



HAL
open science

New electro-optic sensor architecture for temperature measurements

Rémy Claverie, Jean-Paul Salvestrini, Marc Fontana

► **To cite this version:**

Rémy Claverie, Jean-Paul Salvestrini, Marc Fontana. New electro-optic sensor architecture for temperature measurements. IEEE Instrumentation and Measurement Technology Conference (IMTC2007), 2007, Warsaw, Poland. <10.1109/IMTC.2007.379324>. <hal-00186291>

HAL Id: hal-00186291

<https://hal.science/hal-00186291v1>

Submitted on 2 Dec 2021

HAL is a multi-disciplinary open access archive for the deposit and dissemination of scientific research documents, whether they are published or not. The documents may come from teaching and research institutions in France or abroad, or from public or private research centers.

L'archive ouverte pluridisciplinaire HAL, est destinée au dépôt et à la diffusion de documents scientifiques de niveau recherche, publiés ou non, émanant des établissements d'enseignement et de recherche français ou étrangers, des laboratoires publics ou privés.



Distributed under a Creative Commons CC BY-NC 4.0 - Attribution - Non-commercial use - International License

New electro-optic sensor architecture for temperature measurements

Rémy Claverie,* J.P. Salvestrini, and M.D. Fontana
 LMOPS - UMR 7132 Université Paul Verlaine - Metz - Supélec
 2 Rue Edouard Belin - 57070 METZ

I. INTRODUCTION

We show in this paper, the first results on the feasibility of a new electro-optic sensor architecture used for temperature measurements. This sensor is based on the birefringent variation of an optical material. This phenomena is well-known and often exploited for electric field measurements [1, 2] or temperature measurements [3]. All these sensors use the refractive index variation induced on a crystal placed into a polarimetric setup. Optical intensities variations due to temperature variation enable to determine the value of the temperature. Nevertheless, for most of the authors, the electronic part of these sensors is not the main interest, that why, we describe the optical part and focus on the electronic instrumentation of our sensor. This one is based on an electronic detector which remains its output directly proportionnal to the temperature variation [4]. The temperature value is obtained by a control of the static intensity at a specific operating point of the transmittance. The results show that this architecture offers a high linearity and has a short response time (50ms).

II. SENSOR OPTICAL CONFIGURATION

Even if the sensor is used for temperature measurements, the optical configuration allows others applications such as electric field measurements or strain measurements. These applications depends only on the birefringent material (crystal) used for the probe (KTP for temperature or LiNbO_3 for electric field, for example). The optical part shown on figure 1 is based on the Sénarmont setup into which a electrooptic modulator is inserted between the quarter-wave plate and the optical fiber. The optical transmittance is :

$$T = T_0 \left[1 - \sin(\Gamma + \Gamma') \right] \quad (1)$$

*Electronic address: remy.claverie@univ-metz.fr

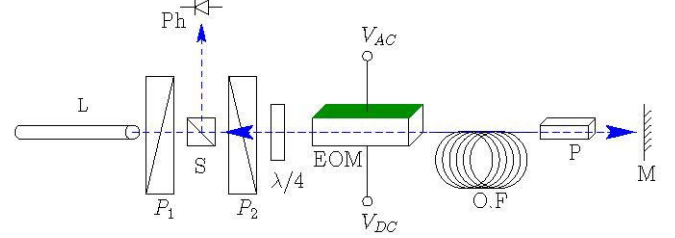


FIG. 1: Sensor optical configuration. L : laser, P_1 : polariser, SC : beam splitter, P_2 : analyser, $\lambda/4$: quarter-wave plate, EOM : electro-optic modulator, O.F : optical fiber, S : probe, M : mirror, Ph : Photodiode + detector

where Γ is the phase retardation of the EOM, related to its bias voltage V_{DC} by $\Gamma = \pi \frac{V_{DC}}{V_\pi}$ and Γ' is the phase retardation due to temperature variation on the probe crystal and related to the birefringence by : $\Gamma' = 2 \cdot \pi \cdot L/\lambda \cdot \delta\Delta n$. Where V_π is the half-wave voltage, λ the wavelength, L the optical path length and $\delta\Delta n$ is the birefringence, linearly linked to the temperature [5].

On the EOM, the V_{DC} voltage sets the operating point on the transmittance and the V_{AC} voltage is used to modulate the intensity. The EOM is a lithium niobate crystal ($L=40\text{mm}$, Section = $3 \times 3\text{mm}^2$).

