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Visualization and analysis of jet oscillation under transverse acoustic perturbation

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Abstract

Schlieren flow visualizations of transverse oscillations of jets submitted to an acoustic perturbation are analyzed in this paper. The aim is to estimate the shape and the position of the median line of the jet. Two methods for image processing are proposed, based on complementary approaches : inter image and intra image analysis. Synthesized images of an oscillating jet are used to validate each method and compare their performances in the case of noisy pictures. Illustrations are then shown on real laminar and turbulent jets. The results obtained using both methods are very close, showing their reliability. Applications investigated in this paper are focused on the estimation of the convection velocity of perturbations along the jet, and the influence of the Reynolds number and of the channel geometry upstream the jet formation.

1 Introduction

In flute-like instruments, acoustic oscillation is generated by the coupling of the unstable modes of an air jet and the acoustic modes of a pipe resonator. For soft blowing conditions, the jet is laminar and the instability is usually described, following Rayleigh's approach ([1]), under assumptions of infinite inviscid 2-D flow. Certainly this approach needs to be combined with ad-hoc assumptions to cope with the specific geometry of

the problem (semi-infinite jet, acoustic transverse perturbation). Furthermore, because it is linear, this perturbation approach may be limited to small amplitudes of jet deflection. For many instruments like transverse flutes and popular music flutes, the sound power required calls for higher total jet flux. Reynolds numbers, based on jet thickness and velocity, up to 10000 have been estimated in transverse flutes. Under such conditions, the jet becomes rapidly turbulent downstream from the flue exit. The development of instability induced by the acoustic perturbation on such jets has been studied by Bechert ([2], [3]) and Fletcher ([4], [5]). Both propose semi-empirical models to describe the jet oscillations.

The intimate detail of the coupling between the acoustic perturbation and the jet instability remain an unsolved problem. It appears that for both laminar and turbulent jets, the lack of theoretical models make experimental data useful to fit, calibrate and evaluate semi-empirical models ([6]).

Different researchers have studied experimentally jet oscillations under acoustical perturbations using hot-wire anemometry measurements ([7], [8] for example). On the other hand, flow visualization has been widely used as an inspiration for a physical analysis and description of the fluid mechanisms and aeroacoustics at work in flutes ([9]).

In the present paper, we present tools for image analysis of flow visualizations to extract quantitative data on jet instability under acoustic perturbation. The development of instability on a jet is

experimentally investigated using a simplified device (see section 2): the pipe resonator is removed from the flute and replaced by an acoustic field generated by loudspeakers. Using the Schlieren technique, flow visualizations have been carried out for a variety of Reynolds and Strouhal numbers.

Two different image analysis techniques have been developed (see sections 3 and 4) and they are discussed in detail in this paper. The extracted data is analyzed in the framework of a harmonic perturbation that is convected downstream and grows in the shear layers of the jet (see section 5).

Finally, the influence of the Reynolds number and the channel geometry on the jet behavior are presented as an application in section 6.

2 Experiment description

Experimental setup: a jet, created by blowing through a slit, is acoustically forced by two out-of-phase loudspeakers (see figure 1). The speed of the

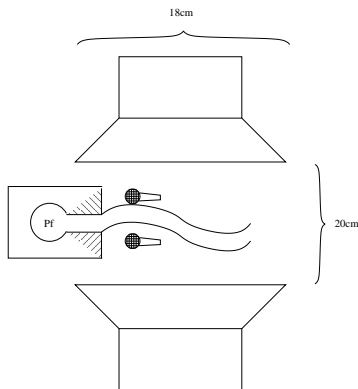


Figure 1: Experimental setup. Jet exit, speakers and two microphones (acoustic velocity estimation).

jet is controlled by varying the pressure in the cavity p_f just before the jet formation. The jet central speed at the channel exit U_b , can be estimated using Bernoulli's equation:

$$U_b = \sqrt{\frac{2p_f}{\rho_0}}, \quad (1)$$

where ρ_0 is the fluid density.

Jet structure: two Reynolds numbers $Re = 500$ and $Re = 3000$ were chosen ($Re \triangleq U_b h / \nu$, with $h = 10^{-3}$ m the channel height and ν the kinematic viscosity). They correspond to two different operating modes of the jet: $Re = 500$ gives a velocity around 7.5 m/s which corresponds to a normal blowing condition for a recorder and assures a laminar behavior, while $Re = 3000$ corresponds to a velocity around 45 m/s producing a turbulent jet.

