Physically-based modelling of hydrological processes in a tropical headwater catchment in Benin (West Africa) ? process representation and multi-criteria validation

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**Hydrology and
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Physically-based modelling of hydrological processes in a tropical headwater catchment in Benin (West Africa) – process representation and multi-criteria validation

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Title Page

Abstract	Introduction
Conclusions	References
Tables	Figures

|◄ | ►|

◄ | ►

Back | Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion

EGU

Title Page

Abstract | Introduction

Conclusions | References

Tables | Figures

◄◄ | ►►

◄ | ►

Back | Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion

EGU

Abstract

The aim of the study was to test the applicability of a physically-based model to simulate the hydrological processes in a headwater catchment in Benin. Field investigations in the catchment have shown that lateral processes as surface runoff and interflow are most important. Therefore the 1-D SVAT-model SIMULAT was modified to a hillslope version (SIMULAT-H). Due to a good database the model was evaluated in a multi-criteria validation using discharge, discharge components and spatially distributed soil moisture data. For the validation of discharge good results were achieved for dry and wet years. Main differences were observable in the beginning of the rainy season. The comparison of the discharge components determined by hydrochemical measurements with the simulation revealed that the model simulated the ratio of groundwater fluxes and fast runoff components correctly. For the validation of the discharge components of single events larger differences were observable, which was partly caused by uncertainties in the precipitation data. The representation of the soil moisture dynamics by the model was good for the top soil layer. For deeper soil horizons, which are characterized by higher gravel content, the differences between simulated and measured soil moisture were larger.

Concerning the runoff generation processes a good agreement of simulation results and field investigations was achieved. On the upper and the middle slope interflow is the predominant process, while at the bottom of the hillslope groundwater recharge and – during the rainy season – saturated overland flow are important processes.

1 Introduction

In the past decades significant progress has been achieved in understanding and modelling hydrological processes. The bulk of hydrological process research was carried out in temperate climate zones while in tropical zones only a few field investigations concerning hydrological processes were effected. Bonell and Bruijnzeel (2005) sum-

marize the research activities concerning hydrology in the humid tropics with special regard to human activities. According to their publication most investigations concerning runoff generation processes in tropical forests were carried out in South and Central America, Australia and South-East Asia. Particularly in the Amazon catchment in Brazil

5 intensive process studies were effected by Elsenbeer et al. (1992), Elsenbeer and Lack (1996), Sobieraj et al. (2002) and Elsenbeer and Vertessy (2000). Most studies in the humid tropics revealed that lateral processes – mainly subsurface stormflow (interflow) – are predominant in tropical forest ecosystems. In West Africa only few studies concerning hydrological processes – particularly in Nigeria and the Ivory Coast – were

10 carried out (Jeje et al., 1986; Ogunkoya and Jenkins, 1993; Chevallier and Planchon, 1993; van de Giesen et al., 2000).

   Due to the poor database the experience with hydrological modelling is relatively low in West Africa. Often conceptual models with low input data requirements are used, because a parameterization of physically-based models is not feasible with the available

15 data. Examples of successful applied conceptual hydrological models are the utilization of the HBV-model in Senegal of Andersen et al. (2001), investigations with the conceptual UHP-model in Benin (Bormann and Diekkrüger, 2004) and a TOPMODEL-application in Nigeria (Campling et al., 2002). The first application of an intermediate approach between a conceptual and a physically-based model was presented by

20 Varado (2004) for the Donga catchment in central Benin, but the development of the model was not finished. In other humid tropical regions as South America physically-based hydrological models were applied successfully for instance from Vertessy and Elsenbeer (1999) and Vertessy et al. (2000).

   This study is part of the IMPETUS-project (Speth et al., 2002), which analyses the

25 impact of Global Change on the water cycle in Benin and Morocco.

   The aim of this study is to test the applicability of the physically-based model SIMULAT-H to simulate the hydrological processes in the sub-humid tropical environment of West Africa with special regard to the process description. The process knowledge obtained by field studies was used to enhance the model which was intensely

tested using own field data. The objective is a thorough understanding of the hydrological processes and its influencing factors in the target region to be able to forecast the effect of Global Change on the water cycle. For this purpose the model must be able to consider the spatial distribution of soils and vegetation and their temporal dynamic.

5 The runoff generation processes have to be studied carefully to be able to predict the ratio of slow and fast runoff components in Global Change scenarios, which imply land use and climate change.

Based on field studies of the hydrological processes the model results are evaluated with special regard to the process description. To analyse the difference in runoff

10 generation processes in catchments with different land cover a catchment with natural vegetation and a catchment which is strongly influenced by agricultural activities are taken into account.

2 Study site

In this study different sub-catchments of the Aguima catchment ($30\,km^2$), which is lo-

15 cated in central Benin (Fig. 1), were investigated. The Aguima catchment was intensively investigated in terms of hydrology (Giertz, 2004), hydrogeology (Fass, 2004), soil properties and soil degradation (Junge, 2004), vegetation (Orthmann, 2005) and agriculture (Mulindabigwi, 2005; Dagbenonbakin, 2005) within the IMPETUS-project (Speth et al., 2002). Therefore a good database for model parameterization and vali-

20 dation was available.

The catchment is located in the sub-humid Sudan-Guinea-Zone, which is characterized by a unimodal rainy season from May to October. The mean annual precipitation of the region is 1100 mm while the mean temperature is 26.4°C. Typically monsoonal rainfall with a long duration and low intensities are of minor importance in the study

25 area. Most of the precipitation comes from squall lines which results in a short period of high intensive rainfall followed by a longer tail with low intensities. Because the origin of the rainfall is the Jos plateau in Nigeria, the severe rainfalls arrive during night when

the measurement of the discharge is dangerous. Therefore, for peak flows only water level measurements are available.

River discharge occurs periodically during the rainy season, while from December to May the rivers dry out. In small rivers, the time between the peak of rainfall and the peak of discharge is extremely short. Over bankfull discharge is common, resulting in problems relating water level measurements to discharge. Because the actual evapotranspiration is about 800 mm/yr, the total discharge is only about 20% of the precipitation.

The main soil types of the catchment are Lixisols and Acrisols according to the World Reference Base classification (ISSS Working Group RB, 1998). Concerning geomorphology the catchment is characterized by a flat, undulating pediplain relief with altitudes from 255 to 333 m above sea level. The underlying rock is migmatite, which is weathered to clayey saprolite. In the headwater catchment swampy depressions – called inland valleys – can be found. These landscape features are the primary drainage system of the African Precambrian basement complex and can often be found on deeply weathered granitic and metamorphosed rocks. As often in West Africa, two aquifers do exist. A fractured rock aquifer is found in depths below 20 m. Near the surface a shallow saprolite aquifer is observed with a fluctuating groundwater level related to the rainfall pattern. The latter aquifer is often used for water supply and is replenished during the rainy season.

The vegetation is mainly composed of woodland and savannah. In the southern part of the catchment agricultural land use is predominant.

To analyse the processes as well as to develop and to validate the hydrological model three sub-catchments were taken into account. These sub-catchments are characterized by different land cover types (Table 1). Due to its location close to a small village, the Niaou catchment is more intensively used for agriculture. The pedological investigations of Giertz and Diekkrüger (2003), Junge (2004), Giertz (2004) and Giertz et al. (2005) revealed that the human impact has a strong influence on soil properties and hydrology of the catchment.

The instrumentation and the available data-sets of the catchment are described in Sect. 5.

3 Hydrological processes

The runoff generation processes are mainly determined by soil properties and land cover. In the following section the soil properties of a typical soil catena of the Upper Aguima (savannah and woodland) and the Upper Niaou catchment (agricultural fields) are described.

According to Junge (2004) Lixisols and Acrisols are the prevailing soils in both catchments. They mainly occur on the middle part of the hillslope. These soils are characterized by loamy sand in the ochric horizon, by clay accumulation in an argic horizon and by plinthitic gravel as evidence of the accumulation of iron compounds. The shallow Plinthosol occurs near the drainage divide and at the bottom of the hillslope. They are defined by a subsurface layer containing an iron-rich mixture of clay minerals (chiefly kaolinite) and silica that hardens on exposure into in impermeable ironstone crust. This crust occurs mostly at 30 to 60 cm depth, which depends on erosion and accumulation processes. The texture of the topsoil layer is loamy sand.

The Gleysols are predominant in inland valleys. Regarding soil physical properties two types of Gleysols can be distinguished in the area of investigation. At the border of the inland valleys the sandy Gleysol is the main soil type, while in the centre often soils with a clayey texture are prevalent. In the riparian zone the Fluvisol, composed of alluvial sands, is the predominating soil type.

Although the texture of the top-soil of the different soil types is relatively uniform (mostly loamy sand), the in-situ measurements of the saturated conductivity revealed a high variability. The differences are mainly caused by different land use, which strongly influences the soil physical properties (e.g. macroporosity due to biological activity), as it was shown by Giertz (2004), Giertz et al. (2005) and Junge (2004). These investigations revealed for instance that on savannah plots a mean density

Physically-based hydrological modelling in Benin

S. Giertz et al.

Title Page

Abstract	Introduction
Conclusions	References
Tables	Figures

◄ | ►

◄ | ►

Back | Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion

EGU

Physically-based hydrological modelling in Benin

S. Giertz et al.

of 219 macropores/m^2 was observable, and only 5 (cotton), 8 (yam) and 60 (maize) macropores/m^2 were existent on agricultural fields (Giertz et al., 2005). The impact of the macroporosity on the infiltration process was shown by in-situ measurements of the saturated conductivity. On agricultural fields the K_{sat}-value was two to five times
5 (depending on soil type) lower than on savannah/woodland vegetation. Therefore for the surface runoff generation process the land use is one of the most important factors.

