839 (9)*	
Cda2	2.1032 (13)	0.7285 (3)	0.7347 (5)	0.02839 (9)*	
Cda3	2.0595 (12)	0.5515 (3)	0.7643 (5)	0.02839 (9)*	
Cda4	1.6164 (13)	0.9734 (4)	0.4042 (5)	0.02839 (9)*	
Cda5	1.5663 (13)	1.2033 (4)	0.5948 (5)	0.02839 (9)*	
Cda6	1.7664 (12)	0.6496 (3)	0.7971 (5)	0.02839 (9)*	
Cda7	2.0617 (13)	1.0474 (3)	0.4263 (5)	0.02839 (9)*	
Cda8	1.6172 (13)	0.5225 (4)	0.9039 (5)	0.02839 (9)*	
Cda9	1.1013 (12)	1.2708 (3)	0.5687 (5)	0.02839 (9)*	
Cda10	2.0589 (12)	0.9520 (3)	0.5930 (5)	0.02839 (9)*	
Cda11	1.6086 (13)	1.0247 (4)	0.5672 (5)	0.02839 (9)*	
Cda12	1.7661 (13)	0.8540 (4)	0.6303 (5)	0.02839 (9)*	
Cda13	1.7696 (13)	1.1468 (4)	0.4662 (5)	0.02839 (9)*	
Cda14	1.6101 (13)	0.4800 (4)	0.7313 (5)	0.02839 (9)*	
Cda15	1.4246 (13)	0.6991 (3)	0.7217 (5)	0.02839 (9)*	
Cda16	1.8687 (13)	0.7759 (4)	0.7450 (5)	0.02839 (9)*	
Cda17	1.5726 (13)	0.7948 (3)	0.4358 (5)	0.02839 (9)*	
Cda18	1.2557 (12)	1.0988 (3)	0.6214 (4)	0.02839 (9)*	
Cda19	1.3785 (12)	0.4754 (4)	0.9130 (5)	0.02839 (9)*	
Cda20	1.5655 (12)	1.2935 (3)	0.4333 (5)	0.02839 (9)*	
Cda21	1.3818 (12)	1.0232 (3)	0.4170 (5)	0.02839 (9)*	
Cda22	1.2474 (11)	0.5825 (3)	0.9694 (4)	0.02839 (9)*	
Cda23	1.0689 (12)	0.5446 (3)	1.1028 (5)	0.02839 (9)*	
Cda24	2.2705 (12)	0.6070 (4)	0.6318 (5)	0.02839 (9)*	
Cda25	1.2728 (13)	1.3942 (3)	0.4650 (5)	0.02839 (9)*	
Cda26	1.7486 (12)	1.3426 (3)	0.2909 (5)	0.02839 (9)*	

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Cda27	2.2764 (13)	0.8944 (3)	0.4704 (4)	0.02839 (9)*	
Cda28	0.8649 (12)	1.2231 (3)	0.5745 (4)	0.02839 (9)*	
Cda29	2.1166 (13)	1.2242 (4)	0.4057 (5)	0.02839 (9)*	
Cda30	1.7174 (13)	0.6045 (4)	0.6877 (5)	0.02839 (9)*	
Cda31	1.9198 (12)	0.5373 (3)	0.8816 (4)	0.02839 (9)*	
Cda32	2.1166 (12)	0.7753 (3)	0.5705 (4)	0.02839 (9)*	
Cda33	1.3638 (12)	0.9737 (3)	0.5729 (4)	0.02839 (9)*	
Cda34	1.9123 (12)	0.9546 (4)	0.3883 (5)	0.02839 (9)*	
Cda35	1.2073 (12)	1.1410 (3)	0.5137 (4)	0.02839 (9)*	
Cda36	2.2152 (13)	0.6458 (4)	0.8537 (5)	0.02839 (9)*	
Cda37	1.7191 (13)	0.8947 (4)	0.5208 (5)	0.02839 (9)*	
Cda38	1.3701 (12)	0.5255 (4)	0.7400 (5)	0.02839 (9)*	
Cda39	1.9150 (12)	0.4637 (3)	0.7151 (5)	0.02839 (9)*	
Cda40	1.4207 (13)	1.2976 (3)	0.5535 (5)	0.02839 (9)*	
Cda41	1.6142 (13)	0.9748 (4)	0.7366 (5)	0.02839 (9)*	
Cda42	1.8776 (13)	1.2699 (4)	0.4192 (5)	0.02839 (9)*	
Cda43	2.2140 (12)	0.8580 (3)	0.6873 (5)	0.02839 (9)*	
Cda44	1.9150 (12)	1.0400 (3)	0.5477 (5)	0.02839 (9)*	
Cda45	1.0648 (13)	1.4509 (3)	0.5971 (5)	0.02839 (9)*	
Cda46	1.2366 (11)	0.6634 (3)	0.5224 (4)	0.02839 (9)*	
Cda47	1.1125 (12)	0.7252 (3)	1.0707 (4)	0.02839 (9)*	
Cda48	1.2266 (12)	1.3472 (3)	0.3536 (5)	0.02839 (9)*	
Cda49	2.2784 (12)	1.1084 (3)	0.2944 (5)	0.02839 (9)*	
Cda50	1.0645 (12)	1.0453 (3)	0.7667 (5)	0.02839 (9)*	
Cda51	1.3816 (12)	0.5230 (3)	1.0874 (5)	0.02839 (9)*	
Cda52	1.7112 (12)	0.8902 (3)	0.1897 (5)	0.02839 (9)*	
Cda53	1.4242 (13)	1.2023 (4)	0.3862 (5)	0.02839 (9)*	
Cda54	1.7482 (12)	0.8369 (3)	0.2999 (5)	0.02839 (9)*	
Cda55	1.7735 (12)	0.3541 (3)	0.6282 (5)	0.02839 (9)*	
Cda56	1.7296 (12)	0.4035 (3)	0.8602 (5)	0.02839 (9)*	