The acoustic excitation frequency f is ranging from 70 to 1400 Hz (when $Re = 500$) and from 1200 to 2900Hz (when $Re = 3000$) to cover a Strouhal ($S_t \triangleq fh/U_b$) range from approximately 0.05 to 1.15. A fixed amplitude of the acoustic velocity is chosen for each of the two experiments described in the present paper and a typical value is 0.5% of the jet velocity¹. The acoustic velocity is measured using a Microflow velocity sensor (low amplitudes) and a microphone doublet (high amplitudes) at a position near the unperturbed jet path, but out of the flow visualization window. Preliminary experiment had been carried out to check the acoustic velocity homogeneity in the jet and sensor area.

Schlieren jet images: Schlieren technique ([10], section 3.2.2 p134) is used to observe the behavior of the oscillating jet: using an optical scheme, light phase shift crossing an inhomogeneous media is converted into light intensity (see figure 2). We use CO₂ jet traversing the air, whose mass density assures enough difference to allow Schlieren visualization (see figure 3) while producing a behavior close to that found in real flute-like instruments. Sequential images of the jet are taken with a digital camera synchronized with a stroboscopic light. Its frequency is set such that multiples of its frequency are slightly out of phase with the excitation frequency providing an aliased representation of the oscillation. Frequency of the camera was set to 14fps, exposure time to 1 μ s. Approximately 100 images are taken covering two cycles of jet oscillation. Images are captured in raw, black and white, bmp files with size 1280 x 448, and 8 intensity bits.

¹This is considerably lower than the 10% observed in real flutes but allows us to cover an interesting range of frequencies without over exciting the speakers.

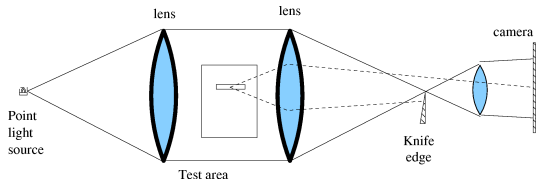


Figure 2: Schlieren basic implementation: a subset S of the test area with different medium (here the CO_2 jet) deviates light rays. A knife edge, placed in the focus of the second lens blocks part of the rays having crossed S , thus producing intensity variations on the screen (see figure 3).

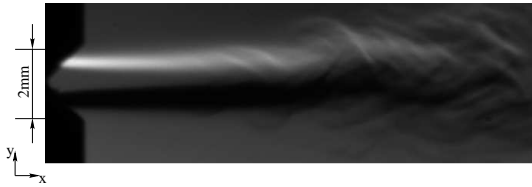


Figure 3: Schlieren jet image (see figure 2 for the optical principle).

3 Image processing

The goal of the image processing algorithm is to detect transverse jet displacement for every image in the oscillation period. Two algorithms are proposed in this section. Their performances will be checked and compared in section 4 and 5 respectively.

3.1 Cross-correlation method

A first algorithm based on cross-correlation between successive images is proposed.

Let us consider the intensity graph of one column of the image as shown in figure 4 (left picture). For that particular column, the shape of the graph does not change much as time goes on: the shape is only shifted, according to the transverse position η in the y direction due to the movement of the jet. However, the particular shape varies with the column considered since it is determined by the mass distribution of the jet as shown in figure 3.

Cross-correlation is calculated between two intensity graphs corresponding to the same column of two successive images of the sequence (see right part of figure 4). The position of the peak allows to

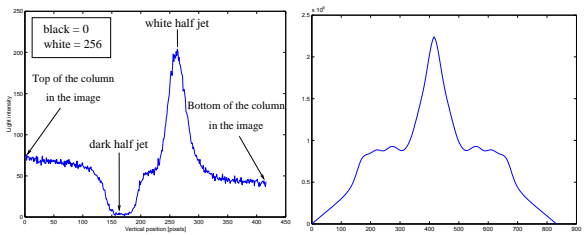


Figure 4: Intensity level of a single column from a Schlieren image (left) and cross-correlation of two intensity graphs corresponding to the same column in two successive images of the sequence (right).

measure the displacement of the jet between these two successive images. This is repeated for each column of the image. Since changes on the jet position may be smaller than one pixel, a parabola is fitted to the three highest points to estimate the position of the peak. When considering all the columns of all the images in the sequence, the jet position can be reconstructed as shown in figure 5 ($R_e = 500$ and $S_t = 0.2$).

