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Ultra-High Q/V Fabry-Perot microcavity on SOI substrate

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Abstract: We experimentally demonstrate an ultra high Q/V nanocavity on SOI substrate. The design is based on modal adaptation within the cavity and allows to measure a quality factor of 58.000 for a modal volume of $0.6(\lambda/n)^3$. This record Q/V value of 10^5 achieved for a structure standing on a physical substrate, rather than on membrane, is in very good agreement with theoretical predictions also shown. Based on these experimental results, we show that further refinements of the cavity design could lead to Q/V ratios close to 10^6 .

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1. Introduction

In recent years, the race for faster optical communications and data processing has motivated research towards optoelectronic devices. The latter will need more functional elements directly interconnected on a single chip to create truly integrated circuits. Functional devices such as channel drop filtering [1,2], On-Off switch or light modulator [3] can be imagined. It is admitted [4] that the exaltation of optical non-linearity and spontaneous emission inhibition or exaltation (threshold laser reduction) [5] are mainly governed by the Q/V ratio. Thus, high quality factor (Q) optical micro-cavities that confine light in small modal volumes (V) at optical wavelength scales are essential components for signal processing. Highest Q as large as 10^8 were obtained on silica toroids [6]. But these toroids have a huge modal volume and gives a Q/V of approximately $5 \cdot 10^4 (\lambda/n)^3$. Recently, the interest in manufacturing ultra small micro-cavities with extremely high Q/V in two dimensional PC slabs have been boosted as those cavities offer mode volumes close to the theoretical limit of $V = (\lambda/2n)^3$. Q factors as high as 10^6 [7,8] have been achieved. These resonators are Fabry-Perot cavities where the Bloch mode is bouncing between two mirrors fabricated on semiconductor air membranes. Even though suspended membranes are viable at a research level, several issues cloud such cavities: they present many drawbacks in terms of electrical injection, thermal dilatation and mechanical stability. So, an ultra-small high Q cavities realized on a substrate is a critical milestone [9-12].

In this work, we report on high-Q, small-V linear Fabry-Perot micro-cavities manufactured in ridge waveguides on silicon-on-insulator wafers without removing the silica cladding. First, we briefly describe the design of modal adaptation principle and present the fabrication process of the photonic nanostructure. After describing the characterization set-up, we detail the optical properties of the microcavities in terms of Q factor, transmittance and losses. Finally, we discuss the increase of cavities performances with the help of a predictive model.

2. Design and fabrication of Fabry-Perot microcavities

In 1997, Foresi et al. [11] demonstrate the viability of a cavity design consisting in two mirrors made of a chain of periodic holes located on a ridge waveguide. Until recent works, the Q factors of such cavities stayed very low and did not exceed 500. The introduction of a tapered section based on modal adaptation permitted to enhance Q factor [12] and we demonstrated the possibility to reach Q factor of about 9000 in a previous work [13]. The tapering process is based on Bloch mode engineering concepts [14] and consists in the adaptation of modes profiles between the fundamental cavity mode supported by the ridge waveguide and the evanescent Bloch mode of the periodic mirror. The design takes into account the vertical cladding dissymmetry of the structure where the cavity lies on the silica cladding. It results in the addition of a tapered section of four holes placed next to the periodic section of the mirror composed of N holes, see Fig. 1. Simulations of such a design show that radiation losses at the ridge-mirror are divided by 400 and that the Q value of the resonant peak calculated for an infinite number of holes is as high as 400,000. This tapering design increase the cavity performance (Q is multiplied by 800) in comparison to a classical Fabry-Perot device with fully-periodic mirrors [15].

Silicon-On-Insulator wafers used in this work were manufactured by SOITEC. Stack layer consists of a 340 nm silicon top layer (waveguide core) and a 2 μm thick SiO_2 insulator supported by a bulk silicon substrate. The ridge waveguide (500 nm width) and holes patterning is performed by electron-beam lithography with a Leica VB-6UHR on a single 400 nm thick NEB22 negative resist spin coated on top of the sample. The electron beam energy is 100 keV resulting in a 5-nm probe-beam diameter. After developing the resist, Inductive-Coupled-Plasma etching of the sample is performed in an industrial plasma chamber (DPS from Applied Materials Inc).