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3	Cda57	1.7094 (12)	1.1054 (4)	0.3530 (5)	0.02839 (9)*	
4	Cda58	1.8701 (13)	1.2277 (4)	0.2421 (5)	0.02839 (9)*	
5	Cda59	1.9094 (12)	0.9587 (3)	0.7131 (5)	0.02839 (9)*	
6	Cda60	1.3747 (12)	0.4761 (3)	0.5834 (5)	0.02839 (9)*	
7	Cda61	1.7216 (12)	1.4008 (3)	0.5192 (5)	0.02839 (9)*	
8	Cda62	1.9190 (12)	0.5449 (3)	0.5568 (5)	0.02839 (9)*	
9	Cda63	1.7265 (12)	1.0975 (3)	0.6842 (5)	0.02839 (9)*	
10	Cda64	1.4328 (12)	0.8010 (3)	0.5562 (5)	0.02839 (9)*	
11	Cdb65	0.9529 (12)	1.2065 (4)	0.7069 (5)	0.0212 (5)*	0.805 (3)
12	Cdb66	1.5262 (12)	0.3475 (3)	0.7911 (4)	0.0212 (5)*	0.805 (3)
13	Cdb67	1.5442 (13)	0.9573 (4)	0.2759 (5)	0.0212 (5)*	0.805 (3)
14	Cdb68	1.2434 (11)	0.2043 (3)	0.7116 (4)	0.0212 (5)*	0.805 (3)
15	Cdb69	1.4934 (11)	0.1482 (3)	0.7061 (4)	0.0212 (5)*	0.805 (3)
16	Cdb70	1.4621 (11)	0.2756 (3)	0.6976 (4)	0.0212 (5)*	0.805 (3)
17	Cdb71	1.0437 (13)	0.7074 (4)	0.9445 (5)	0.0212 (5)*	0.805 (3)
18	Cdb72	1.4513 (13)	1.4564 (4)	0.3740 (5)	0.0212 (5)*	0.805 (3)
19	Cdb73	1.5278 (11)	0.6524 (3)	0.9598 (4)	0.0212 (5)*	0.805 (3)
20	Cdb74	1.4833 (12)	0.8499 (4)	0.8707 (4)	0.0212 (5)*	0.805 (3)
21	Cdb75	1.4641 (11)	0.7242 (3)	0.8671 (4)	0.0212 (5)*	0.805 (3)
22	Cdb76	1.2544 (11)	0.8006 (3)	0.8860 (4)	0.0212 (5)*	0.805 (3)
23	Cdb77	1.2713 (12)	0.9712 (4)	0.2909 (5)	0.0212 (5)*	0.805 (3)
24	Cdb78	1.2736 (12)	0.5282 (3)	0.4594 (4)	0.0212 (5)*	0.805 (3)
25	Cdc79	-1.491 (3)	0.6737 (12)	-0.0717 (12)	0.020 (3)*	0.195 (3)
26	Cdc80	-1.510 (3)	0.2921 (10)	-0.2642 (11)	0.020 (3)*	0.195 (3)
27	Cdc81	-1.228 (3)	1.0627 (10)	0.1363 (11)	0.020 (3)*	0.195 (3)
28	Cdc82	-1.152 (3)	0.2624 (11)	-0.2267 (12)	0.020 (3)*	0.195 (3)
29	Cdc83	1.668 (3)	1.0232 (11)	0.2107 (12)	0.020 (3)*	0.195 (3)
30	Cdc84	0.445 (3)	0.8213 (12)	0.8604 (12)	0.020 (3)*	0.195 (3)
31	Cdc85	0.443 (3)	0.5325 (10)	0.3500 (11)	0.020 (3)*	0.195 (3)
32	Cdc86	0.197 (4)	0.7797 (15)	0.8615 (16)	0.020 (3)*	0.195 (3)
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Table 4

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (Å²)