The runoff generation processes in the subsoil are more related to the soil types, as the soil physical properties vary strongly between them. The permeability of the subsoil is relatively low for Lixisols/Acrisols (mean: 21.1 cm/d) and especially for Plinthosols
10 with the nearly impermeable ironpan crust (Giertz, 2004).

Based on the soil investigation and the land use types the prevalent runoff generation processes for the hillslope units of the two catchments can be characterized as listed in Table 2. Figure 2 shows the flow paths for the Upper Aguima and the Upper Niaou catchment as derived from the soil investigations, hydrogeological investigations from
15 Fass (2004) and field observations. In the Upper Aguima catchment surface runoff occurs only on pathways (Hortonian overland flow) or at the bottom of the hillslope (saturated overland flow), when the inland valley is saturated during the rainy season. But as inland valleys only occur at 1/3 of the channel length of the Upper Aguima, this process is not as important as in the Upper Niaou, where the whole river is character-
20 ized by inland valleys (Giertz and Diekkrüger, 2003). Due to the high macroporosity in soils of natural savannah and woodland vegetation, the infiltration rates are very high. The low permeability of the subsoil of Lixisols and Plinthosols results in subsurface flow processes, which can be considered as the prevailing processes on the hillslopes. In the Upper Niaou catchment the amount of surface runoff is higher due to low infiltration
25 rates on fields. The generated surface runoff – often flowing concentrated on pathways – infiltrates at the bottom of the hillslope in the sandy Gleysol at the border of the inland valley. This process contributes to the saturation of the inland valley during the rainy season. After saturation of this area, saturated overland flow occurs.

Due to higher surface runoff amounts and lower evapotranspiration (Giertz et al.,

EGU

2005) the discharge amount is higher in the agricultural catchment, which is shown in Table 3. Mainly in dry years like the year 2001 the differences between the catchments with natural vegetation and with agricultural land use is high.

4   Model approach

The analysis of the hydrological processes revealed that lateral processes as interflow and surface runoff are the major runoff generation processes in the catchment. Consequently the incorporation of lateral flow processes into the modelling approach is essential for an adequate process description.

To simulate the hydrological processes the physically-based 1-D SVAT-model SIMULAT (Diekkrüger and Arning, 1995) was modified to a hillslope version SIMULAT-H. The model structure of the 1-D-model and the modified model is shown in Figs. 3a and b.

In SIMULAT-H hillslope processes are taken into account. The hillslope is subdivided in a number of subunits. The simulated surface runoff of the upslope unit is considered as additional water input at the soil surface on the downslope subunit.

The algorithms to calculate the evapotranspiration, soil water fluxes and the lower boundary condition are taken from the 1-D-model SIMULAT. In the following sections the algorithms of the major processes are described. The complete model description can be found in Giertz (2004).

To simulate base flow, a conceptual, linear groundwater model was linked to SIMULAT-H. Because no overland flow routing was integrated in SIMULAT-H, the discharge is simulated as the superposition of the single runoff components. Because validation is performed at a daily time step and the reaction time is within hours this simplification is assumed to be acceptable.

EGU

4.1 Evapotranspiration

In this section the following terms are used:

ET_{pot} = potential evapotranspiration [kg $(m^2 s)^{-1}$]

5 Δ = slope of the saturation vapour pressure temperature relationship [–]

λ = latent heat of vaporisation [J kg^{-1}]

c_p = specific heat of the air [1005 J $(kg K)^{-1}$]

$(e_s - e_a)$ = vapour pressure deficit of the air [hPa]

γ = psychrometric constant [0.68 hPa K^{-1}]

10 r_s = bulk-stomata resistance [s m^{-1}]

r_a = aerodynamical resistance [s m^{-1}]

R_n = radiation balance [W m^{-2}]

G = soil heat flux [W m^{-2}]

LAI = leaf area index [–]

15 E_{pot} = potential evaporation [kg $(m^2 s)^{-1}$]

E_{act} = actual evaporation [kg $(m^2 s)^{-1}$]

E_{max} = maximum evaporation [kg $(m^2 s)^{-1}$]

ξ = soil factor [–]

i = days since a defined minimal precipitation [d]

20 T_{pot} = potential transpiration [kg $(m^2 s)^{-1}$]

$\tau(\psi, z)$ = reduction factor [–]

ψ_1 = minimal matrix potential, where water uptake of the roots occurs [hPa]

ψ_2 = matrix potential, where a reduction of the water uptake of the roots starts [hPa]

ψ_3 = wilting point [hPa]

EGU

The potential evapotranspiration is calculated with the Penman-Monteith equation:

$$\lambda ET_{pot} = \frac{\Delta(R_n - G) + c_\rho \frac{e_s - e_a}{r_a}}{\Delta + \gamma\left(1 + \frac{r_s}{r_a}\right)} \tag{1}$$

To calculate the actual evapotranspiration the potential evapotranspiration is primarily separated in evaporation (E_{pot}) and transpiration (T_{pot}) based on the leaf-area index (Ritchie, 1972):

$$E_{pot} = ET_{pot}e^{-0.4LAI}$$
$$T_{pot} = ET_{pot}\left(1 - e^{-0.4LAI}\right) \tag{2}$$

The actual evaporation is computed with the empirical approach of Ritchie (1972). Two cases are distinguished:

1. Until the maximum of evaporation (E_{max}) is achieved the actual evaporation is equal to the potential evaporation

2. After the attainment of E_{max} the actual evaporation declines continuously with time. The soil factor ξ, which depends on the clay content of the soil, determines the decrease rate of the actual evaporation.

$$E_{act} = \begin{cases} E_{pot} & \text{for } E_{pot} < E_{max} \\ E_{max} & \text{for } E_{pot} \geq E_{max} \end{cases}$$

$$E_{max} = \begin{cases} \xi(\sqrt{i} - \sqrt{i-1} & \text{if } \sum E > 9(\xi-3)^{0.42} \\ \infty & \text{if } \sum E \leq 9(\xi-3)^{0.42} \end{cases} \tag{3}$$

To determine the actual transpiration the approach of Feddes et al. (1978) is implemented in SIMULAT. The potential transpiration T_{pot} is reduced by the factor τ, which

EGU

is calculated depending on the matrix potential.

$$\tau(\psi, z) = \begin{cases} 0 & \text{for } \psi > \psi_1 \vee \psi \leq \psi_3 \\ 1 & \text{for } \psi \leq \psi_1 \wedge \psi \geq \psi_2 \\ \frac{\psi - \psi_3}{\psi_2 - \psi_3} & \text{for } \psi < \psi_2 \wedge \psi > \psi_3 \end{cases} \qquad (4)$$

4.2 Infiltration and surface runoff

The infiltration rate is computed with a semi-analytical solution of the Richard's equation based on Smith and Parlange (1978):

$$f = K_{sat} \frac{e^{F/B}}{e^{F/B} - 1} \qquad (5)$$

With the cumulative infiltration rate defined as:

$$B = G(\theta_s - \theta_i) \qquad (6)$$

with

f = infiltration rate [cm d^{-1}]
F = cumulative infiltration [cm]
G = capillary drive [hPa]
θ_s = saturated water content [cm^3 cm^{-3}]
θ_i = initial soil water content [Vol-%]
K_{sat} = effective saturated hydraulic conductivity [cm d^{-1}]

To take into account the high variability of the saturated conductivity a log-normal distribution of the K_{sat}-values is considered. A certain number of K_{sat}-values are chosen using the Latin-Hypercube method (MacKay et al., 1979). For the determined values the Smith-Parlange equation (Eq. 5) is calculated. The mean of all calculations is considered as infiltration rate of the soil matrix.

Physically-based hydrological modelling in Benin

S. Giertz et al.

Title Page

Abstract | Introduction

Conclusions | References

Tables | Figures

|◀ | ▶|

◀ | ▶

Back | Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion

EGU

4.3 Soil water fluxes

In this section the following terms are used:

θ = volumetric water content [cm^3 cm^{-3}]

5 ψ = matrix potential [hPa]

Q = Q(z,t) = sources and sinks [cm^3 cm^{-3} d^{-1}]

z = depth under soil surface [cm]

$K(\theta) = K_r\, K_{sat}$ = hydraulic water conductivity [cm d^{-1}]

K_r = relative hydraulic water conductivity [–]

10 K_{sat} = saturated hydraulic water conductivity [cm d^{-1}]

$C(\psi)$ = specific water capacity [cm^3 cm^{-3} hPa^{-1}]

The soil water fluxes are calculated based on Richards's equation:

$$C\left(\psi\right)\frac{\partial \psi}{\partial t} = \frac{\partial}{\partial z}\left(K\left(\theta\right)\frac{\partial}{\partial z}\left(\psi - z\right)\right) + Q \tag{7}$$

15 For the mathematical description of the soil-water-retention curve the approach of Brooks and Corey (1964) is used.

Interflow

20 The interflow is considered as a sink in the Richard's equation. The lateral flow is the product of the lateral conductivity $K_{sat,lat}$ and the slope α:

$$q_l = K_{sat,lat} \cdot \sin(\alpha) \text{ for } \psi > 0 \tag{8}$$

with

q_l = interflow [cm^3 cm^{-3} d^{-1}]

25 $K_{sat,lat}$ = lateral saturated hydraulic water conductivity [cm d^{-1}]

α = slope [–]

EGU

S. Giertz et al.

EGU

5 Data base and model parameterization

As mentioned in the introduction intensive field studies were carried out in the Aguima catchment, therefore a reliable database to parameterize and validate the physically-based model is available. In Fig. 4 the measuring sites relevant for this study are shown.