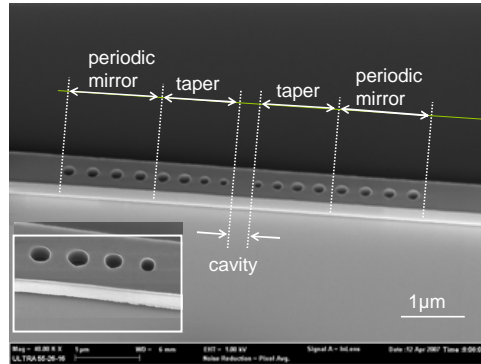


Fig. 1. SEM picture of the lineic Fabry-Perot cavity inserted in the silicon waveguide. On both sides of the cavity, each mirror is composed of a taper and of a periodic section. The taper is located on the cavity side of the mirror and is made of four holes with increasing diameter (130, 170, 200, 200 nm) and separated by increasing distances (300, 320, 350 nm respectively). The periodic mirror is made of N holes (N=4 on the picture) with a diameter of 200 nm and a period of 370 nm. The inset presents a magnification of the tapered zone.

The native oxide is first removed by a short breakthrough with a CF_4 gas mixture. Then, the silicon native layer is etched with a HBr , Cl_2 , O_2 gas mixture, at a pressure of 4 mT. Finally, the resist is stripped by oxygen plasma. Then, each sample is manually cleaved in order to obtain optical facets. As an example, Fig. 1 presents a fabricated Fabry-Perot cavity where each mirror is composed of two sections. The periodic section of the mirror is formed of holes with identical diameter and with identification hole-separation distances. The tapered section is formed with four holes with different diameters and with periods decreasing as one approaches the cavity defect.

3. Optical resonance properties of the microcavities

After cleaving optical facets, the device is mounted on a XYZ translational stage regulated in temperature. TE-polarized light from a tunable laser source emitting from 1.45 μm to 1.59 μm is launched into the 9 mm long ridge access waveguide. Light is injected through the cleaved facets in waveguides. We use a polarization maintaining optical fiber. This optical fiber is chemically etched in order to obtain an end diameter of about 2 μm . After passing through the device, the light is collected by a x15 reflective objective. The waveguide output is then imaged, either onto an IR camera for observing light at the output of the cleaved facet, or onto an InGaAs photodiode for transmission measurements. Additionally, when using the photodiode, the imaging system incorporates a diaphragm and a polarizer in order to spatially filter inevitable spurious substrate-guided light. Sample is observed by a microscope with an angle of collection of 30°, which permits to collect the light escaping vertically from the structure. This light is guided via an optical fiber from the microscope objective onto another InGaAs detector.

Figure 2 presents the cavity-loss spectrum of the cavity with $N=7$. On the whole measurement range, the cavity exhibits a band gap with a sharp resonance at wavelength of 1574 nm. Fabry-Perot oscillations corresponding to the sample facets superimpose on the cavity mode signal and perturb cavity quality factor measurement. In order to separate both contributions, we acquire spectra at different temperature (see the two insets in Fig. 2). In the worst case, this effect could boost the estimation of the cavity Q, concluding to the observation of a Q factor as high as 80 000 ($T=21^\circ\text{C}$). The left-inset ($T=20^\circ\text{C}$) shows a width of the lorentzian peak of 27 pm, which correspond to a Q factor of 58000 in the less favorable case. Many measurements have been performed to estimate the Q value by varying the temperature, and we conclude that the Q is actually larger than 58000. Because the calculated modal volume is approximatively equal to $0.6(\lambda/n)^3$, we estimate that the O/V ratio is as high as $1.0 \cdot 10^5(\lambda/n)^3$.

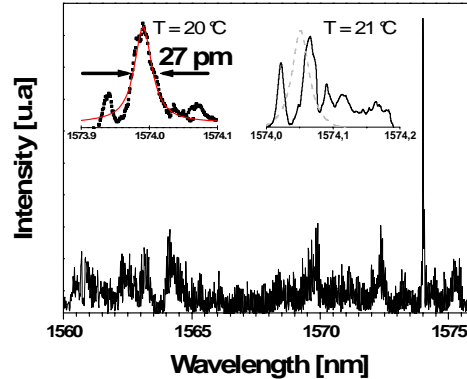


Fig. 2. Resonant cavity peak collected above the cavity. The insert details the resonant peak for two regulated temperature of the sample. Left-inset is fitted with a lorentzian curve replicated with a dashed line in the right-inset.

We have also performed measurements for other cavities for N ranging from $N=3$ to $N=7$. The spectra in Fig. 3 show the transmission of these cavities in black and the radiation losses measured by the top of the cavity in light grey. Transmission spectra through the device are normalized by a reference waveguide measurement. Spectra collected above the cavity show a resonant peak with the same spectral position and linewidth as observed in transmission spectra. This is consistent with the Fabry-Perot model [16] and gives a second check for the estimation of the Q factor.