	<i>x</i>	<i>y</i>	<i>z</i>	<i>U</i> _{iso} */ <i>U</i> _{eq}	Occ. (<1)
Sb1_1	1.600263	0.8787 (3)	0.692587	0.00971 (9)*	
Sb1_2	2.1016 (11)	0.6281 (3)	0.6908 (4)	0.00971 (9)*	
Sb1_3	1.6020 (10)	0.8707 (3)	0.3601 (4)	0.00971 (9)*	
Sb1_4	1.6033 (11)	0.6184 (3)	0.8548 (4)	0.00971 (9)*	
Sb1_5	2.1013 (10)	0.8724 (3)	0.5231 (4)	0.00971 (9)*	
Sb1_6	2.1013 (11)	1.1274 (3)	0.3551 (4)	0.00971 (9)*	
Sb1_7	1.1033 (11)	0.6225 (3)	1.0285 (5)	0.00971 (9)*	
Sb1_8	1.5946 (10)	1.1261 (3)	0.5216 (4)	0.00971 (9)*	
Sb1_9	1.1053 (10)	1.3725 (3)	0.5243 (4)	0.00971 (9)*	
Sb1_10	1.6009 (9)	1.3639 (2)	0.3562 (4)	0.00971 (9)*	
Sb1_11	1.0994 (10)	1.1171 (3)	0.6883 (4)	0.00971 (9)*	
Sb1_12	1.3815 (10)	0.6263 (3)	0.7864 (4)	0.00971 (9)*	
Sb1_13	1.3883 (10)	1.1249 (3)	0.4501 (4)	0.00971 (9)*	
Sb1_14	1.3832 (10)	0.8785 (3)	0.6191 (4)	0.00971 (9)*	
Sb1_15	1.3809 (11)	1.3726 (3)	0.2806 (4)	0.00971 (9)*	
Sb1_16	1.8855 (9)	0.6279 (3)	0.6190 (4)	0.00971 (9)*	
Sb1_17	1.8806 (7)	0.8751 (3)	0.4514 (3)	0.00971 (9)*	
Sb1_18	0.8855 (10)	1.1202 (3)	0.6137 (4)	0.00971 (9)*	
Sb1_19	0.8903 (10)	0.6142 (3)	0.9527 (4)	0.00971 (9)*	
Sb1_20	1.3802 (10)	0.8715 (2)	0.2841 (4)	0.00971 (9)*	
Sb1_21	0.8828 (10)	1.3689 (2)	0.4531 (4)	0.00971 (9)*	
Sb1_22	1.3795 (10)	0.3758 (3)	0.6173 (4)	0.00971 (9)*	
Sb1_23	1.8835 (10)	1.1273 (3)	0.2857 (4)	0.00971 (9)*	
Sb1_24	1.6034 (10)	0.3755 (3)	0.6894 (4)	0.00971 (9)*	
Sb2_1	1.8145 (10)	0.5380 (3)	0.7707 (4)	0.00914 (9)*	
Sb2_2	1.6734 (10)	0.7147 (3)	0.7069 (4)	0.00914 (9)*	
Sb2_3	1.4954 (10)	0.9490 (3)	0.4858 (4)	0.00914 (9)*	

Sb2_4	1.3194 (10)	1.2828 (3)	0.4412 (4)	0.00914 (9)*	
Sb2_5	1.3191 (10)	0.7144 (3)	0.6113 (4)	0.00914 (9)*	
Sb2_6	1.8140 (10)	0.9630 (3)	0.6022 (4)	0.00914 (9)*	
Sb2_7	1.4896 (9)	0.5437 (2)	0.9869 (4)	0.00914 (9)*	
Sb2_8	2.1679 (10)	0.5343 (3)	0.8671 (4)	0.00914 (9)*	
Sb2_9	1.9871 (10)	0.8046 (3)	0.6537 (4)	0.00914 (9)*	
Sb2_10	1.3206 (9)	0.7924 (2)	0.7659 (4)	0.00914 (9)*	
Sb2_11	1.3225 (10)	1.2098 (3)	0.6043 (4)	0.00914 (9)*	
Sb2_12	1.9915 (10)	0.6942 (3)	0.8209 (4)	0.00914 (9)*	
Sb2_13	1.9927 (10)	1.2974 (3)	0.3223 (4)	0.00914 (9)*	
Sb2_14	1.4922 (10)	0.5572 (2)	0.6519 (4)	0.00914 (9)*	
Sb2_15	0.9941 (10)	1.1981 (3)	0.4884 (4)	0.00914 (9)*	
Sb2_16	2.1726 (10)	0.5430 (3)	0.5407 (4)	0.00914 (9)*	
Sb2_17	1.6776 (10)	0.7822 (2)	0.5385 (4)	0.00914 (9)*	
Sb2_18	1.2949 (9)	0.7162 (2)	0.9470 (4)	0.00914 (9)*	
Sb2_19	1.4859 (9)	1.0492 (3)	0.6524 (4)	0.00914 (9)*	
Sb2_20	1.4967 (10)	0.4528 (3)	0.8180 (4)	0.00914 (9)*	
Sb2_21	1.8176 (10)	1.0415 (2)	0.4362 (4)	0.00914 (9)*	
Sb2_22	1.6831 (9)	0.7830 (2)	0.8674 (4)	0.00914 (9)*	
Sb2_23	1.4906 (10)	1.0496 (3)	0.3188 (4)	0.00914 (9)*	
Sb2_24	2.1639 (10)	0.9674 (3)	0.6971 (4)	0.00914 (9)*	
Sb2_25	1.6725 (10)	1.2883 (3)	0.5369 (4)	0.00914 (9)*	
Sb2_26	1.8005 (9)	0.9594 (2)	0.2740 (4)	0.00914 (9)*	
Sb2_27	1.8254 (10)	0.4678 (3)	0.9445 (4)	0.00914 (9)*	
Sb2_28	0.9950 (10)	1.3031 (3)	0.6531 (4)	0.00914 (9)*	
Sb2_29	1.4973 (10)	1.4476 (3)	0.4870 (4)	0.00914 (9)*	
Sb2_30	2.1755 (9)	0.9636 (2)	0.3720 (4)	0.00914 (9)*	
Sb2_31	1.8169 (10)	0.4633 (3)	0.6039 (4)	0.00914 (9)*	
Sb2_32	2.1675 (10)	0.4685 (3)	0.7005 (4)	0.00914 (9)*	
Sb2_33	2.1574 (9)	1.0315 (3)	0.5308 (4)	0.00914 (9)*	