5.1 Model parameterization

5.1.1 Spatial discretization

To apply SIMULAT-H according to the hillslope concept the catchment is discretized into hillslopes. This was performed with TOPAZ (Topographic Parametrization Tool) (Garbrecht and Martz, 1997), a tool for terrain analysis. The determination of sub-catchments and hillslopes are based on the calculated flow direction which is determined with the D8-Method (Fairchild and Leymarie, 1991). The discretized hillslopes were subdivided in sub-units according to the soil units of the soil investigations (Giertz, 2004; Junge, 2004). Figure 5 shows the discretization of the sub-catchment Upper Aguima into slopes and the subdivision into homogeneous soil units.

For the Upper Aguima and the Upper Niaou catchment all determined hillslopes were parameterized, while for the 16 km^2 sized Lower Aguima catchment ten representative hillslopes were chosen from the total of 68 hillslopes.

Field observations revealed that during extreme precipitation events a high quantity of surface runoff concentrates on small tracks and flows rapidly into the river. To simulate this process, the percentage of tracks in the catchment, which was mapped using a GPS, was considered as separate subunit with a low permeability. The surface runoff occurring on this subunit is added directly to the river discharge during the simulation process.

5.1.2 Soil parameterization

SIMULAT-H enables a variable horizontal discretization of the soil columns. Therefore, each horizon of the classified soil units were parameterized with physical soil properties (θ_s, θ_r, ψ_b and λ) which were determined with laboratory measurements on undisturbed soil samples.

The saturated conductivities of the soil surface were taken from in-situ measurements, while the permeability of the subsoil was determined in laboratory with soil cores (Giertz, 2004).

5.1.3 Vegetation parameters

For each hillslope-unit several vegetation types can be defined. For each vegetation type interzeption, evapotranspiration and infiltration is calculated separately in the model. The water balance of the whole hillslope-unit is then calculated dependent on the ratio of the vegetation type on the hillslope-unit.

Based on the classification of the Landsat 7 ETM+ image (Judex, 2003) the different vegetation types were allocated to the hillslope-units with GIS.

The vegetation parameters (LAI, vegetation height, root depth etc.) were mainly taken from measurements in the Aguima catchment in the framework of the IMPE-TUS project (Orthmann, 2005; Mulindabigwi, 2005). Missing data were estimated from Cournac et al. (2002), de Wasseige et al. (2003) and Scourlock et al. (2001).

5.1.4 Climatic data

To obtain the required climate data for the model (temperature, relative humidity, wind velocity, global radiation and precipitation) the data of three climatic stations were available in the Aguima catchment (Fig. 4). Additionally data from two rain gauges outside the catchment were obtainable. These data were used to fill up gaps of precipitation data during periods with failure of the climatic stations.

EGU

5.2 Validation data

To validate the model, measurement data of discharge, discharge components and soil moisture were used. As the water level gauges were installed in June 2001 the discharge data were obtainable from 2001 to 2003.

5　　The discharge components for single events were determined by temporally highly resolved measurements of electric conductivity at the river gauging station "Upper Aguima" and "Upper Niaou". The measurements were only performed for the rainy season 2002. Additionally, independent water analysis data of Fass (2004) were used to validate the discharge components. He analysed the hydrochemistry of water sam-

10　ples from different sources (rain water, river water, groundwater, soil water, saprolitic water) to determine the fraction of the different water types on the river discharge. The mixing-ratio of the river water was calculated with PHEREEQC-2 (Parkhurst and Appello, 1999) based on water samples taken during the rainy season of the years 2001 and 2002.

15　　The soil moisture was measured with TDR-probes in four different depths (0–20, 30–50, 80–100, 120–140 cm) with an automatic data logger system in a temporal resolution of 10 min. Due to a failure of the measuring system the soil moisture data are only available for 2001 and 2002.

6　Sensitivity analysis

20　The investigation concerning parameter sensitivity was performed for one representative slope of the Upper Aguima catchment. Mainly soil and vegetation parameters were taken into account.

　　To evaluate the sensitivity the sensitivity index SI_{10} was calculated according to de

EGU

Roo (1993):

$$SI_{10} = \frac{|O_{P10} - O_{M10}|}{O_o} \qquad (9)$$

with

O_{P10} = model output with a 10% increase of the parameter value

5 O_{M10} = model output with a 10% reduction of the parameter value

O_o = model output with base simulation

Table 4 shows the sensitivities for the chosen soil, vegetation and groundwater parameters with regard to discharge, discharge components and evapotranspiration.

10 The sensitivity analysis reveals that among the soil parameters the saturated water content is the most sensitive parameter concerning the total discharge and the groundwater flow. Regarding the vegetation parameters the stomata resistance is the most sensitive parameter.

7 Calibration and validation of the model SIMULAT-H

15 7.1 Model performance criteria

To evaluate the model performance for the calibration and the validation the following criteria are taken into account:

1. the coefficient of determination r^2

2. the coefficient of model efficiency (Nash and Sutcliff, 1970)

20 3. the index of agreement (Willmott, 1981)

4. for the discharge validation: the difference between the simulated and measured annual discharge amount

The model efficiency according to Nash and Sutcliff (1970) is defined as:

$$ME = \frac{\sum\limits_{i=1}^{n} (x_i - \bar{x})^2 - \sum\limits_{i=1}^{n} (x'_1 - x_i)^2}{\sum\limits_{i=1}^{n} (x_1 - \bar{x})^2} \tag{10}$$

with

x_i = measured variable

$\bar{x}$ = arithmetic mean of x_i for all events, i=1 to n

x'_i = simulated variable

The model efficiency can attain values from $-\infty$ to 1. The value of 1 indicates the total agreement of measured and simulated values.

In addition to r^2 and the model efficiency, which are usually used as objective functions for model validation, the index of agreement according to Willmott (1981) is applied. This index is a good indicator to evaluate the temporal representation of the discharge by the model. It is calculated with the following equation:

$$IA = 1 - \frac{\sum\limits_{i-1}^{n} (x_i - x'_i)^2}{\sum\limits_{i=1}^{n} (|x_i - \bar{x}'| + |x'_i - \bar{x}'|)^2} \tag{11}$$

The range of values of the index of agreement is between 0 and 1, while 1 represents the total agreement of measured and simulated values.

7.2 Calibration of the model

The model was manually calibrated for the year 2002 for the Upper Aguima catchment for the river discharge. As nearly all input parameters were determined by field measurements only the parameters of the conceptual groundwater model and the lateral K_{sat}-value were calibrated.

Figure 6 shows the result of the simulated hydrograph compared with the measured discharge. Only in the beginning of the discharge period major differences between measured and simulated discharge are observable. This is due to the fact that the runoff at the beginning of the rainy season infiltrates in the river bed and fills up the groundwater storage. Because the conceptual groundwater model is not spatially distributed, the infiltration of river discharge into groundwater can not be computed correctly. In the remaining period the agreement of the hydrographs is good. The discharge peaks as well as the recession period fit to the measured values. The model efficiency and the r^2 attain 0.82, while the index of agreement has a value of 0.95. The total discharge is slightly overestimated by the model (109 mm measured, 117 mm simulated).

7.3   Model validation

Due to a good database a multicriteria validation of the model was feasible. In addition to discharge data, discharge components and soil moisture data which were not used for calibration were available to validate the model results.

7.3.1   Validation of discharge

The validation of the model was performed with the split sample and the proxy basin test according to Refsgaard and Storm (1996).

For the proxy basin test the model was applied in the 16 km^2 sized Lower Aguima catchment without further adjusting of parameters for 2002. For the split sample test the simulation was applied for the years 2001 and 2003 in the Upper and Lower Aguima and the Upper Niaou catchments.

Proxy basin test

The scatter plot in Fig. 7 shows the comparison of measured and simulated dis-

EGU

charge on daily basis for the years 2001, 2002 and 2003. The criteria for the model performance of the simulated years are shown in Table 5. For the year 2002 the correspondence of the simulated and measured discharge is given in Fig. 8. There is a slight underestimation of the discharge amount for the whole year but the model efficiency and the r^2 are even higher than for the calibration period (Table 5). Comparable to the calibration period the major differences between the measured and modelled hydrograph can be observed in the beginning of the discharge period where the baseflow is underestimated, while discharge peaks are often overestimated. In the middle of the rainy season the peaks as well as the baseflow are modelled well and also the recession of the discharge is simulated accurately.

Split sample test

The model was applied with the same parameter set for the years 2001 and 2003 to perform the split sample test for all considered catchments.

The diagram of the model validation in the Lower Aguima catchment for the year 2001 in Fig. 9 shows that the agreement of simulated and measured discharge is good. The discharge peak at the end of September and also the baseflow is simulated well in 2001. Due to the reason explained before, in the beginning of the rainy season small discharge peaks are simulated, although no discharge was measured at all. The model efficiency and the r^2 are 0.82, while an index of agreement of 0.95 is achieved. The measured discharge amount is slightly underestimated by the model (2 mm).

For 2003 (Fig. 10) the model performance is less good than for 2001 and 2002. The comparison of simulated and measured discharge reveals that there is a strong overestimation of discharge events in June. Also the events of the 31 August 2003 and 2 October 2003 are overestimated by the model.

Due to a failure of the measuring system the precipitation data for the climatic station within the Aguima catchment were partly not available for the year 2003. Therefore measurements from the pluviometers outside the catchment were used as input-

data. The high spatial variability of rainfall events causes the poor simulation of certain events. This is documented by the rainfall event of the 15 August 2003, where the highest discharge peak of the year was measured while nearly no precipitation was recorded by the pluviometers. Consequently the model underestimates the discharge for this event. Concerning the representation of the baseflow the simulation shows good results. The model efficiency (0.64) and the r^2 (0.67) are lower than for the years 2001 and 2002.

Further validation of discharge was performed for the Upper Aguima catchment (2001 and 2003) and for the Upper Niaou catchment (2001–2003). The results are summarized in Table 6. Comparable to the validation in the Lower Aguima catchment best results were obtained for the year 2002. Due to the uncertainties of the precipitation data the model performance is lower in 2003.