According to the figure 2, representing the equation 1, when the V_{DC} voltage is chosen to have the operating point is at M'_0 , the V_{AC} voltage create a amplitude modulated signal related to this V_{AC} voltage and with the same ω_0 pulsation than V_{AC} pulsation (ω_0 is the fundamental). On the opposite, at M_0 point, the modulated signal has a double pulsation $2\omega_0$ [6]. Between M_0 and M'_0 (at M''_0 for exemple) the modulated signal is composed by two harmonics at ω_0 and $2\omega_0$ pulsations.

III. FULL SENSOR ARCHITECTURE

When a birefringent variation of the probe crystal occurs, induced by a temperature variation, the phase Γ' is shifted and thus modify the operating point. The return to the initial point can be done by an opposite variation of Γ with the same value. This compensation leads to a linear relationship between the temperature variation

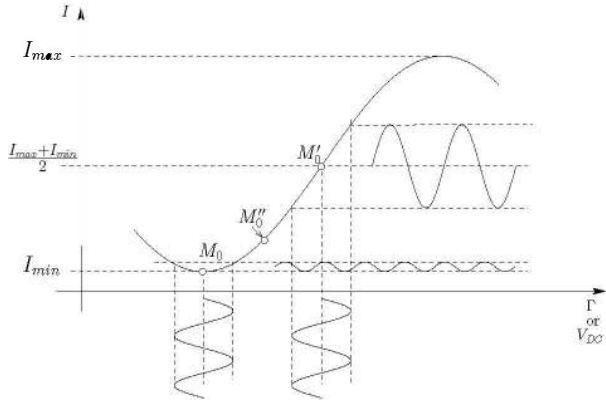


FIG. 2: Transmittance of the setup and associated operating points

and the EOM bias compensation voltage V_{DC} [7] :

$$dT = \alpha dV_{DC} \quad (2)$$

Where α depends on the already defined parameters : λ , $\delta\Delta n$, L and V_{π} . Our goal is to control the system at M_0 point to ensure an unsensitivity to the laser variation. To do that, we have chosen to control the system on the amplitude of ω_0 signal. As shown the figure 3, at M_0 point, ω_0 signal amplitude is zero and intensities variations are linear for small variations of V_{DC} . We can also notice that the sign of this signal depends on relative position of the operating point and thus informs us about the variation sense of the temperature.

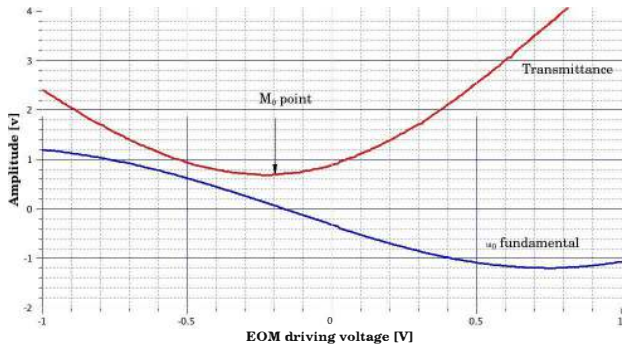


FIG. 3: Voltage amplitude of the fundamental at ω_0 according to V_{DC}

The control is made by a feedback loop and a PID controller (see figure 4).

V_{AC} sinusoidal voltage is the output of a stable low frequency oscillator associated to a transformer (52V - 20.7kHz). The DC voltage is generated by an high voltage PWM oscillator whose mean value ($0 \rightarrow 740V_{PP}$) is proportional to the driving voltage ($-3V \rightarrow +3V$) of

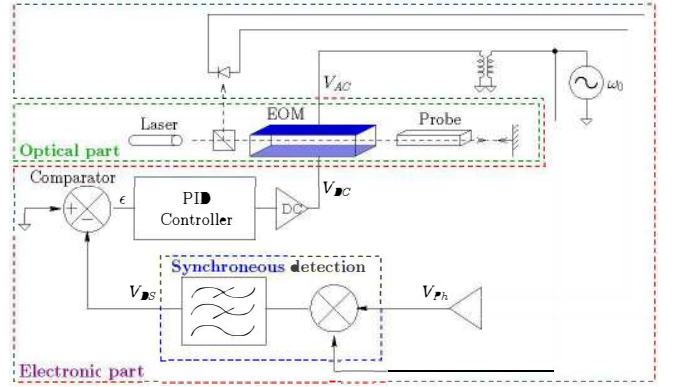


FIG. 4: Sensor with the feedback loop and the PID Controller

the PWM oscillator. The optical signal is converted to a voltage signal by a photodiode and a transconductance amplifier. Detection is made by a multiplier and a low-pass filter.