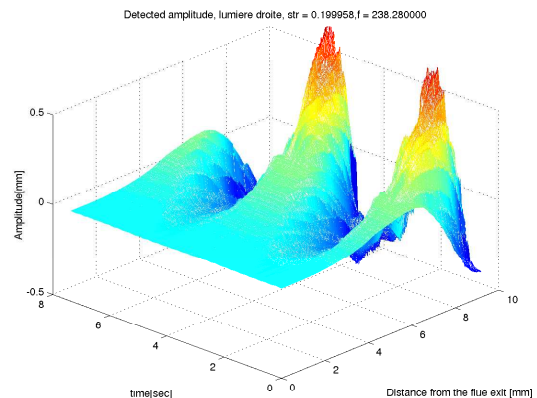


Figure 5: Jet deviation, as estimated after image analysis through cross-correlation approach, in the case $R_e = 500$ and $S_t = 0.2$

Some defects of the experimental setup are clearly visible in left part of figure 4: the two peaks corresponding to the brighter and darker part of the image should ideally be of the same height, but in practice a symmetrical contrast is very difficult to obtain. Moreover, unhomogenous background intensity (inside each image) is represented as a non horizontal line on the borders of the left image in figure 4. However, these features of the images are

useful for the cross-correlation since they help to produce the well shaped peak in the curve observed in the right part of figure 4.

3.2 Morphological method

The idea of this method is to apply morphologic functions on binarized images, in order to identify large spatial scales, corresponding to the jet main structure, while ignoring the smallest scales (vortices, background noise ...). This is done through the five following steps (also illustrated in figure 6):

Contrast enhancement and homogenization between all the images of a sequence (figure 6b): the contrast is first enhanced by histogram equalization; the histogram of each image is stretched to lie on the full 8-bit range, and to match a flat histogram. This also plays the role of contrast homogenisation between different images of a given sequence.

Conversion from greyscale to black and white images (figure 6c) : a statistical method based on the Otsu principle estimates the threshold which best separates the histogram within two classes ([11]). The binarization threshold is therefore different for each image. As a global method, the efficiency of the Otsu method is known to vary according to the type of image. A classical improvement is adopted, which consists in multiplying the Otsu threshold by an empirical constant in order to better enhance the jet structure for a given sequence of image. Typical values for this constant lie between 0.9 and 1.1. In the resulting BW images, the jet is represented by a lower and a upper half jet, black and white respectively (figure 6c). In the following, both half jets are treated separately : the same operations are applied to the BW image and to its 1-complemented image. For clarity, only operations on the image containing the lower half jet are shown in figures 6d, 6e and 6f.

Extraction of largest spatial scales in the image (figures 6d and 6e): for each half-jet, the black and white picture includes several black structures, among which the half jet. This image is usually noisy, with black dots or small-sized sets of black pixels on the background. This can result

either from a non-optimal threshold, or from the Schlieren experiment itself, which does not produce perfectly uniform backgrounds (mainly because the optical lens are never dispersion free). Therefore, a morphological closure ([12]) is performed to clean all small structures (figure 6d). Then a morphological opening is applied in order to highlight large scales in the image (figure 6e). The structuring element is a disk, the size of which (optimized manually), is the same for all the images of a given sequence.

Identification of the half-jet among the remaining large scales (figure 6f): The image is decomposed into different regions, defined as groups of contiguous pixels. A unique region, corresponding to the estimated half-jet, must be retained. However, since the jet is oscillating, sometimes with large amplitudes, its position may vary significantly between different images of the same sequence. Therefore the discriminating criterion retained, involves both the area and the localization of each region and uses the (known) main flow direction from left to right).

Jet edges and median line estimation : jet edges detection in figure 6f is trivial and is performed with Sobel algorithm which uses gradient information ([13]). Edge detection is interesting in order to analyse in further studies the spreading of the jet as a function of the distance from the exit. Moreover, it is an intermediate step to estimate the median line, which we are mainly interested in. Finally, an image containing edges of both half jets is scanned column after column and the median line is constructed point after point, including empirical criteria to select, among several possible paths, the one to follow. This guarantees that the resulting median line is single-valued, but possibly discontinuous in the case of vortices.

Structure length: The largest the distance from the exit, the most complex the structure of the jet, and the least reliable the estimation of the median line. An index of confidence is then used: the estimation of the median line stops at the distance (i.e. the column) corresponding to the length of the smallest half-jet. Indeed beyond that limit, median line estimation would rely on information

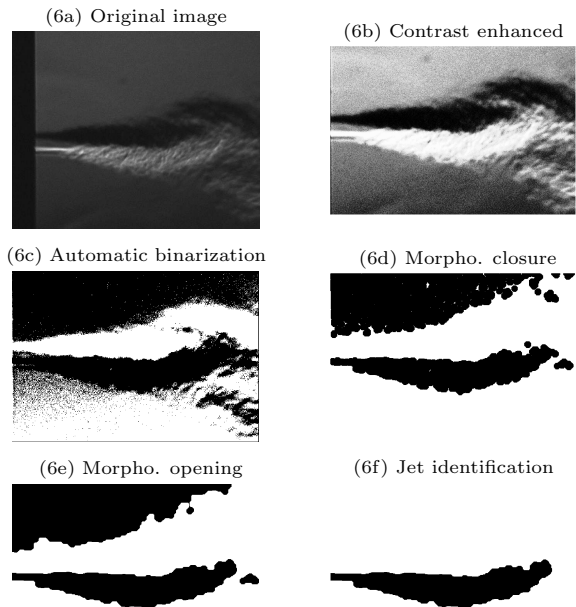


Figure 6: Morphological method: illustration of the different steps (from left to right and top to bottom).