7.3.2 Validation of discharge components

As explained in Sect. 5.2 the water analysis data of Fass (2004) were used to validate the discharge components.

The following mixing-ratio was determined by Fass (2004):

- 73% surface water and soil water

- 25% groundwater of the saprolitic zone

- 2% deep groundwater

This ratio is a mean value for all rivers of the catchment. Due to the low sampling number a determination of the ratio for each river was not feasible.

The simulated discharge components of SIMULAT-H for the different river gauges are shown in Table 7 for the years 2001 and 2002. The simulated groundwater ratio for all considered gauges of 31% is very close the ratio determined by the hydrochemical measurements (27%). Consequently the correspondence of the modelled and measured surface and soil water fraction is also good.

EGU

Additionally a validation of the discharge components was performed for single events based on continuous measurements of electric conductivity of the river water during the rainy season 2002. The separation of surface runoff from the baseflow was calculated with the following equation:

$$qr = (cd - cb) \cdot \frac{qd}{(cp - cb)} \qquad (12)$$

with

qr = surface runoff [l/s]
qd = river discharge [l/s]
cd = electric conductivity of the river discharge [μs/cm]
cb = electric conductivity of the baseflow [μs/cm]
cp = electric conductivity of the precipitation [μs/cm]

The calculation of the surface runoff amount based on the electric conductivity is not always precise because not only the conductivity of the surface runoff but also the conductivity of the quick subsurface flow is lower than the conductivity of the baseflow.

Figure 11 shows the scatterplot of simulated and "measured" (=calculated with Eq. 12) surface runoff for recorded discharge peaks during the rainy season 2002. Considering all above mentioned uncertainties the correspondence between the simulated and "measured" surface runoff is relatively good for the Upper Aguima catchment. Only for one event the surface runoff is strongly overestimated. For the other events under- and overestimation is observable. As shown in Table 8 no dependency of the over-/underestimation on discharge amount is observable.

Due to a failure of the conductivity probes only measurements of a few peaks are available for the surface runoff validation in the Upper Niaou catchment. For the discharge events in the beginning and the middle of September the agreement is good, but for the events of the 24 August and the 21 September no surface runoff was simulated by the model, while the measurements determined surface runoff. The poor

Physically-based hydrological modelling in Benin

S. Giertz et al.

Title Page

Abstract	Introduction
Conclusions	References
Tables	Figures

◄	►
◄	►
Back	Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion

EGU

model performance for the event of the 24 August could be explained with high amount of runoff on the pathways. Although the pathways were taken into account in the simulation, the process of surface runoff flowing from fields to pathways is not considered in the model. Consequently the direct runoff from pathways to the river is underestimated. In general the model performance for the discharge is relatively poor in August (see Figs. 6 and 8).

The lack of simulated runoff on the 21 September 2002 could be explained by a failure in the precipitation input data for the simulation. For this day no rain was recorded on the rain gauge in the Upper Niaou catchment.

7.3.3   Validation of soil moisture

The validation of the soil moisture was carried out for the Upper Aguima catchment by comparing the simulated soil moisture of different depth with the soil moisture measurements with TDR-probes of the same depth. The validation was performed for a Lixisol with woodland vegetation for the years 2001 and 2002 as nearly no measurement values were available for 2003 due to a failure of the measuring system.

The soil hydrological parameters K_{sat}, θs, θr and Brooks and Corey parameters used for the simulation were taken from measurements without additional calibration. Because the soil moisture data were not used for the calibration of the model also the data from 2002 can be used for validation. The comparison of measured and simulated soil moisture is shown in Figs. 12 and 13.

In both years the agreement between simulated and measured soil water dynamic in the depth of 0–30 cm is good. The peaks as well as the drying of the soil at the end of the rainy season are simulated well. For both years the r^2 and the index of agreement are over 0.94 (Table 9), while a model efficiency of 0.86 for the year 2001 and of 0.72 for the year 2002 was achieved. For the layer 30–50 cm the model performance is lower. While the dynamic of the soil moisture is well reproduced by the model, the agreement of the simulated and measured soil moisture peaks are poorer than in the first layer. Overall the results are reasonable for this layer. As shown in Figs. 12 and 13

Title Page

Abstract | Introduction

Conclusions | References

Tables | Figures

◄ | ►

◄ | ►

Back | Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion

EGU

and in Table 9 the simulation result of the Btc-horizon (80–100 cm) is poor. This could be explained by the high gravel content of this layer, which causes inaccuracies in the TDR-measurements and for the determination of the soil-water-retention curve.

In the saprolitic layer (120–140 cm) the constant soil water content of 10% in the beginning of the rainy season is well simulated in 2002. In 2001 the saturation of the sub-soil is a very rapid process, which is not simulated accurately by the model. According to the measurements the soil moisture increases from 10 to 35% during one day in 2001, which is caused by preferential flow in continuous macropores. Calculating the amount of water required for saturating the soil in this depth it became clear that this is a local scale phenomenon. As there is no macropore-model available in SIMULAT-H the model is not able to simulate this process.

8 Representation of the runoff generation processes

The characterization of the major soil types with regard to the runoff generation processes in Sect. 3 has shown that the soil physical properties differs strongly for the subsoil of the dominant soil types (Plinthosol, Lixisol/Acrisol, Gleysol). The runoff generation processes based on the soil investigations and field observations are explained in Sect. 3. The model concept of SIMULAT-H allows quantifying the runoff generation processes for each soil unit of the hillslope. Figure 14 shows the runoff generation for 2002 for one representative slope of the Upper Aguima and Fig. 15 for the Upper Niaou catchment.

In the Upper Aguima catchment interflow is the predominant runoff generation process in the major soil types of the upper and middle hillslope (Plinthosol, Lixisol/Acrisol). While for the Plinthosol no groundwater recharge was determined, about 25% groundwater recharge were calculated by the model for the soil unit Lixisol/Acrisol. For the Gleysols groundwater recharge is the major runoff generation process.

Due to the lower infiltration rates on fields (compare Giertz, 2004, and Giertz et al., 2005) the proportion of surface runoff is higher in the Upper Niaou catchment. In par-

ticular on the middle slope on Plinthosols the ratio of surface runoff of all runoff generation processes is very high. On Lixisols/Acrisols the interflow is predominant. Here the overland flow is even lower than in the Upper Aguima catchment. This is caused by the extremely high saturated conductivity which was determined for a cashew plantation in the Upper Niaou on this soil type (Giertz and Diekkrüger, 2003).

⁵

The simulation results of the runoff generation processes confirm the perceptual model based on the field investigations, which was presented in Sect. 3. As major runoff generation process on the upper and middle hillslope of the Upper Aguima catchment interflow was determined by the simulation and the perceptual model. Dependent on the land cover surface runoff or interflow are predominant for Plinthosols and Lixisols/Acrisols for the same slope section. At the bottom of the slope groundwater recharge is an important process, due to high permeability of the Gleysols. In the Upper Niaou also surface runoff occurs due to a high amount of surface runoff from the upper slope soil units.

9 Discussion of uncertainties

Generally three sources of uncertainties in the modelling process could be distinguished:

1. Input parameter

2. Model assumptions and algorithms for process description

3. Measuring data for model validation

9.1 Input parameter

Due to the interdisciplinary research in the Aguima catchment the database to parameterize the model was – for West African conditions – very good. Consequently the uncertainties related to the input parameters are relatively low.

Concerning vegetation parameters measurement data of LAI and vegetation height were available from studies of Orthmann (2005) and Mulindabigwi (2005). Solely the stomata resistance had been taken from literature data. As the sensitivity for this parameter is relatively high, the uncertainty caused by these parameters is relatively high
5　compared to the other parameters.

The spatial distribution of the land cover types was taken from the land cover classification of Landsat ETM scenes by Judex (2003). Due to detailed ground-truth the quality of the classification is very good.

Soil physical parameters were available from in-situ and laboratory measurements
10　(Giertz, 2004; Junge 2004; Giertz et al., 2005). As no data for the lateral K_{sat}-values were available this parameter was calibrated. The sensitivity analysis revealed that the influence of this parameter on the discharge amount is relatively low. The highest sensitivity index was determined for the saturated water content. But as this parameter was measured on soil cores the uncertainty related with this parameter is relatively low.
15　As climate data were available from own measurements in the catchment the uncertainties related to this data are low. For West African conditions the existence of 3 climatic stations in a small basin of 30 km^2 is exceptional. Only six climatic stations of the national meteorological service exist for whole Benin.

Due to a failure of the measuring system more uncertainties are related to the pre-
20　cipitation data for 2003, because data from rain gauges outside the catchment had been used as model input.

For the groundwater parameters no measurement data were available, hence these parameters were calibrated for the catchment. The sensitivity analysis pointed out that the influence of these parameters on the model result is low.

25　9.2　Model assumptions and algorithms for process description

In general the model related uncertainties are lower for physically-based models as for conceptual or empirical models. As pointed out in Sect. 8 SIMULAT-H is able to simulate the runoff generation processes in the catchment correctly. Therefore it can

Physically-based hydrological modelling in Benin

S. Giertz et al.

EGU

be assumed that the uncertainties related to the process description in general are low. But the validation of the soil moisture revealed that some details as the saturation of the sub-soil are not correctly simulated by the model. This is caused by the lack of a macropore model in SIMULAT-H. As macropores play an important role for soil water fluxes in the catchment (Giertz, 2004; Giertz et al., 2005), neglecting the macropores can cause a poorer representation of the processes. An integration of this could ameliorate the model performance.