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Sb2_34	1.6825 (10)	1.2117 (3)	0.7008 (4)	0.00914 (9)*	
Sb2_35	1.6724 (10)	1.2105 (3)	0.3682 (4)	0.00914 (9)*	
Sb2_36	1.8146 (10)	1.0385 (3)	0.7746 (4)	0.00914 (9)*	
Cd1_1	1.5635 (10)	0.7963 (3)	0.7566 (4)	0.01184 (7)*	
Cd1_2	2.1002 (10)	0.7248 (3)	0.7307 (4)	0.01184 (7)*	
Cd1_3	2.0592 (10)	0.5506 (3)	0.7592 (4)	0.01184 (7)*	
Cd1_4	1.6154 (11)	0.9725 (3)	0.4001 (4)	0.01184 (7)*	
Cd1_5	1.5690 (11)	1.2043 (3)	0.5901 (4)	0.01184 (7)*	
Cd1_6	1.7726 (10)	0.6485 (3)	0.7918 (4)	0.01184 (7)*	
Cd1_7	2.0572 (10)	1.0458 (3)	0.4222 (4)	0.01184 (7)*	
Cd1_8	1.6189 (11)	0.5202 (3)	0.9020 (4)	0.01184 (7)*	
Cd1_9	1.1108 (10)	1.2736 (3)	0.5645 (4)	0.01184 (7)*	
Cd1_10	2.0588 (10)	0.9515 (3)	0.5902 (4)	0.01184 (7)*	
Cd1_11	1.6095 (10)	1.0262 (3)	0.5621 (4)	0.01184 (7)*	
Cd1_12	1.7657 (11)	0.8539 (3)	0.6272 (4)	0.01184 (7)*	
Cd1_13	1.7667 (10)	1.1466 (3)	0.4604 (4)	0.01184 (7)*	
Cd1_14	1.6052 (10)	0.4772 (3)	0.7275 (4)	0.01184 (7)*	
Cd1_15	1.4185 (10)	0.6997 (3)	0.7182 (4)	0.01184 (7)*	
Cd1_16	1.8692 (11)	0.7752 (3)	0.7410 (4)	0.01184 (7)*	
Cd1_17	1.5718 (10)	0.7945 (3)	0.4318 (4)	0.01184 (7)*	
Cd1_18	1.2527 (10)	1.0928 (3)	0.6215 (4)	0.01184 (7)*	
Cd1_19	1.3769 (10)	0.4753 (3)	0.9088 (4)	0.01184 (7)*	
Cd1_20	1.5646 (10)	1.2907 (3)	0.4292 (4)	0.01184 (7)*	
Cd1_21	1.3786 (10)	1.0205 (3)	0.4121 (4)	0.01184 (7)*	
Cd1_22	1.2561 (10)	0.5872 (2)	0.9637 (4)	0.01184 (7)*	
Cd1_23	1.0672 (10)	0.5431 (3)	1.0977 (4)	0.01184 (7)*	
Cd1_24	2.2746 (10)	0.6079 (3)	0.6310 (4)	0.01184 (7)*	
Cd1_25	1.2759 (11)	1.3942 (3)	0.4591 (4)	0.01184 (7)*	
Cd1_26	1.7579 (10)	1.3484 (3)	0.2862 (4)	0.01184 (7)*	
Cd1_27	2.2815 (10)	0.8932 (3)	0.4647 (4)	0.01184 (7)*	

