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Noise in Vortex Matter

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ABSTRACT

The large increase in the flux-flow voltage noise, commonly observed in the vicinity of the peak-effect in superconductors, is ascribed to a novel noise mechanism. The mechanism consists in random injection of the strongly pinned metastable disordered vortex phase through the sample edges and its subsequent random annealing into the weakly pinned ordered phase in the bulk. This results in large critical current fluctuations causing strong vortex velocity fluctuations. The excess noise due to this dynamic admixture of two vortex phases is found to display pronounced reentrant behavior. In the Corbino geometry the injection of the metastable phase is prevented and, accordingly, the excess noise disappears. Excess flux-flow noise in the peak effect regime is dominated by vortex velocity fluctuations while the density fluctuations, frequently considered in the conventional flux-flow noise models, are negligibly weak. Strong nongaussian fluctuations are associated with S-shaped current-voltage characteristics. The spectral properties of the noise reflect the first order filter-like response of the dynamically coexisting vortex phases. The cutoff frequency in the spectra corresponds to the time-of-flight of vortices through the disordered part of the sample.

Keywords: vortex matter, flux-flow noise, order-disorder transition

1. INTRODUCTION

Fluctuating component of the voltage induced by motion of magnetic flux structures in a superconducting sample, commonly referred to as the flux flow noise, has been intensively studied for many years. Since its discovery in the 1960's, the flux-flow noise is regarded as a powerful tool enabling a deep insight into the dynamics of vortices. Nevertheless, a comprehensive description of the phenomenon is still lacking, for a critical review of early results see Ref. 1. In general, flux-flow noise can be attributed either to velocity or to density fluctuations of the moving flux. The major unsolved controversy regards the very origin of the flux-flow noise.^{1,2}

The most popular "shot noise model" assumes that vortex density fluctuations rigidly flowing across the sample at a constant velocity constitute the source of the flux-flow noise. Such fluctuations are expected to manifest themselves in the time-of-flight oscillations of voltage noise power spectra as well as in a strong dependence of the noise on the geometry of the voltage measuring circuit. These features are seldom, if at all, observed in the experiments. Moreover, the intensity of the experimentally measured flux-flow noise frequently exceeds by orders of magnitude the predictions of the shot noise model. Subsequent modifications of the original ideas introduced the interrupted and chained motion to account for the realistic effects of the time of flight.^{1,3,4} The noise magnitude problem has been cured by incorporating the Anderson flux bundle concept in the shot noise model.^{1,5} The flux bundle scenario, although very useful in explaining the discrepancies between the theoretical picture and the experimental reality, see e.g.,^{5,6} introduces esoteric huge flux bundles containing thousands of flux quanta, shrinking to just few flux quanta, or even nonphysical fraction of a quantum, with increasing temperature or current flow.^{1,3,5,7}

Recently, experiments involving direct SQUID detection of the magnetic noise and flux-to-voltage noise cross-correlation measurements clearly demonstrated that the noise associated with flux motion can not be explained in the framework of the existing models.^{2,7} Critical analysis of the early experiments resulted in a new model

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based entirely on velocity fluctuations caused by a turbulent flow of surface currents.² Although the model has successfully passed several experimental tests, nevertheless, it fails to explain a puzzling feature of the magnetic field and current dependent excess flux-flow noise appearing in a specific and narrow region of the H - T phase diagram.⁸⁻¹² In low- T_c superconductors the low frequency excess noise occurs in the vicinity of the peak effect (PE) below H_{c2} , where the critical current I_c anomalously increases with field.⁸⁻¹⁰ In high- T_c superconductors similar noise enhancement was found in the vicinity of the melting, or order-disorder transitions.¹¹⁻¹⁵ This unconventional noise is inconsistent with the common flux-flow noise mechanisms due to its high intensity, exceeding the usual flux-flow noise by orders of magnitude, and strongly non-Gaussian character of the fluctuations.^{1,8-10}

The excess noise in low- T_c superconductors is just one of several puzzling effects appearing in the lower part of the PE region. Along with the excess noise one observes memory effects, history and frequency-dependent dynamic response, suppression of ac response by small dc bias current, negative differential resistance, and slow voltage oscillations related to the time of flight. For example, the vortex system remembers the direction, the amplitude, the duration, and the frequency of the previously applied current. On the basis of a strong experimental evidence we have recently proposed the edge contamination model (EC) which provides a comprehensive explanation of all exotic phenomena showing out below the PE, attributing them to a dynamic coexistence of the ordered (OP) and disordered (DP) metastable vortex phase.¹⁶⁻¹⁸ In this paper we present direct experimental evidence, obtained using Fe-doped 2H-NbSe₂ crystals, that the excess noise does not result from any previously known flux-flow noise mechanism, but rather is due to a qualitatively different phenomenon of random creation and annihilation of a metastable vortex phase.

2. EDGE CONTAMINATION MECHANISM

Our current understanding of the peak effect is that it is due to the first order phase transition between quasi-ordered weakly pinned Bragg glass-like vortex phase below the PE and strongly pinned disordered solid vortex matter within and above the PE. The order-disorder phase transition of the vortex lattice occurring between two solid vortex matter phases allows for existence of a supercooled metastable DP in the part of the phase diagram occupied by the equilibrium OP. At temperatures well below the PE the supercooled phase is very fragile and any small perturbation, such as transport current, will easily anneal it into the equilibrium OP. However, at temperatures only slightly below the PE the applied current will have two competing effects: on one hand it will anneal the disorder, but on the other hand, it will contaminate the system with the fresh DP disorder resulting in a dynamic coexistence of the two phases. The injection of the disordered vortex phase through the sample edges is the core of the edge contamination mechanism.