given by a single half-jet (as can be seen in figure 7). This distance depends on the experimental conditions (Reynolds and Strouhal numbers) but obviously varies from an image to another within a sequence, depending both on the phase of the excitation (whether the jet is horizontal or deflected), and on the image itself (the whole process of jet identification being more or less efficient from an image to another).

The result of this method on one image is presented in figure 7. Bringing together the median line found for each image allows to construct 3D plots similar to those obtained through cross-correlation image analysis (figure 5).

4 Evaluation of both methods

Both methods are evaluated in this section: they are first validated through the use of computer made images (section 4.1) and their robustness against background noise is compared in section

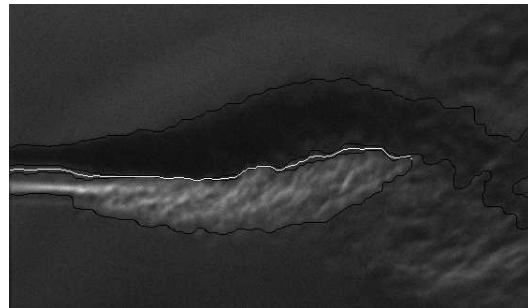


Figure 7: Original Schlieren image superimposed with edge detected (black line) and the median line deduced (white line).

4.2.

4.1 Validation with digitally synthesized jet movies

To validate both methods, the image analysis procedures described in section 3 are applied to digitally synthesized images of a jet (see figure 8).

The images have been synthesized to imitate Schlieren images of real laminar jets like the ones captured in our experiments: same lines and columns numbers, 8-bit intensity images, upper and lower shear layers of the jet respectively black and white, grey homogenous background.

The synthesized jet has an exponentially amplified sinusoidal motion with controllable parameters. It is checked for different parameters of the jet (jet width, amplification coefficient, frequency of oscillation) that both methods are successful (see for example a graphical confirmation in the first row of figure 8 where the median line is superimposed with the synthesized image).

4.2 Sensitivity to background noise

Since a real image is always noisy, it is worth testing the influence of noise on the image analysis results. To do this, white noise has progressively been added to the original synthesized image. This gives some insight on how algorithms behave when background noise is increasing and contrast is decreasing. Results are presented in figure 8 for different signal to noise ratio.