The input of the comparator is set to zero which is the ω_0 amplitude. This value is adjusted with a spectrum analyser because of the very small amplitude of fundamental ω_0 . The electronic loop controls the system at this value.

IV. RESULTS

The system was studied in open loop in order to calculate controller's parameters according to the Strejc-Naslin method. Furthermore, we have evaluated the dynamical performances in both open-loop and close-loop configurations. Figure 5 shows the response of the system submitted to a disturbance (simulated by a step voltage added after the PID controller). We can deduce from this

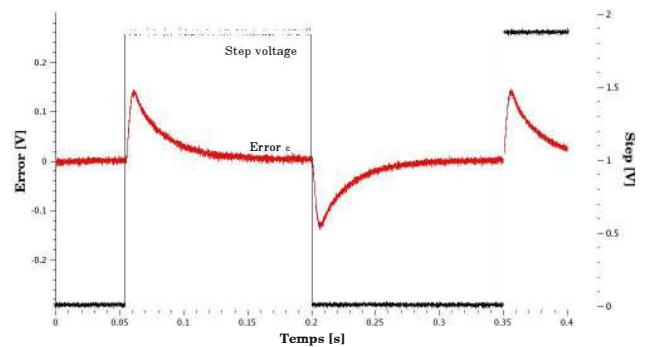


FIG. 5: Error signal when the system is submitted to a disturbance.

figure that the response time is 50ms while it was 100ms in the close-loop configuration. This quite long time is

mainly due to the PWM based amplifier. The error signal shows us that the PID controller fully compensates the disturbance.

As an application, we show on figure 6, the sensitivity of the sensor (output voltage versus temperature). The slope of this curve gives the sensitivity which is $0.91^{\circ}\text{C}/\text{V}$.

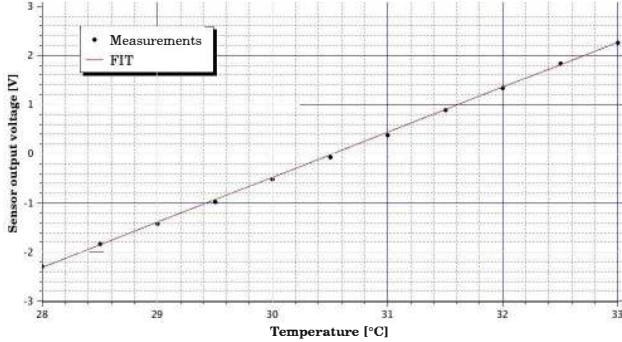


FIG. 6: Sensor sensitivity for temperature measurements

V. CONCLUSION

We introduced an electro-optic sensor with a new architecture, based on Sénarmont setup and controlled in order to hold the same operating point. For temperature measurements, the sensor has a sensitivity of $0.91^{\circ}\text{C}/\text{V}$. The response time is closed to 50ms. This sensor can be easily adapted for others parameters such as electrical field or strain measurements. It's fully insensitive to EMC and to the laser variations.

- [1] W.K. Kuo, W.H. Chen, Y.T. Huang and S.L. Huang, Two dimensional electric-field vector measurement by a LiTaO_3 electro-optic tip, *Appl. Opt.* **39**, 27, 4985-4993 (2000)
- [2] F. Cecelja, M. Bordovsky and W. Balachandran, Electro-optic Sensor for Measurement of DC Fields in the Presence of Space Charge, *IEEE Trans. Instr. Meas.*, **51**, 2, 282-286 (2002)
- [3] S.M. Jeon and Y. P. Kim, Temperature measurements using fiber optic polarization interferometer, *Op. Las. Tech.*, **36**, 181-185, (2004)
- [4] R. Claverie, J.P. Salvestrini and M.D Fontana, Feedback loop for electro-optic sensors, *ECAPD'8 Metz*, p134 (2006)
- [5] J.D. Bierlein and C.B. Arweiler, Electro-optic and dielectric properties of KTiOPO_4 , *Applied Physics Letters*, **49**, 15, 917-919 October 13, (1986)
- [6] N. Théofanous, M. Aillerie, M.D. Fontana, and G.E Alexakis, A frequency doubling electro-optic modulation system for Pockels effect measurements : Application in LiNbO_3 , **68**, 5, 2138-2143 (1997)
- [7] M. Aillerie, P. Kolata, J.P. Salvestrini, and M. Fontana, French patent nr 9609271 (1997)