Cd1_28	0.8713 (11)	1.2241 (3)	0.5735 (4)	0.01184 (7)*	
Cd1_29	2.1168 (11)	1.2258 (3)	0.4024 (4)	0.01184 (7)*	
Cd1_30	1.7141 (10)	0.6054 (3)	0.6828 (4)	0.01184 (7)*	
Cd1_31	1.9173 (11)	0.5435 (3)	0.8771 (4)	0.01184 (7)*	
Cd1_32	2.1222 (10)	0.7778 (3)	0.5692 (4)	0.01184 (7)*	
Cd1_33	1.3695 (10)	0.9761 (3)	0.5711 (4)	0.01184 (7)*	
Cd1_34	1.9114 (10)	0.9537 (3)	0.3821 (4)	0.01184 (7)*	
Cd1_35	1.2122 (11)	1.1433 (3)	0.5122 (4)	0.01184 (7)*	
Cd1_36	2.2116 (10)	0.6425 (3)	0.8510 (4)	0.01184 (7)*	
Cd1_37	1.7154 (10)	0.8935 (3)	0.5165 (4)	0.01184 (7)*	
Cd1_38	1.3715 (11)	0.5282 (3)	0.7385 (4)	0.01184 (7)*	
Cd1_39	1.9138 (10)	0.4607 (3)	0.7106 (4)	0.01184 (7)*	
Cd1_40	1.4199 (11)	1.2975 (3)	0.5487 (4)	0.01184 (7)*	
Cd1_41	1.6122 (11)	0.9738 (3)	0.7342 (4)	0.01184 (7)*	
Cd1_42	1.8736 (10)	1.2664 (3)	0.4129 (4)	0.01184 (7)*	
Cd1_43	2.2105 (11)	0.8567 (3)	0.6806 (4)	0.01184 (7)*	
Cd1_44	1.9139 (10)	1.0409 (3)	0.5429 (4)	0.01184 (7)*	
Cd1_45	1.0651 (11)	1.4503 (3)	0.5920 (4)	0.01184 (7)*	
Cd1_46	1.2304 (10)	0.6545 (3)	0.5238 (4)	0.01184 (7)*	
Cd1_47	1.1227 (10)	0.7244 (3)	1.0681 (4)	0.01184 (7)*	
Cd1_48	1.2311 (10)	1.3450 (3)	0.3490 (4)	0.01184 (7)*	
Cd1_49	2.2636 (10)	1.1038 (3)	0.2902 (4)	0.01184 (7)*	
Cd1_50	1.0628 (10)	1.0397 (3)	0.7629 (4)	0.01184 (7)*	
Cd1_51	1.3839 (10)	0.5214 (3)	1.0806 (4)	0.01184 (7)*	
Cd1_52	1.7146 (10)	0.8900 (3)	0.1839 (4)	0.01184 (7)*	
Cd1_53	1.4226 (11)	1.2031 (3)	0.3814 (4)	0.01184 (7)*	
Cd1_54	1.7571 (10)	0.8392 (3)	0.2948 (4)	0.01184 (7)*	
Cd1_55	1.7707 (10)	0.3493 (3)	0.6286 (4)	0.01184 (7)*	
Cd1_56	1.7385 (10)	0.4079 (3)	0.8564 (4)	0.01184 (7)*	
Cd1_57	1.7153 (11)	1.1034 (3)	0.3492 (4)	0.01184 (7)*	

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Cd1_58	1.8678 (11)	1.2270 (3)	0.2407 (4)	0.01184 (7)*	
Cd1_59	1.9093 (10)	0.9604 (3)	0.7092 (4)	0.01184 (7)*	
Cd1_60	1.3830 (10)	0.4791 (3)	0.5771 (4)	0.01184 (7)*	
Cd1_61	1.7145 (10)	1.3953 (3)	0.5174 (4)	0.01184 (7)*	
Cd1_62	1.9246 (10)	0.5459 (3)	0.5540 (4)	0.01184 (7)*	
Cd1_63	1.7324 (10)	1.0960 (3)	0.6808 (4)	0.01184 (7)*	
Cd1_64	1.4315 (10)	0.8005 (3)	0.5531 (4)	0.01184 (7)*	
Cd3_1	0.9614 (9)	1.2057 (3)	0.7031 (4)	0.0041 (3)*	0.836 (3)
Cd3_2	0.5007 (9)	1.3497 (3)	0.7765 (4)	0.0041 (3)*	0.836 (3)
Cd3_3	1.0450 (10)	1.2938 (3)	0.7696 (4)	0.0041 (3)*	0.836 (3)
Cd3_4	1.2582 (9)	1.1997 (2)	0.7142 (4)	0.0041 (3)*	0.836 (3)
Cd3_5	1.5004 (9)	1.1465 (2)	0.7043 (4)	0.0041 (3)*	0.836 (3)
Cd3_6	0.4658 (9)	1.2754 (2)	0.6948 (4)	0.0041 (3)*	0.836 (3)
Cd3_7	0.7761 (10)	1.2757 (3)	0.7895 (4)	0.0041 (3)*	0.836 (3)
Cd3_8	1.0414 (10)	0.7067 (3)	0.9408 (4)	0.0041 (3)*	0.836 (3)
Cd3_9	1.4547 (10)	1.4556 (3)	0.3702 (4)	0.0041 (3)*	0.836 (3)
Cd3_10	1.5196 (9)	0.6517 (2)	0.9520 (4)	0.0041 (3)*	0.836 (3)
Cd3_11	1.4528 (9)	0.8474 (3)	0.8538 (4)	0.0041 (3)*	0.836 (3)
Cd3_12	1.4659 (9)	0.7251 (2)	0.8634 (4)	0.0041 (3)*	0.836 (3)
Cd3_13	1.2497 (9)	0.7987 (2)	0.8785 (4)	0.0041 (3)*	0.836 (3)
Cd3_14	1.2711 (9)	0.5312 (2)	0.4512 (4)	0.0041 (3)*	0.836 (3)
Cd2_1	0.527 (4)	1.3220 (15)	0.7817 (15)	0.021 (3)*	0.164 (3)
Cd2_2	1.379 (3)	1.2755 (12)	0.7222 (13)	0.021 (3)*	0.164 (3)
Cd2_3	0.951 (3)	1.2668 (12)	0.7228 (13)	0.021 (3)*	0.164 (3)
Cd2_4	1.031 (3)	1.2274 (12)	0.7788 (13)	0.021 (3)*	0.164 (3)
Cd2_5	-1.498 (3)	0.6780 (14)	-0.0718 (14)	0.021 (3)*	0.164 (3)
Cd2_6	0.387 (3)	0.8133 (12)	0.8466 (14)	0.021 (3)*	0.164 (3)
Cd2_7	0.225 (3)	0.5027 (12)	0.3892 (13)	0.021 (3)*	0.164 (3)
Cd2_8	0.199 (4)	0.7733 (17)	0.8593 (17)	0.021 (3)*	0.164 (3)