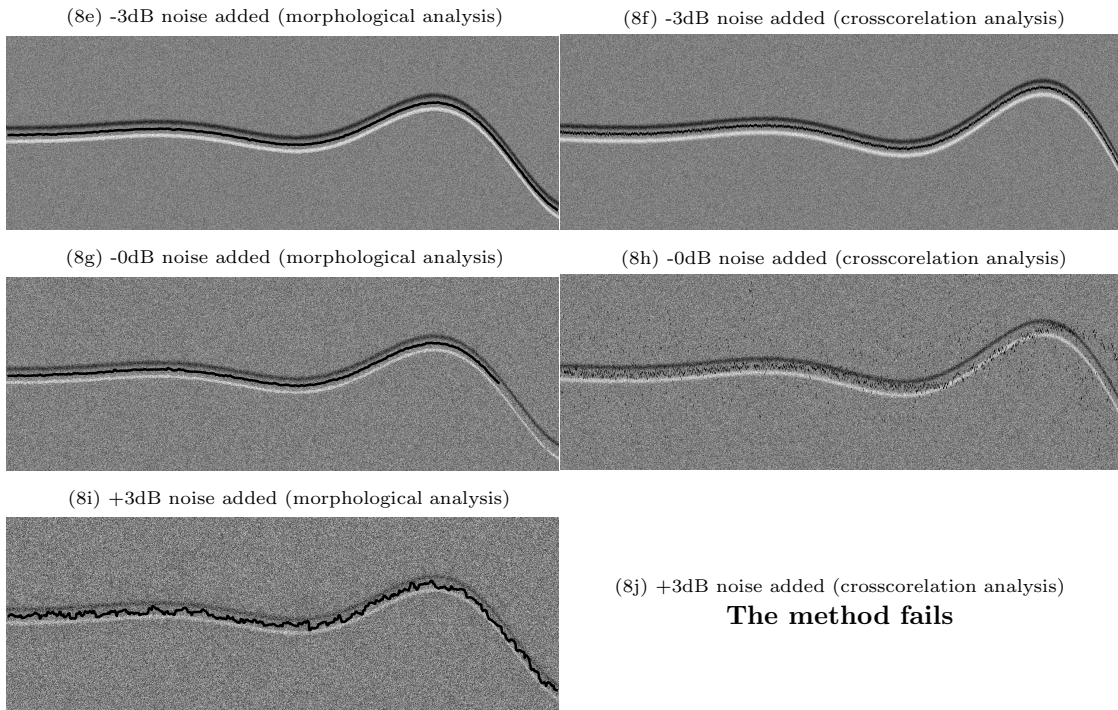


Figure 8: Influence of signal to (white) noise ratio on the estimated median line: comparison between morphological (left column) and crosscorrelation analysis (right).

The morphological approach (left column) appears to estimate successfully the median line on the whole image length until $-3dB$ of noise. When the noise ratio is increased to $0dB$, the median line is still estimated but not until the right border of the image. In the noisiest case ($+3dB$) the range on which the median line would have been estimated would be even shorter. To show how to prevent this, we have slightly modified the parameters of the analysis: the empirical constant multiplying the Otsu binarisation threshold is increased up to 1.5 for the upper half jet and decreased down to 0.5 for the lower half jet. Moreover, the radius of the structuring element for the closure has been divided by two. This allows to track the median line on the whole length by manual adjustment of the analysis parameters, but the estimation is somehow more crude.

The crosscorrelation method gives reliable results for moderate levels of noise but shows more sensitivity than the morphological method for the noisiest images. However, real Schlieren images obtained in our experiment are less noisy than the

extreme case tested here.

5 Results comparison

5.1 Data analysis

Every column of the images oscillates in time at the same frequency of the excitation. It is therefore possible to fit a sinusoid of that frequency to each column, and obtain the amplitude $|Y(f)|$ and phase $\angle Y(f)$ of the fitted jet transverse displacement:

$$Y(f) = \frac{1}{N} \sum_{k=0}^{N-1} X_k e^{-jk \frac{2\pi f}{f_s}}, \quad (2)$$

where f_s is the sampling frequency, N is the number of images in the sequence, X_k is the jet deflection for that column at image number k . These values $Y(f)$ are used to recreate a fitted version of the jet position as shown in figure 9.

In a linear description of the jet ([14], [15]), the perturbation is amplified while being convected

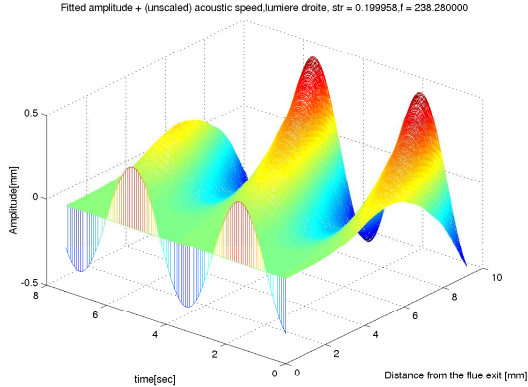


Figure 9: Fitting of a sinusoidal model (cf. Eq. (2)) on the data plotted in figure 5. The wave superimposed at the flue exit corresponds to the perturbing acoustic velocity. It is plotted for phase reference.

downstream. The perturbation travels at a velocity about one half of the jet speed. Inspired from this theory, the experimental data can be analyzed assuming a jet transverse displacement η following ([16]):

$$\eta(x, t) = \Re \left(\eta_0 e^{\gamma x} e^{i\omega(t-x/c_p)} \right) \quad (3)$$

where η_0 represents a complex initial amplitude of the oscillation, γ is the spatial growing rate, c_p is the convection velocity and x is the distance from the flue exit.

The growing rate γ can be estimated by fitting an exponential to the detected amplitude curve. The fitting is performed on a range of distances from the flue exit which is chosen as follows: the starting point corresponds to the minimal resolution obtained with the two methods (that is half a pixel for the morphological approach) whereas the last point considered is such that the oscillation amplitude reaches 80% of the maximum oscillation amplitude estimated by the morphological method. This upper limit was found empirically to correspond to the limit above which an exponentially growing model is no more relevant.

The convection velocity c_p of the perturbation can be estimated as the slope of the linear fitting to the phase (on the same fitting range as for the estimation of the growing rate γ) as shown in figure 10 for the cross correlation method and the

morphological method, in the case of a laminar jet ($Re=500$, left column), and for a turbulent jet ($Re=3000$, right column).