Another model related uncertainty is the lack of a routing-routine in SIMULAT-H. As the results are validated on a daily time step and the regarded catchments are small, the inaccuracy caused by this is relatively small. For the validation of single events as performed in Vertessy and Elsenbeer (1999) the lack of a routing-routine would have a stronger influence on the model result.

As already mentioned in Sect. 7 the poor representation of surface runoff generation on pathways is one model related uncertainty. Most of all the process of surface runoff running from fields on the pathways is poorly represented in the model. But it has to be noticed that a parameterization is difficult to perform because these pathways are spontaneous build by the local farmers.

Although the model SIMULAT-H implies some simplifications in the process description the process representation is quite good, as shown in the validation section.

9.3 Measuring data for model validation

Compared to other studies the database for model validation is good, as in addition to discharge also discharge components and soil moisture data were available for model validation.

In general all measurements contain measurement errors, which have to be taken into account while using this data for validation.

9.3.1 Discharge data

The discharge was calculated based on continuous water level measurements and a stage-discharge relationship for each gauge. The latter was obtained by numerous discharge measurements in 2001 and 2002 with the cross section method (Davie, 2003) at different water levels. Although this method is related with uncertainties, it is the standard-method for discharge measurements, because other methods for continuous discharge measurements are not available.

One uncertainty of this method is the possible change in the morphology of the riverbed caused by erosion and sedimentation processes, which can influence the stage-discharge relationship.

Another problem is that often during the peak discharge no discharge measurements were carried out or the measurements were difficult to perform (e.g. because of inundation of the river bank). To calculate the peak-discharge based on the stage-discharge relationship an extrapolation is performed. Consequently the calculated peak discharge is very uncertain.

As shown in Sect. 8 the representation of the peak discharge is very good for the year 2002. In 2003, no additional discharge measurements were carried out to complete the stage-discharge relationship. Consequently for this year higher uncertainties concerning the discharge data are expectable.

The validation of simulated surface runoff of single peaks was performed using measurement data of electric conductivity. The calculation of the surface runoff from the conductivity data is based on Eq. (12). The assumption is that the conductivity of the discharge is a mixture of baseflow and surface runoff, which has a lower conductivity as the baseflow. The uncertainty in this assumption is that in addition to the surface runoff also the quick interflow can reduce the electric conductivity of the discharge. But if the residence time of the water in the soil is low or if the water runs in macropores to the river the electric conductivity is comparable with the surface runoff.

EGU

9.3.2 Soil moisture

TDR-probes are a standard measuring instrument for the determination of soil mois-
ture. The accuracy of the soil moisture measurements is very high, in exception of
soils with a very high humus content, salinity or density. Measurement errors also oc-
cur when the contact between the soil matrix and the probe is poor. This is often the
case in soils with high gravel content. As the sub-soil of the Lixisol, where the mea-
surement of soil moisture were carried out in the Aguima catchment, is characterized
by a high gravel content, the possible measurement error has to be taken into account
when using this data for model validation. The comparison of simulated and measured
soil moisture in this layer has shown a poor agreement. One reason for this could be
possible errors in the measurement data as explained before.

The discussion of the uncertainties pointed out that at all levels (input data, model
assumptions and validation data) uncertainties exist. Often it is not possible to deter-
mine which uncertainties cause the deviation between modelled and measured state
variables. By calibration often uncertainties are reduced due to the wrong reason. Be-
cause in this study only two parameters have been calibrated, the uncertainties were
better identifiable.

10 Conclusion

The validation of the physically-based model SIMULAT-H has shown that the model
concept is suitable to simulate the hydrological processes in a tropical environment.
For the discharge validation good results were achieved for dry and wet years. Main dif-
ferences were observable in the beginning of the rainy season. This was also observed
for application of other hydrological models in similar climate conditions (Campling et
al., 2002; Varado, 2004).

The comparison of the discharge components determined by hydrochemical mea-
surements with the simulation revealed that the model simulated the ratio of ground-

EGU

water and surface water correctly. For the validation of the discharge components of single events larger differences were observable, which was partly caused by uncertainties in the precipitation data. For one event the reason for the lack of surface runoff was rather the insufficient representation of the runoff generation processes on pathways. First modifications of the modelling process have shown that the assumption that a higher proportion of surface runoff flows directly into the river instead of running on the next soil unit ameliorates the simulation results.

Concerning soil water dynamics the model performance was good for the topsoil. Major problems occurred in the gravel-enriched Btc-horizon. Due to the high gravel content the uncertainties in the measurements of the soil physical parameters are high (e.g. K_{sat} measurements, determination of soil water retention curve) and also the installation of TDR-probes in the soil is difficult. Both could be a reason for the big differences between the measured and simulated soil moisture. In the saprolitic horizon the model was not able to reproduce the quick saturation of this layer, because no macropore model is available in SIMULAT-H. An integration of macropores in the modelling system could ameliorate the model performance concerning the soil water dynamics. But in general the parameterization of a macropore-system is very difficult, because often no information about the size, the amount and the continuity of macropores is available. Another problem is that the measured K_{sat}-values include marcropore-flow, so that they are not usable to parameterize a model with an additional macropore system without further assumptions.

Although the model SIMULAT-H implies some simplifications in the process description the model is able to simulate the processes correctly, which was revealed by a comparison with the field observations.

With the application of a physically-based model in Benin this study is a relevant contribution to the research domain of hydrological modelling in tropical regions, especially West Africa. Due to the limited data availability the experience with physically-based models in this region is low therefore often only conceptual models are applied.

The multi-criteria validation for catchments with different land use and for dry and wet

HESSD

3, 595–651, 2006

**Physically-based
hydrological
modelling in Benin**

S. Giertz et al.

years has shown that the presented model is applicable to calculate future scenarios of land use and climate change in tropical regions in order to predict the impact of these changes on the hydrological processes and the water availability on the local scale. Furthermore the model can be used for a model-model comparison in Global Change studies to evaluate the scenario simulation results of conceptual models for larger scales.

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Title Page

Abstract | Introduction

Conclusions | References

Tables | Figures

◄ | ►

◄ | ►

Back | Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion

EGU

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Physically-based hydrological modelling in Benin

S. Giertz et al.

EGU

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Physically-based hydrological modelling in Benin

S. Giertz et al.

EGU

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Physically-based hydrological modelling in Benin

S. Giertz et al.

EGU

Table 1. Size and vegetation of the investigated sub-catchments.

Name of the sub-catchment	Upper Aguima	Lower Aguima	Upper Niaou
Size of the sub-catchment [km^2]	3.2	16.5	3.1
Land cover of the catchments [%]			
Woodland	64.7	61.1	31.2
Savannah	29.7	31.2	32.1
Fallow/cashew or teak plantation	0.4	1.6	13.5
Field	3.1	5.6	23.2
Inselberg	2.1	0.5	0.0

Physically-based hydrological modelling in Benin

S. Giertz et al.

Table 2. Runoff generation processes in the Upper Aguima and Upper Niaou catchments.

Hillslope, soil type	Prevailing runoff generation processes Upper Aguima, natural vegetation	Prevailing runoff generation processes Upper Niaou, agricultural land use
Upper hillslope, Plinthosol	Interflow	–
Upper/middle hillslope, Lixisol	Groundwater flow (saprolite), interflow	Surface runoff (dependent on land use), groundwater flow (saprolite), interflow
Lower hillslope, Plinthosol	Interflow	Surface runoff, interflow
Inland valley fringe, sandy Gleysol	Groundwater flow	Infiltration of surface runoff from hillslope causes high groundwater recharge (saprolite)
Inland valley center, clayey Gleysol	Saturated surface runoff, groundwater flow	Saturated surface runoff, groundwater flow
Pathways	Surface runoff	Surface runoff

EGU

Table 3. Water balance of the investigated catchments of the years 2000 to 2003.

	Upper Aguima	Lower Aguima	Upper Niaou
2001 (18 June 2001–31 December 2001)			
Precipitation [mm]	609	609	609
Discharge volume [m^3]	74 145	752 415	483 054
Discharge height [mm]	23.0	45.5	155.8
Discharge coefficient [%]	3.8	7.5	25.6
2002			
Precipitation [mm]	1145	1145	1157
Discharge volume [m^3]	351 633	2 323 637	568 804
Discharge height [mm]	109.2	139.6	183.5
Discharge coefficient [%]	9.5	12.2	15.8
2003			
Precipitation [mm]	1216	1216	1230
Discharge volume [m^3]	631 473	3 033 868	714 710
Discharge height [mm]	196.1	183.3	230.6
Discharge coefficient [%]	16.1	15.2	18.7

Table 4. Sensitivity indices SI_{10} for different model parameters calculated for a representative hillslope (in bold the most sensitive parameters).

	SI_{10} Total discharge	SI_{10} Surface runoff	SI_{10} Interflow	SI_{10} Ground-waterflow	SI_{10} Evapotrans-piration
Soil parameter					
θ_s	**0.9167**	0.2468	0.7876	**1.2858**	0.0084
θ_r	0.0479	0.0150	0.0339	0.0832	0.0158
K_{sat}	0.0420	1.0563	0.0424	0.0834	0.0050
$K_{sat-lat}$	0.0033	0.0000	0.0367	0.0704	0.0002
$K_{sat-sigma*}$	0.0194	0.4868	0.0190	0.0372	0.0000
Vegetation parameter					
LAI	0.0826	0.0185	0.0889	0.0766	0.0042
Stomata resistance	0.2833	0.0551	0.2321	0.4249	0.0228
Vegetation height	0.0844	0.0169	0.0326	0.3566	0.0044
Root depth	−0.0250	0.0425	0.0233	0.0370	0.0110
Groundwater parameter					
Gw-constant	0.0030	0.0000	0.0099	0.0320	0.0000
Initial Gw-storage	0.0001	0.0000	0.0000	0.0003	0.0000

* $K_{sat-sigma}$: standard deviation of log-normal distribution of K_{sat}-values

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Table 5. Model validation Lower Aguima catchment.