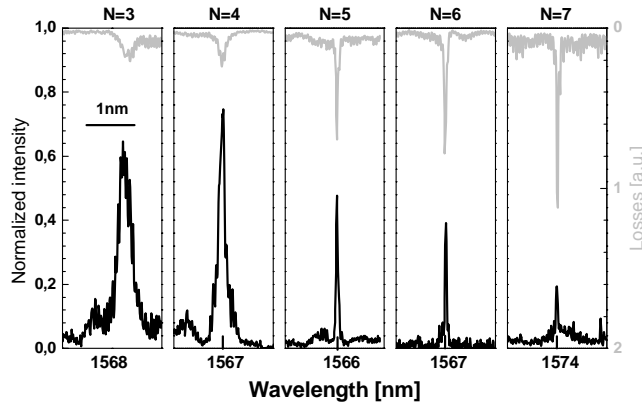


Fig. 3. Evolution of the resonant peak with increasing the number of holes in the periodic mirror (N). The black curve presents the normalized transmission across the cavities, the grey one shows the vertical losses collected by the top of the sample in arbitrary units with inverted axis.

As the number N of holes increases, the transmission peak (T_{\max}) at resonance shows a global significant decrease, meanwhile losses collected above the cavity increase (Fig. 3 and table 1). When the light is bouncing inside the cavity, it could experience two kinds of losses: In one hand, losses at each reflection due to the mode-profile mismatch and located at the tapered sections. This term is roughly constant and independent of the number of holes in the periodic section of the mirror. In a less significant way, the second source of loss corresponds to in-line losses due to the ridge waveguide roughness estimated to 6 dB/cm.

As the Q factors increase, both the number of reflections inside the cavity and the light path increase. This explains the decrease of T_{\max} and the increase of the light collected above the cavity.

Table 1. Experimental Cavity Q 's and T_{\max} for N ranging from 3 to 7 designed with the same tapering section.

N	$\lambda_r(\text{nm})$	Q_{exp}	$T_{\max}(+/-0.05)$
3	1568.22	2,700	0.6
4	1567.26	8,200	0.7
5	1569.09	19,000	0.5
6	1567.62	45,000	0.4
7	1574.00	58,000	0.2

4. Cavity performances

The experimental evolution of the Q factor with the number of holes N is represented in Fig. 4 with black dots and is compared with computational data obtained with a 3D fully vectorial Fourier modal method.

The 3D frequency-domain modal method used in this work for the computation is described in Ref.[17-18]. In brief, the method relies on an analytical integration of Maxwell's equations along the ridge-waveguide z -axis and on a supercell approach in the two others. Periodic boundary conditions with Perfectly-Matched-Layers implemented as nonlinear coordinate transforms are used in the orthogonal directions to carefully handle out-of-plane far-field radiations in the air and in the SiO_2 substrate. Since these layers absorb non-evanescent radiations, the electromagnetic fields are null on the boundaries of the supercell and are thus periodic functions of the z -coordinates. This allows to calculate the radiated and guided modes in a Fourier basis in each layer (the cylindrical bumps are discretized in a series of thin uniform layers) and to analytically integrate Maxwell's equations in the z -direction by relating recursively the modes amplitudes in the different layers using a scattering matrix approach [19]. The Q factors in Fig. 4 are computed by looking for the complex-poles $\tilde{\lambda}$ of the scattering matrix and by use of the relation $Q = \text{Re}(\tilde{\lambda})/2\text{Im}(\tilde{\lambda})$. In Fig. 5, in order to strongly reduce the computational loads, the Q 's are estimated by calculating the mirror modal reflectivity spectra [18]. From these values, we infer the cavity Q factors using a Fabry-Perot model. The latter has been shown to provide highly accurate predictions for Q for these cavities, see Ref. [13,14]. Convergence tests have been performed to estimate the accuracy of the computational results by increasing the number P of plane-waves retained for the computation. Stable results for the modal-reflectivity and for the Q values have been obtained for $P > 1000$, letting us expect a relative error below 1% for all calculated data. Thus the only approximation results from the spatial discretization (staircase profile) used to numerically encode the mirror holes.

Figure 4 shows that the Q factors (model and experimental) augment with N , which corresponds to the increase of the mirror reflectivity.

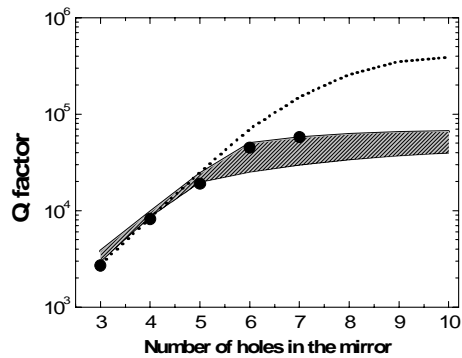


Fig. 4. Experimental (dots) evolution of the Q factor for the lineic Fabry-Perot cavity with increasing N . The shaded region represents the theoretical values for an increasing number of holes in the periodic mirror of the cavity and for a tolerance of ± 10 nm on the nominal value of the hole diameters. The dot curve shows the optimum Q factor value calculated for an optimal cavity length for each N .