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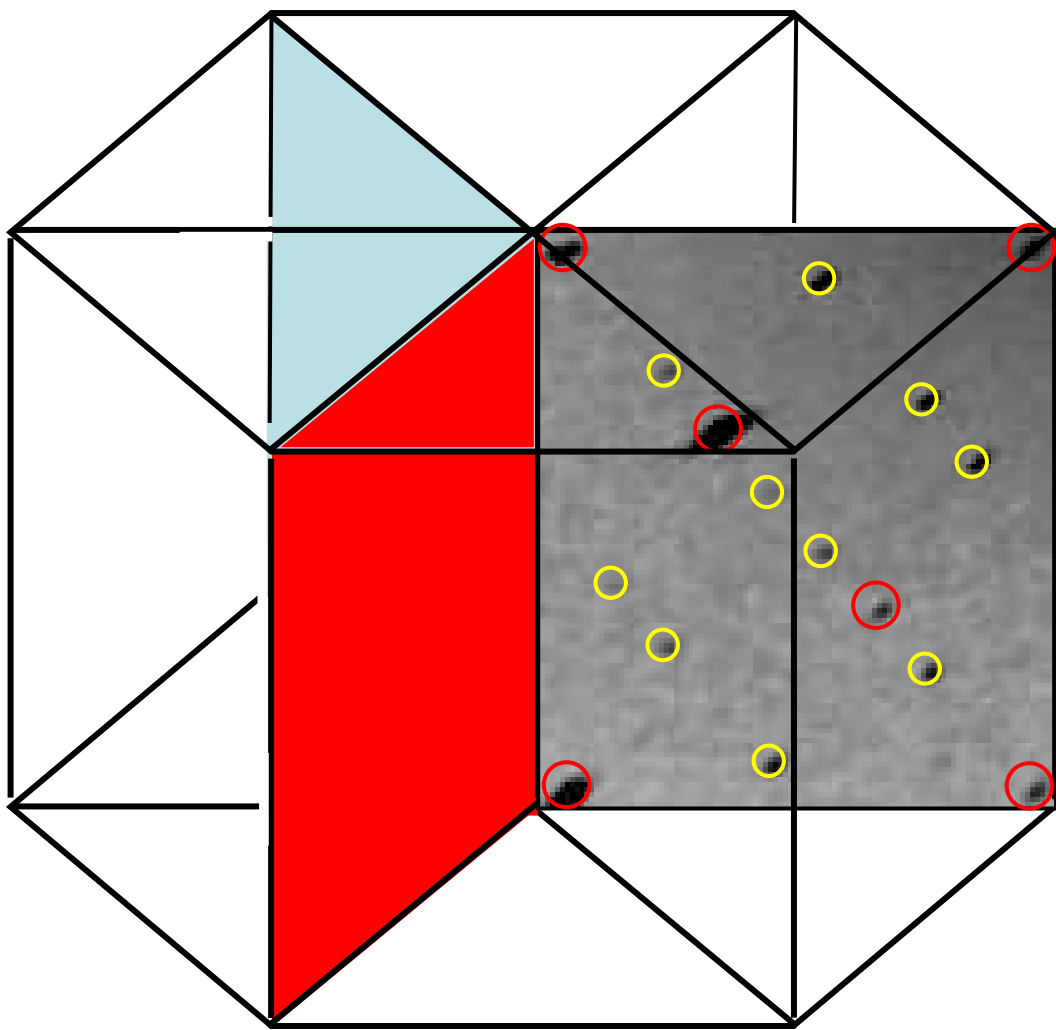