	Q measured [mm]	Q simulated [mm]	ME	r^2	IA
2001*	45.5	47.4	0.82	0.82	0.95
2002	139.6	132.5	0.86	0.87	0.96
2003	183.3	254.7	0.64	0.67	0.87

* simulated period: 20 June 2001–31 December 2001

Table 6. Model validation for the Upper Aguima and Upper Niaou catchments.

Upper Aguima					
	Q measured [mm]	Q simulated [mm]	ME	r^2	IA
2001*	23.0	40.2	0.67	0.78	0.87
2002 C	109.2	117.2	0.82	0.82	0.95
2003	196.1	225.1	0.42	0.53	0.84
Upper Niaou					
	Q measured [mm]	Q simulated [mm]	ME	r^2	IA
2001*	155.8	187.5	0.42	0.49	0.84
2002	183.5	202.1	0.67	0.71	0.91
2003	230.6	265	0.58	0.66	0.89

* simulated period: 20 June 2001–31 December 2001
C= Calibration period

Table 7. Simulated discharge components [%].

	Upper Aguima		Lower Aguima		Upper Niaou		Mean
	2001	2002	2001	2002	2001	2002	2001+2002
Surface runoff	14	15	8	10	24	13	14
Interflow	64	59	43	39	58	67	55
Groundwater	22	26	48	51	18	20	31

Table 8. Measured (= determined with Eq. 12) and simulated surface runoff for the Upper Aguima and the Upper Niaou catchments for runoff events in the rainy season 2002.

	Upper Aguima Discharge [mm]	Surface runoff measured [%]	Surface runoff simulated [%]	Upper Niaou Discharge [mm]	Surface runoff measured [%]	Surface runoff simulated [%]
24 Aug 2002	1.18	26.1	38.4	6.85	22.0	0
29 Aug 2002	0.71	16.8	80.6	n.a.	n.a.	n.a.
3 Sep 2002	2.19	30.4	51.6	n.a.	n.a.	n.a.
5 Sep 2002	12.02	40.8	52.6	14.01	34.8	31.2
15 Sep 2002	8.37	32.5	9.2	10.11	31.9	36.5
19 Sep 2002	n.a.	n.a.	n.a.	5.05	11.8	42.49
21 Sep 2002	n.a.	n.a.	n.a.	1.48	7.7	0
27 Sep 2002	2.65	30.5	30.8	n.a.	n.a.	n.a.
5 Oct 2002	1.30	18.7	11.7	n.a.	n.a.	n.a.
9 Oct 2002	2.99	21.1	8.7	n.a.	n.a.	n.a.
11 Oct 2002	1.65	17.2	5.4	n.a.	n.a.	n.a.
19 Oct 2002	2.75	31.8	26.6	n.a.	n.a.	n.a.
25 Oct 2002	0.56	18.7	30.4	n.a.	n.a.	n.a.

n.a.: no data available

Table 9. Validation of soil moisture at different depths for a Lixisol with woodland vegetation in the Upper Aguima catchment.

	ME	r^2	IA
2001			
0–20 cm	0.86	0.95	0.97
30–50 cm	0.55	0.86	0.91
80–100 cm	−0.25	0.57	0.45
120–140 cm	0.51	0.79	0.88
2002			
0–20 cm	0.72	0.94	0.95
30–50 cm	0.71	0.94	0.94
80–100 cm	0.57	0.81	0.85
120–140 cm	0.19	0.54	0.76

Title Page

Abstract | Introduction

Conclusions | References

Tables | Figures

|◄ | ►|

◄ | ►

Back | Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion

EGU
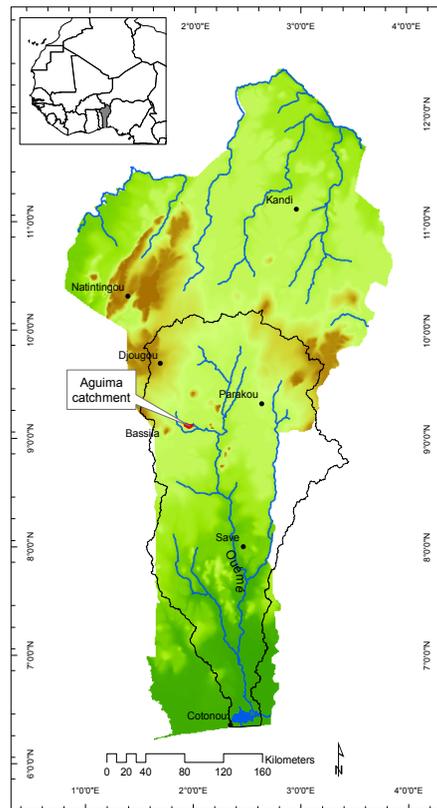
Fig. 1. Location of the Aguima catchment, a sub-catchment of the Ouémé river in Benin, West Africa.

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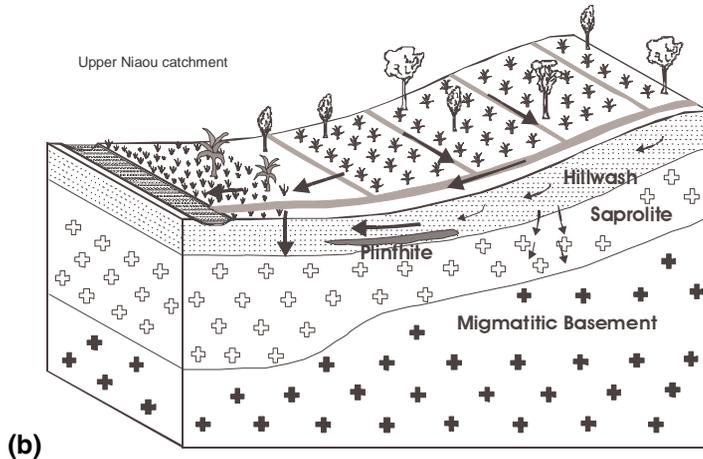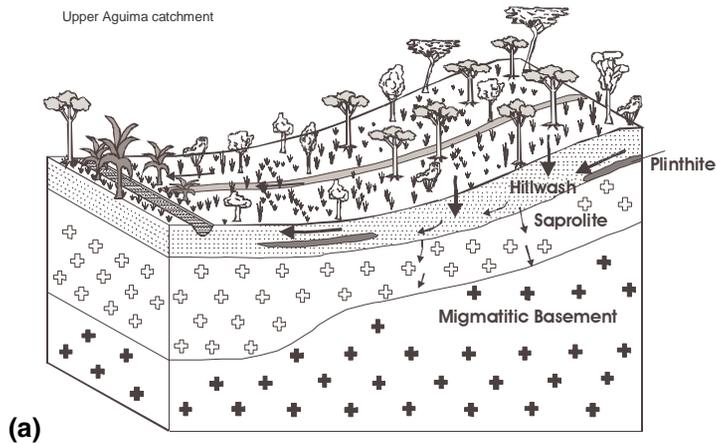
Fig. 2. (a) Flow paths in the Upper Aguima (natural vegetation) and **(b)** flow paths in the the Upper Niaou (agriculture) catchment. The size of the arrows determines the importance of the flow paths.
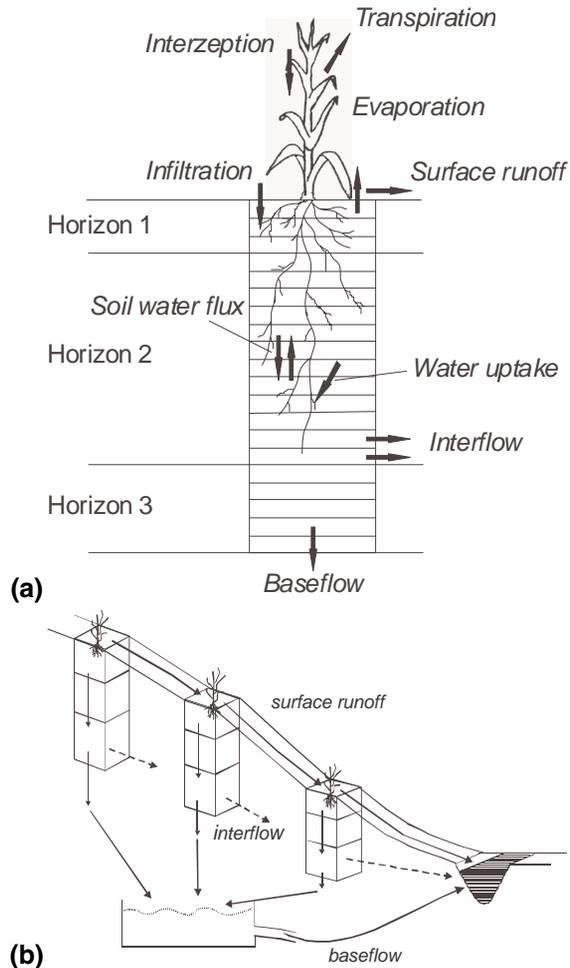
Fig. 3. (a) Model concept of SIMULAT. **(b)** Modification of SIMULAT to the hillslope version SIMULAT-H.
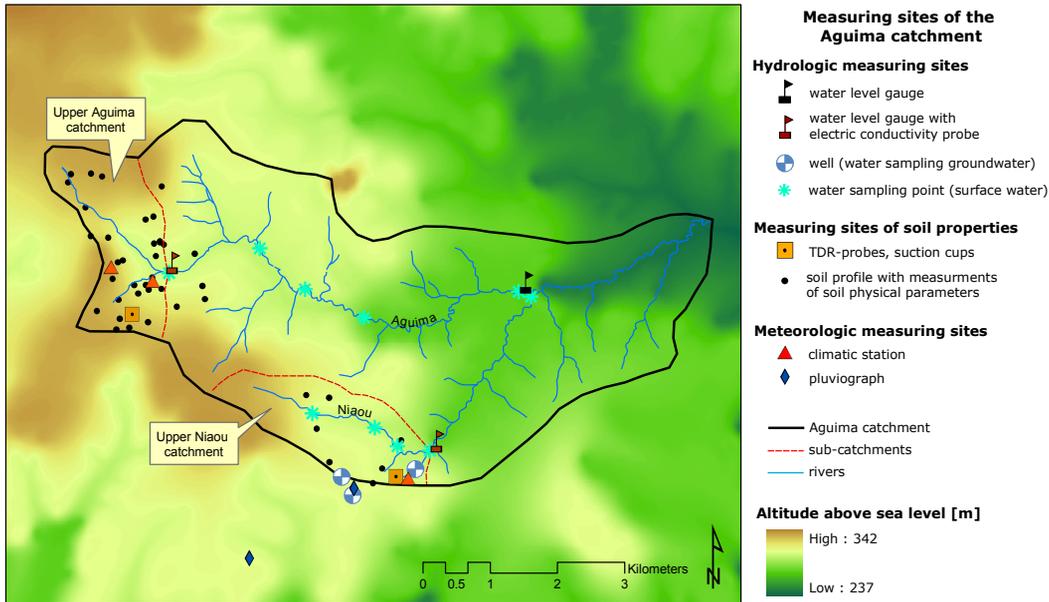
Fig. 4. Instrumentation of the Aguima catchment.