5.2 Methods comparison

5.2.1 Laminar jet

A laminar jet ($Re=500$) is first considered. We display in the left column of figure 10 amplitude and phase of the sinusoidal fit of the jet displacement. The two methods show very similar results:

- the oscillation amplitude follows roughly an exponential up to a distance of $x/h \approx 11$ where h is the thickness of the slit.
- the phase shift of the oscillation decreases roughly linearly downstream from flue exit, corresponding to the delay induced by the convection of the perturbation on the jet at a somehow constant velocity.

5.2.2 Turbulent jet

The case of a turbulent jet ($Re=3000$) is now investigated, for a similar Strouhal number ($St = 0.21$). Here again, the two methods give similar results (see figure 10, right column). It should be pointed out that, due to the lower relative acoustic excitation amplitude in the turbulent case ($v_{ac}/U_j = 2.7 \cdot 10^{-3}$, compared to $v_{ac}/U_j = 5 \cdot 10^{-3}$ in the laminar case), the transverse jet displacement is much smaller on the right column of figure 10 than on the left column ($\eta_{max}/h \approx 0.3$ compared to $\eta_{max}/h \approx 0.8$). Analyses in the right column of figure 10 therefore correspond to a very severe case of a turbulent jet with very small transverse displacement. Regarding the phase shifts, a downward bending is observed, as expected in the case of a rapidly slowing turbulent jet.

5.2.3 Singular flow behavior

For some conditions, the flow instability moves away from the simple exponential model described in the previous section. For laminar condition, this is the case for the roll-up of vortices as well as for the development of varicose modes on the jet.

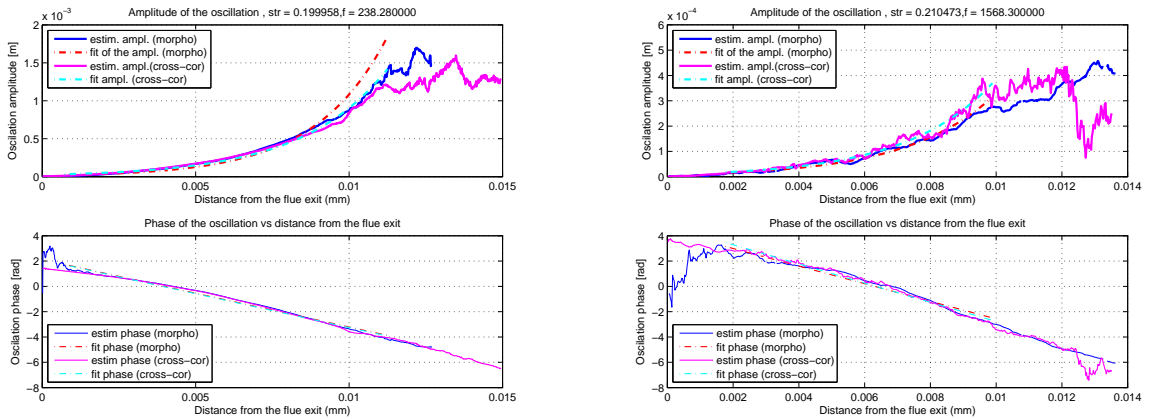


Figure 10: Amplitude (top) and phase (bottom) of the jet transverse displacement using the cross correlation method (pink line) and the morphological method (green line). In the left column, the jet is laminar ($Re=500$, excitation frequency 238 Hz, i.e. $St=0.195$). In the right column, the jet is turbulent ($Re=3000$, excitation frequency is 1568 Hz i.e. $St=0.21$).

Roll-up of the jet: In the case of strong jet amplification, the accumulation of the vorticity in the jet shear layers at the inflexion points induces the formation of vortices: as a result, the jet breaks into an alternated vortex street ([17]). Depending on the Reynolds number, this vortex street may rapidly be decomposed by turbulence. Even if the cross correlation appears to track the jet transverse displacement further downstream than the morphological method, figure 11 (left column) shows that both analysis methods used are affected by this vortex formation.

Developpement of varicose modes: Depending on the symetrical properties of perturbations on both shear layers of the jet, the jet oscillation can be sinuous or varicose. Sinuous oscillations are characterised by a transverse displacement of the jet while varicose oscillations correspond to an oscillation of the jet thickness ([15]). Even if sinuous modes appear to be dominant ([18]) in flute-like instruments, varicose contributions can sometime be observed related to fluctuations in the jet velocity. In the case of the presence of varicose oscillation on the jet (see figure 11, right column), the morphological method appears to track the jet median line further downstream than the cross-correlation method.

A partial conclusion of these examples above is

that, in both cases, the bias between results of the two methods is an indication for singular flow behavior.

6 Selected results on the jet behavior

Two applications of the proposed methods are presented within this section.