Fig 1

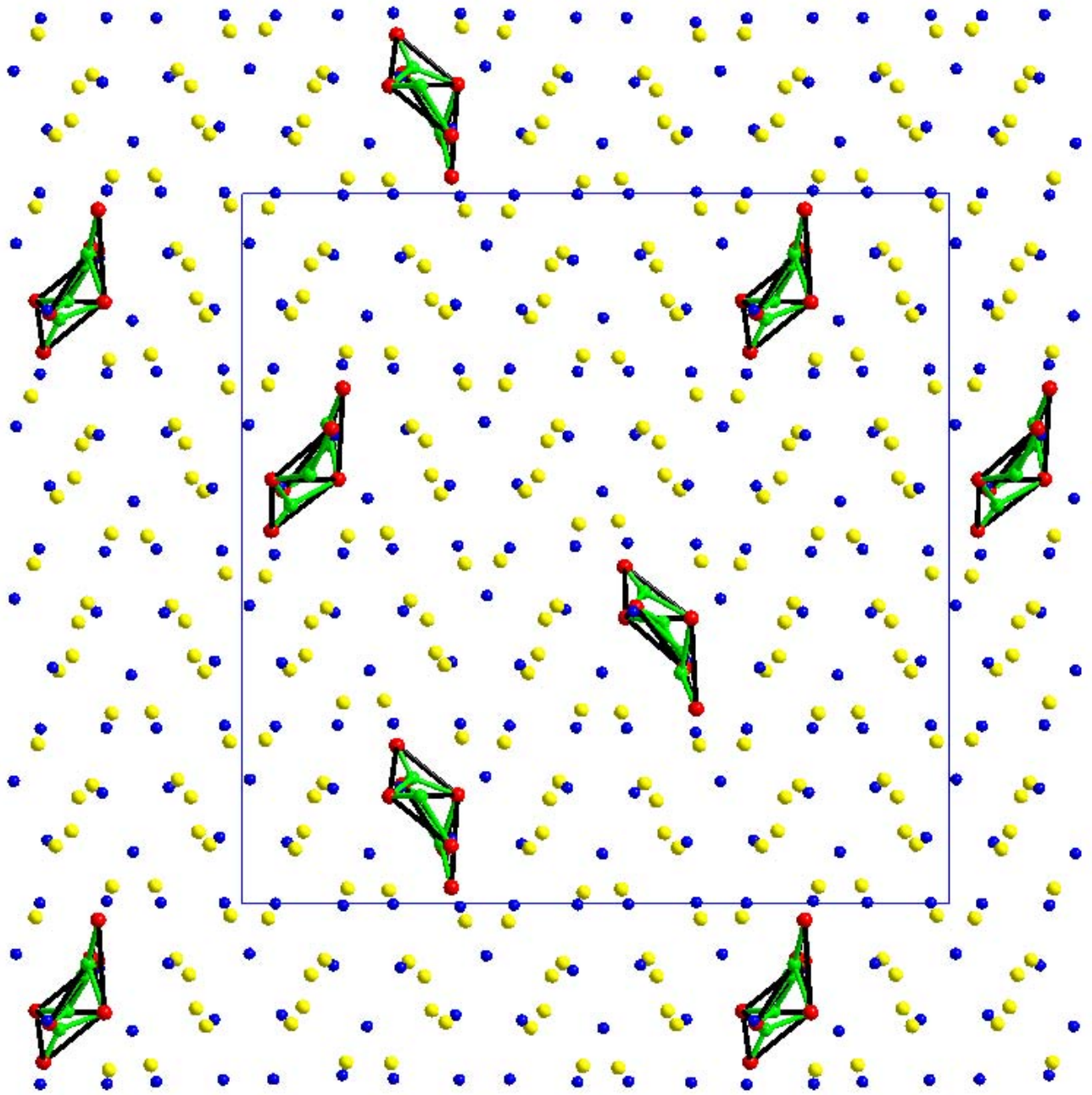


Fig 2a

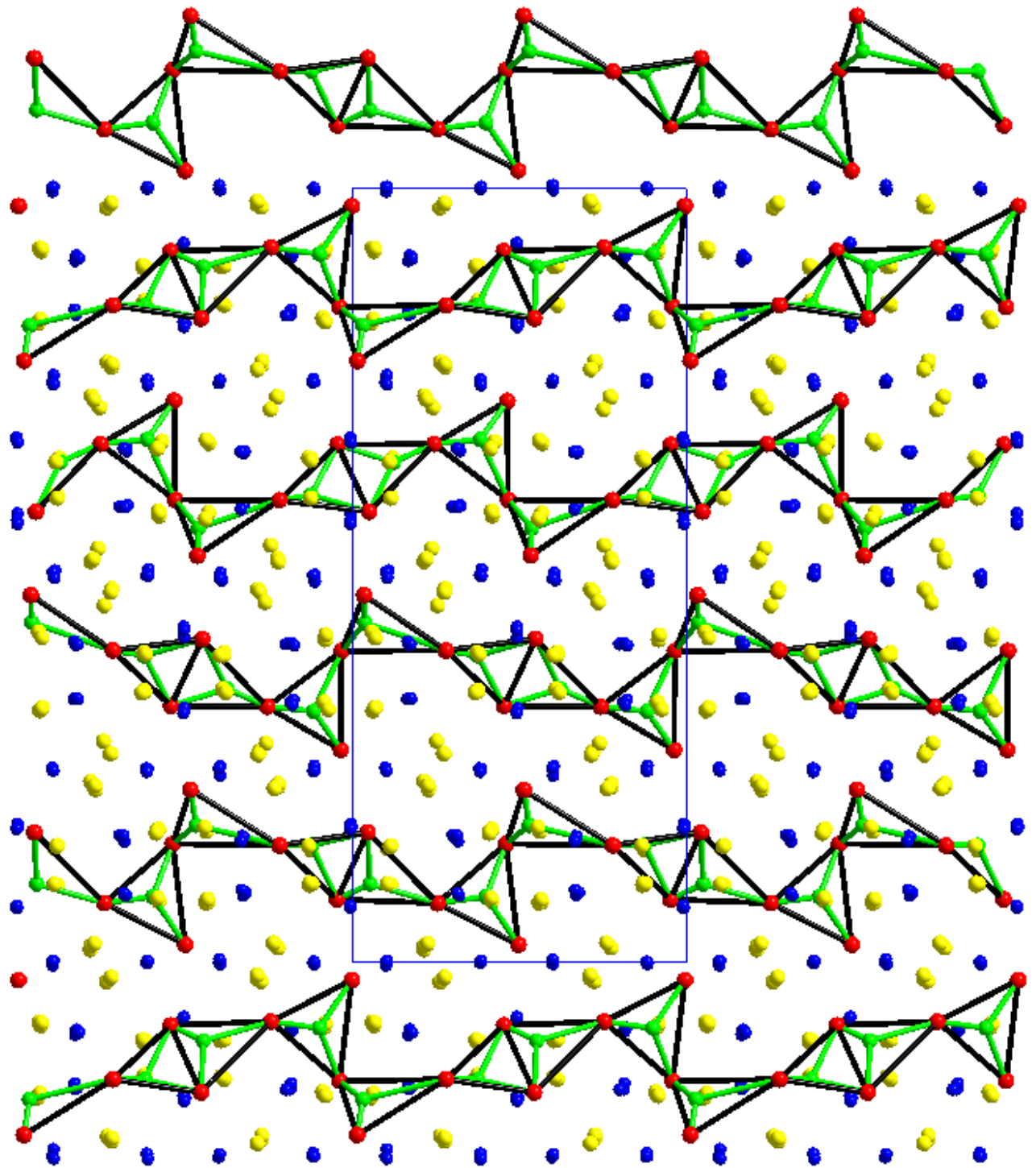


Fig2b