Measuring sites of the Aguima catchment

Hydrologic measuring sites
- water level gauge
- water level gauge with electric conductivity probe
- well (water sampling groundwater)
- water sampling point (surface water)

Measuring sites of soil properties
- TDR-probes, suction cups
- soil profile with measurments of soil physical parameters

Meteorologic measuring sites
- climatic station
- pluviograph

— Aguima catchment
---- sub-catchments
— rivers

Altitude above sea level [m]
High : 342
Low : 237

Upper Aguima catchment

Upper Niaou catchment

Aguima

Niaou

Kilometers
0 0.5 1 2 3

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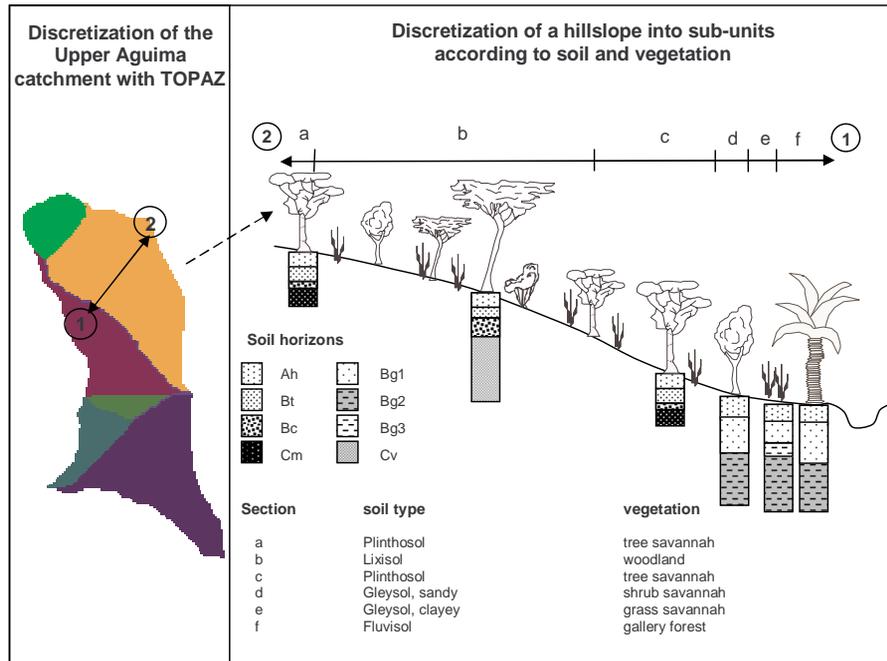
Fig. 5. Discretization of a representative hillslope of the Upper Aguima catchment.

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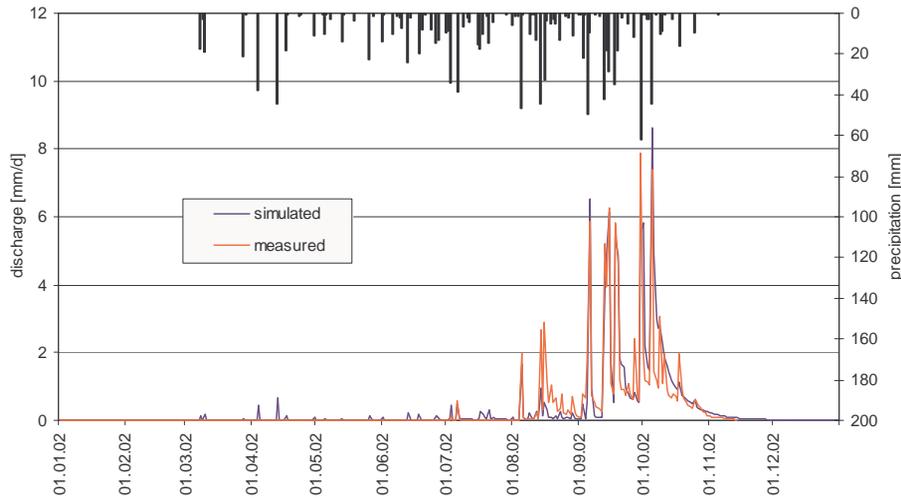
Fig. 6. Comparison of the simulated and measured hydrograph of the Upper Aguima catchment, year 2002 (3.2 km^2, calibration result).

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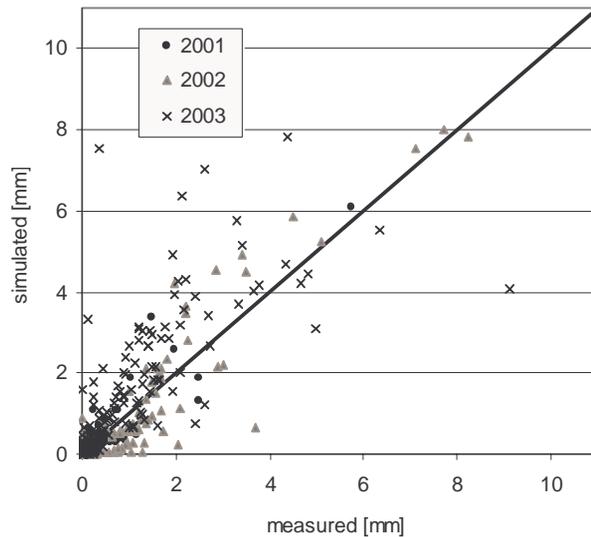
Fig. 7. Scatter plot of simulated and measured discharge for the Lower Aguima catchment (16.5 km^2, validation results).

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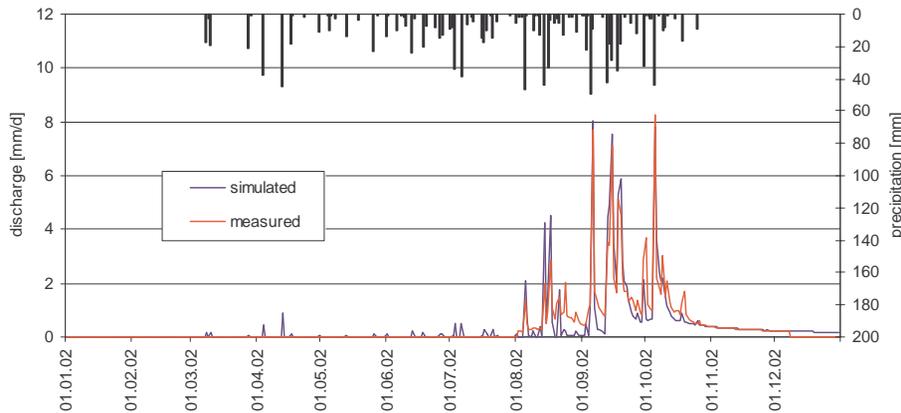
Fig. 8. Comparison of the simulated and measured hydrograph of the Lower Aguima catchment, year 2002 (16.5 km^2, validation result, proxi-basin test).