6.1 Influence of the Reynolds number on the convection velocity

The results obtained with cross-correlation and morphological methods can be compared in a more general way by considering the evolution of the estimated parameters as function of the frequency in the case of a laminar (figure 12) and a turbulent (figure 13) jet. The mean convection velocity of the perturbation on the jet (defined as the mean slope of the phase shift) appears to be nearly independent of the frequency of oscillation. This is true for a laminar jet as well as for a turbulent jet. In the former case, $c_p/U_b \simeq 0.4$ and in the latter $c_p/U_b \simeq 0.3$. These results have to be compared with the Rayleigh ideal linear jet for which c_p/U_b varies between 0.3 and 0.5 depending on the jet

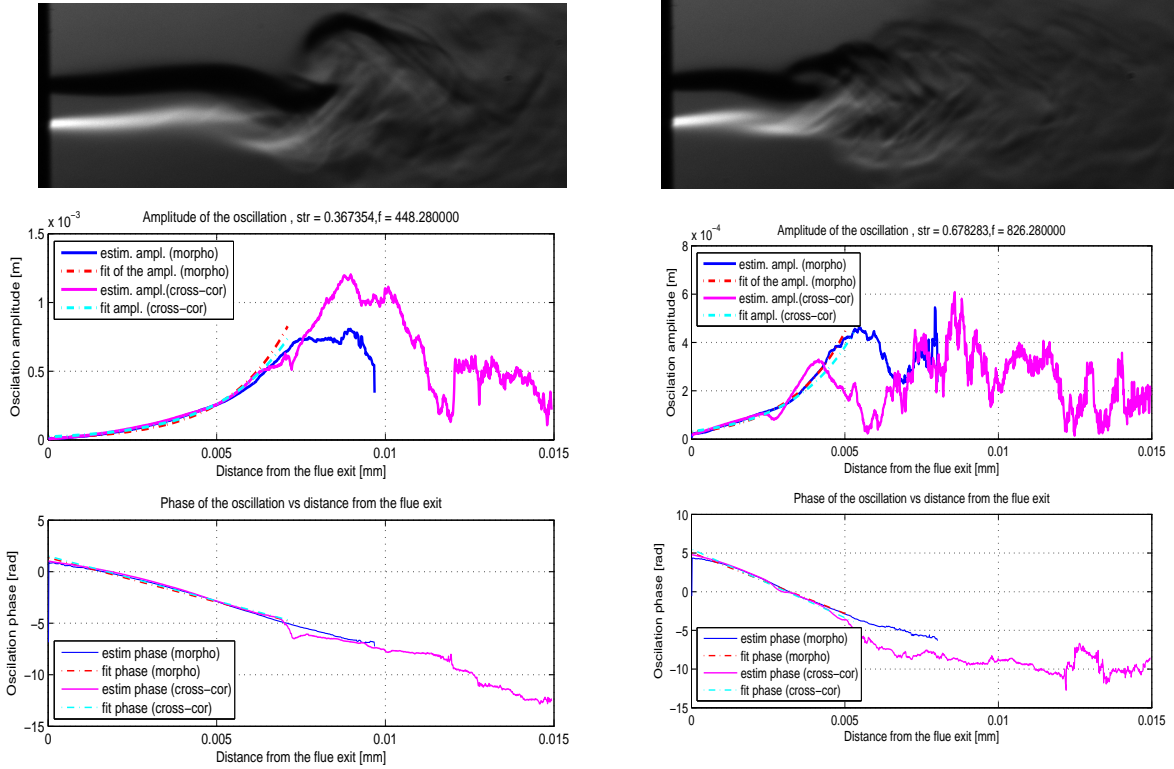


Figure 11: Two illustrations of singular flow behaviours (one image of the sequence (top) and analysis results). Left column: roll-up of the jet ($Re=500$, $St=0.36$). Right column: development of varicose modes on the jet ($Re=500$, $St=0.68$).

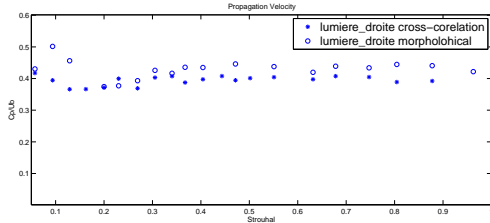


Figure 12: Convection velocity of the perturbations on the jet as estimated through cross-correlation and morphological methods, laminar jet ($Re=500$).