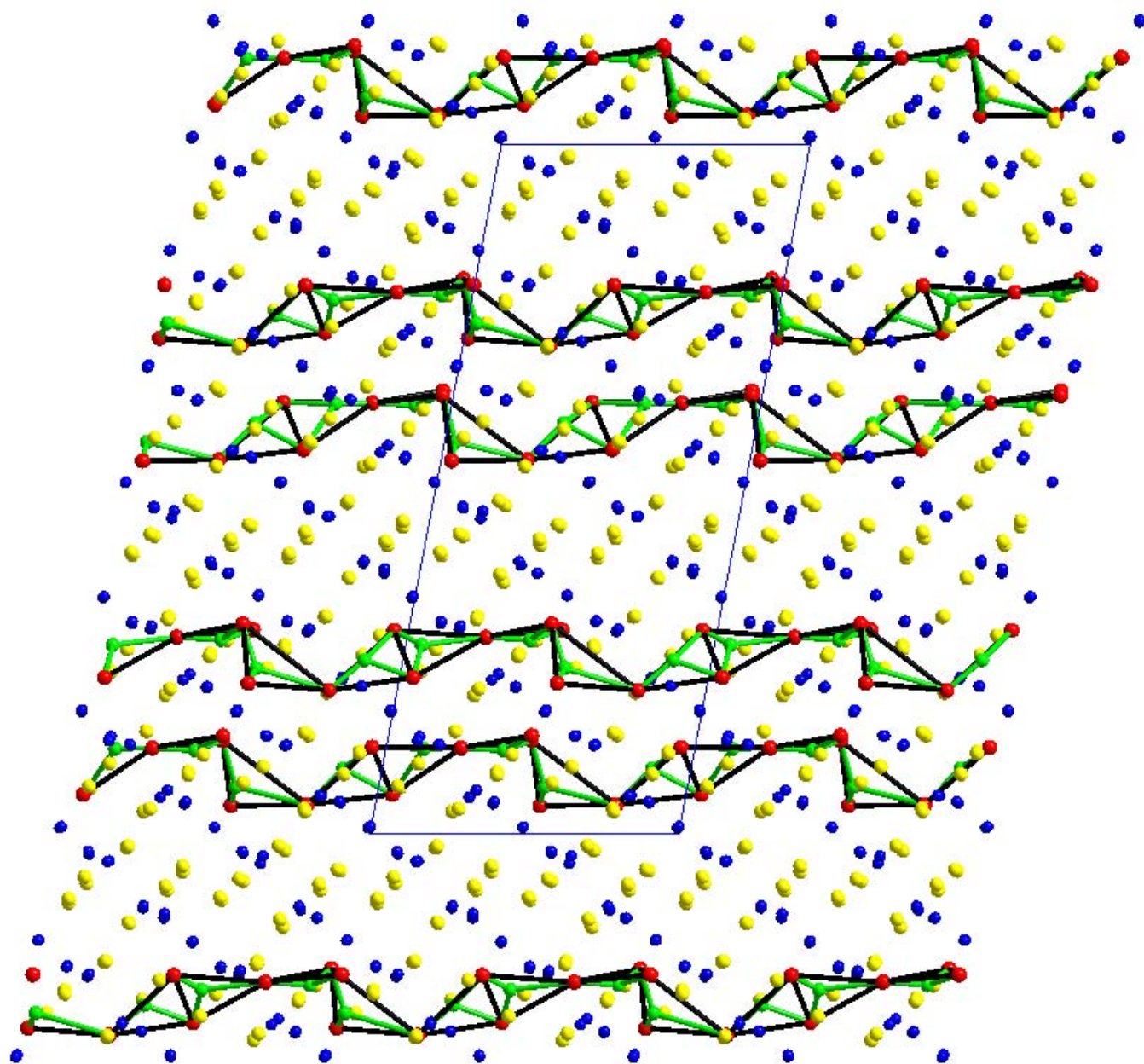


Fig 2c

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