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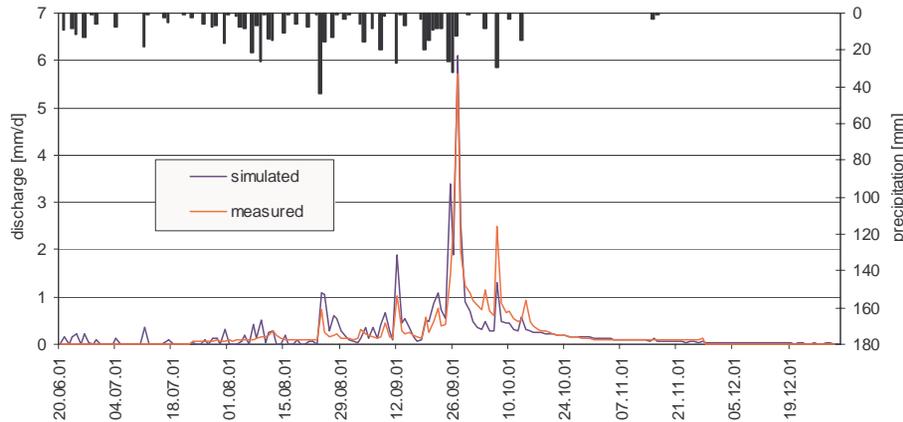
Fig. 9. Comparison of the simulated and measured hydrograph of the Lower Aguima catchment, year 2001 (16.5 km^2, validation result, proxy-basin and split-sample test).
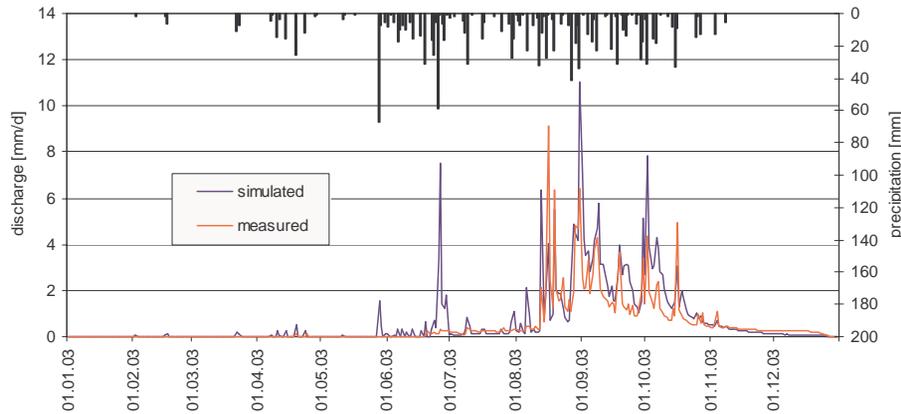
Fig. 10. Comparison of the simulated and measured hydrograph of the Lower Aguima catchment, year 2003 (16.5 km^2, validation result, proxi-basin and split-sample test).

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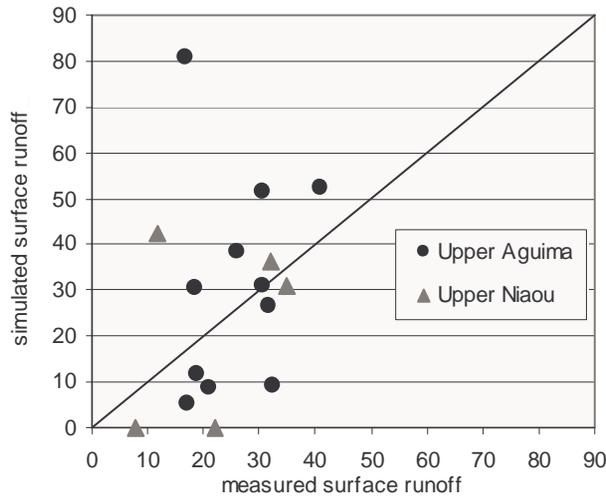
Fig. 11. Scatter plot of simulated and measured (= determined with Eq. 12) surface runoff for the Upper Aguima (3.2 km^2) and the Upper Niaou (3.1 km^2) for runoff events in the rainy season 2002 (in % of the total discharge).
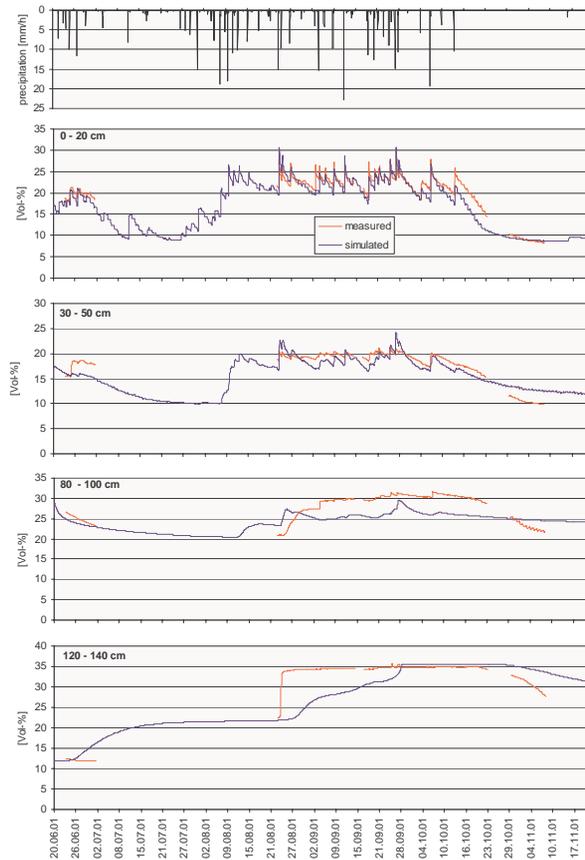
Fig. 12. Comparison of simulated and measured soil moisture at different depths for a Lixisol with woodland vegetation in the Upper Aguima catchment, year 2001 (missing data: failure of measuring system).

Printer-friendly Version

Interactive Discussion

EGU
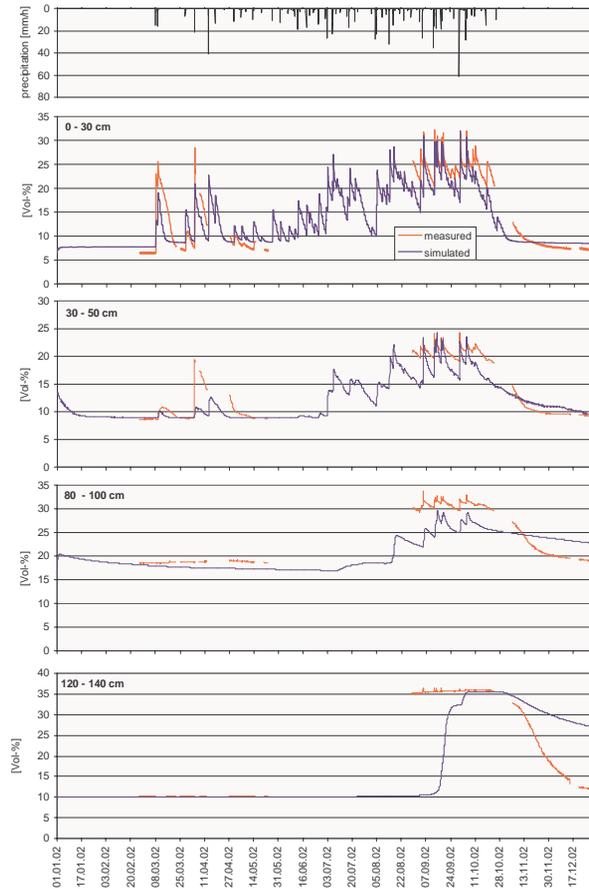
Fig. 13. Comparison of simulated and measured soil moisture at different depths for a Lixisol with woodland vegetation in the Upper Aguima catchment, year 2002 (missing data: failure of measuring system).
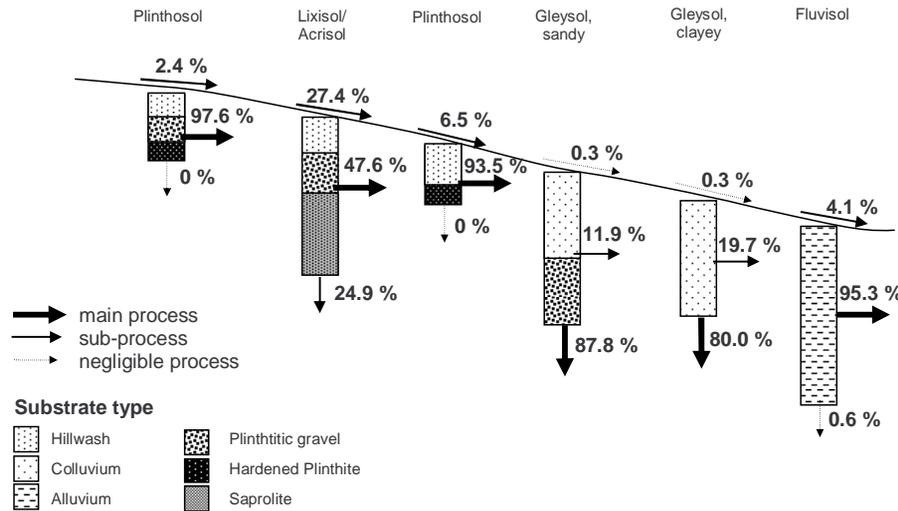
Fig. 14. Simulated runoff generation processes [%] for a representative hillslope of the Upper Aguima catchment (natural vegetation).

Title Page

Abstract   Introduction

Conclusions   References

Tables   Figures

◄◄   ►►

◄   ►

Back   Close

Full Screen / Esc

Printer-friendly Version

Interactive Discussion

EGU
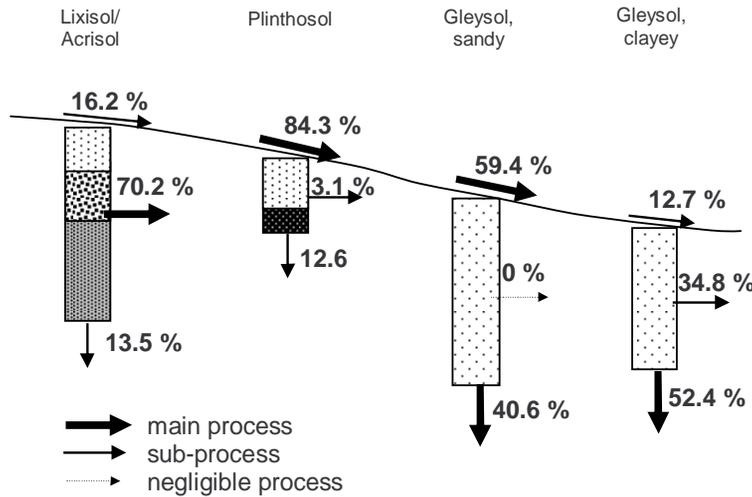
Fig. 15. Simulated runoff generation processes [%] for a representative hillslope of the Upper Niaou catchment (agriculture). Explanation of the substrate types in Fig. 14.