The mirror (periodic section with N holes + tapered section) is defined by three intrinsic parameters: its modal reflectivity R_m , its modal transmittance T_m and its losses L_m , all linked by the relation $R_m + T_m + L_m = 1$. The losses L_m correspond to the mode profile mismatch at the taper and do not depend on N as already mentioned. Both experimental and calculated values saturate as N increase over 4-5 due to the losses located at the tapered section. The experimental Q factor values (dots) are included between two fitted models (grey zone) corresponding to a variation in the nominal hole dimensions of ± 10 nm. It shows the robustness of the cavities performances in association with realistic nanofabrication possibilities.

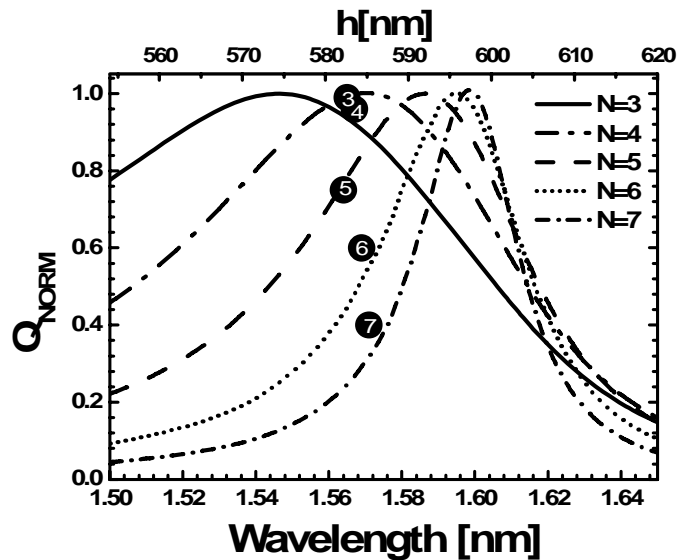


Fig. 5. Evolution of the normalized quality factor Q_{NORM} as a function of the resonant wavelength of for $N=3$ to $N=7$. The labeled numbers represent the experimental values ($Q_{\text{exp}}, \lambda_r$). h is the cavity length given by the relation $h = \lambda / n_{\text{eff}}$.

Figure 5 details the evolution of calculated Q_{NORM} factor (Q_{NORM} being the normalised Q factor obtained by dividing the actual Q by the maximum Q achievable with the same number N of holes) as a function of the cavity defect length h. On the same picture, the experimental values for the resonant wavelengths and Q factors have been added for N ranging from 3 to 7.

We first observe that the calculated Q_{NORM} optimum (curves in Fig. 5) is shifting and is getting sharper as N increases. This shift is due to the fact that the Q factors for $N < 4$ are mainly limited by the mirror transmission T_m , which is minimal for $\lambda = 1.55 \mu\text{m}$. For $N > 4$, the Q factor is limited by the losses L_m , which is minimal for $\lambda = 1.6 \mu\text{m}$. Thus the maximum of Q factor achievable is shifted from $1.55 \mu\text{m}$ to $1.6 \mu\text{m}$. Secondly, cavities have been designed and fabricated with a constant length h for all N's. The experimental cavity length allows to obtain Q factors close to the optimum Q_{NORM} for $N=3$ and $N=4$, but a progressively-increasing wavelength shift is obtained for larger N values. Finally, we report on Fig. 4 (dash-line) the theoretical evolution of Q factor calculated with the optimum h value for every N. Figure 5 additionally shows that the experimental Q factors can be further improved by adjusting the cavity length for each N values in order to have the optimal Q factor.

To conclude, with such a design optimization, cavity Q factor's could become closer and closer to the calculated value $Q=150,000$ for $N=7$ or $Q=400,000$ for $N=10$. Moreover, we note that the cavity geometry allows to achieve ultra-high Q/V on a SOI substrate over a broad spectral range (e.g. $Q > 58\,000$ over $\sim 40 \text{ nm}$ and $Q > 20\,000$ over $\sim 100 \text{ nm}$).

5. Conclusion

We report on experimental studies of Fabry-Perot microcavities with a tapered sections lying on a substrate. Cavity optical characteristics have been studied for an increasing number of holes in the mirror. This study shows the reliability of the modal adaptation concept and points the fact that large Q factor can be achieved over a wide spectral range of operation (compatible with U-DWDM) and thus could still be improved by adjusting the cavity defect length as a function of the number of holes in the mirrors. Q factor of 58000 with a modal volume of about $0.6(\lambda/n)^3$ have been demonstrated. This implies a Q/V of $1.0 \cdot 10^5 (\lambda/n)^3$ which is, to our knowledge, the highest Q/V value measured on a SOI substrate at telecom wavelengths.

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