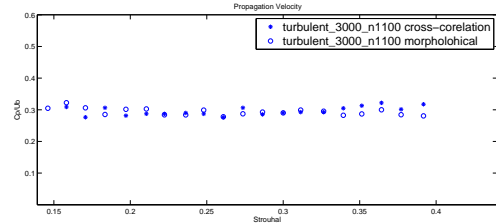


Figure 13: Convection velocity of the perturbations on the jet as estimated through cross-correlation and morphological methods, turbulent jet ($Re=3000$).

velocity profile. The values found are also in agreement with values suggested by other authors ([15], [7]).

A closer look at the evolution of the phase with the distance x from flue exit indicates a higher convection velocity at short distances from flue exit (a downward bending is observed). This can be interpreted both in terms of the slowing down of the jet velocity and of the smoothing of the jet velocity profile, both induced by the viscosity. A fit of

the phase with a power law reveals that the speed of the jet decreases as a function of $x^{-0.33}$ in the laminar case (mean value obtained from all the excitation frequencies available) and as a function of $x^{-0.53}$ in the turbulent case (mean value on all excitation frequencies also). From [19] (p133 and p323) the jet centerline velocity in the laminar case is expected to decrease as $x^{-1/3}$, while the decrease is much faster in the case of a turbulent jet since

the jet centerline velocity follows $x^{-1/2}$. The fitted values appear to be very close to the theoretical values, even if it should be noted that the dispersion around the mean value is important, due to experimental problems for some frequencies. However, this approach appears promising and could be extended to tackle the detection of the transition from laminar to turbulence in a jet.

6.2 Influence of the channel geometry on the convection velocity

Another application of the methods presented can be illustrated by the comparison of different flue channel geometries, as studied by Segoufin [20]. Convection velocities of perturbations on jets issuing from long (27mm) and short (1mm) channels are compared. Both channels show the same thickness $h = 1\text{mm}$. In the case of the short channel with squared exit, the convection velocity is clearly higher than in the other cases, confirming the observations done by Ségoufin [20] in the context of edge-tones. This can be interpreted, as suggested by Ségoufin, in terms of the boundary layers' thickness of the jet, which becomes thinner in the case of short channel. The present experiment was carried using the channels also used by Segoufin, and our results strongly correlate with Segoufin's results and interpretation.

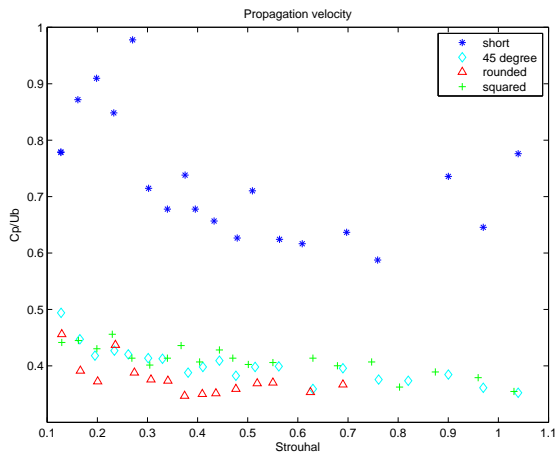


Figure 14: Dimensionless velocity, flue exit short (dashed), squared (dashdot), rounded (solid) and 45 degrees (dotted).

7 Conclusion

Compared to hot-wire anemometry, flow visualization allows a non intrusive measurement as well as a clear identification of the jet as composed of fluid particles issuing from the flue channel (streaklines, [21]). On the other hand, flow visualizations does not give direct information on the velocity field (streamlines) and requires the use of a gas of different light refraction than that of the surrounding air.

The images obtained by the Schlieren method are extremely sensible to variations on the setup. The position of the blade, the aperture of the diaphragm, the alignment of the optics, the saturation curve of the acquisition software, the vertical and horizontal position of the jet, etc. are some of the parameters that needs to be adjusted for each experiment. Small differences on these parameters produce image variations. Therefore, even under a attentive care, images obtained from any two experiments are different.

Both methods allow to estimate fairly well the amplitude as well as phase evolution of the perturbation. The main difference is that the cross-correlation method performs an inter-image analysis while the morphological method is an intra-image technique. Moreover, to achieve its best results the morphological method needs to be manually calibrated for each sequence of images while the cross-correlation method can be completely automate. The resolution of the detection is restricted to one pixel in the morphological method while continuous for the cross-correlation. Turbulent jet and noisy images seem to be better handled by the morphological method while the cross-correlation is preferred for laminar jets.

The slowing down of the jet can be quite accurately evaluated, and appears to follow the theoretical values expected for both laminar and turbulent jets.

The two methods we developed give very close results in terms of jet amplification and convection velocities for a wide range of control parameters. Together with the interpretation of results presented by Segoufin using the same channels, this indicates that both methods can be reliable and useful to the study of jet oscillation in edge-tones and flute-like instruments.

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