Current flow in a superconducting sample containing the equilibrium ordered vortex phase well below the phase transition results in a uniform motion of the entire vortex lattice. The penetrating vortices enter at their proper lattice location and the order of the lattice is preserved. However, the presence of surface barriers in real samples significantly changes the situation. Since the barrier height is sensitive to the surface quality, vortices penetrate predominantly at the weakest spots of the barrier, and locally destroy the ordered lattice. Far below the phase transition the disordered state is highly unfavorable energetically and anneals rapidly into OP. However, in the close vicinity below the order-disorder phase transition a metastable DP will be formed near the sample edge. Since near the phase transition the free energies of the two phases are comparable, the metastable DP becomes sufficiently stable on the relevant experimental time scales and gradually penetrates deep into the sample with the flow of the entire lattice.^{16,17} Since the DP can be pinned more efficiently it is characterized by significantly larger critical current than the weakly pinned ordered vortex phase.^{19,20} The contamination process causes thus an enhancement of the total integrated critical current of the sample. A strongly pinned metastable disordered vortex phase dynamically anneals in the bulk into an ordered phase with much smaller critical current. Randomness in the DP injection (injection noise) and randomness in its annealing (annealing noise) into the OP results in strong fluctuations of the instantaneous critical current and a pronounced voltage noise.

Let us characterize the DP by the local critical current density $J_c(x)$ which has a non-equilibrium excess value $\tilde{J}_c(x) = J_c(x) - J_c^{ord}$ relative to the critical current of the fully annealed OP. Since in low-temperature superconductors thermal activation is negligible, the sole annealing mechanism is through a current-driven displacement that allows rearrangement of the vortices during the motion. The relative annealing of \tilde{J}_c upon displacement by a small Δx is therefore given by $\Delta x/L_r$, where L_r is a characteristic relaxation length over which the DP

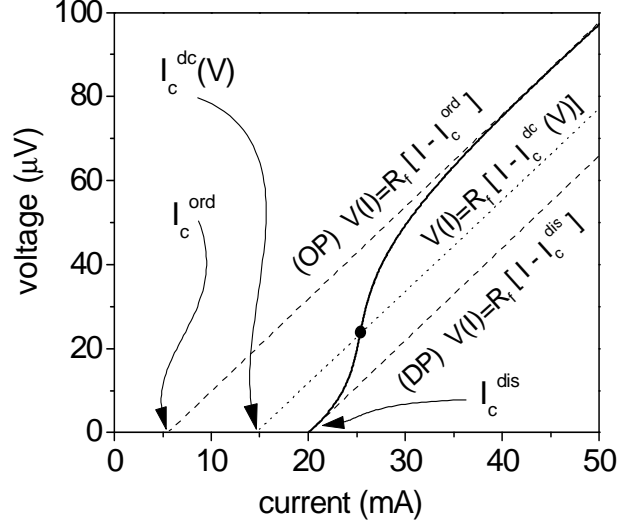


Figure 1. Numerically simulated $V - I$ characteristics, thick line, of coexisting vortex phases at a given dc current bias. The asymptotic characteristics of fully ordered and fully disordered vortex phases are shown with dashed lines.

anneals into the OP. Since the lattice flows with velocity v , \tilde{J}_c at $x + \Delta x$ and at time $t + \Delta t = t + \Delta x/v$ is thus described by $\tilde{J}_c(x + \Delta x, t + \Delta x/v) = \tilde{J}_c(x, t)(1 - \Delta x/L_r)$, which leads to the partial differential equation of the annealing process²¹

$$\partial \tilde{J}_c(x, t) / \partial x + (1/v) \partial \tilde{J}_c(x, t) / \partial t = -\tilde{J}_c(x, t) / L_r(v), \quad (1)$$

with a boundary condition at $x = 0$, where vortices penetrate into the sample, of $\tilde{J}_c(0, t) = J_c^{dis} - J_c^{ord}$. A key aspect of the annealing process is that the relaxation length L_r crucially depends on the displacement velocity v and on the proximity to the phase transition. Close to the phase transition the metastable DP is rather stable and L_r is large. Deeper into the OP region the metastable phase becomes more and more unstable, L_r is small and I_c is depressed. Fast transient measurements²⁰ show that L_r decreases with increasing vortex displacement velocity according to an empirical relation $L_r \simeq L_0(v_0/v)^\eta = L_0(V_0/V)^\eta$. Here η is typically in the range of 1 to 3, L_0 , v_0 , and V_0 are scaling parameters, $V = vBl$ is the measured voltage drop, B is the magnetic field, and l is the distance between the voltage contacts.

The dc solution of (1) reads $J_c^{dc}(x) = (J_c^{dis} - J_c^{ord}) \exp(-x/L_r) + J_c^{ord}$ and the integrated dc critical current becomes

$$I_c = d \int_0^W J_c^{dc}(x) dx = (J_c^{dis} - J_c^{ord}) [1 - e^{-\frac{W}{L_r(V)}}] L_r(V) d + I_c^{ord}, \quad (2)$$

where $I_c^{ord} = J_c^{ord} W d$, W is sample width and d thickness. Observe, that I_c depends on L_r , which in turn depends on voltage V . To evaluate the shape of the $V - I$ characteristics in the EC scenario assume, for simplicity, that the flux-flow resistance R_f of DP and OP is the same. Then the asymptotic $V - I$ characteristics for the DP and OP are $V = R_f(I - I_c^{dis})$ and $V = R_f(I - I_c^{ord})$, respectively. When the DP and OP coexist $V = R_f(I - I_c)$ with the voltage dependent I_c given by Eq. 2. An example of the non-linear $V - I$ characteristic obtained by means of numerical simulations is shown in fig. 1. At very low voltages L_r is larger than the sample width, the entire sample is contaminated by the DP, and the $V - I$ initially follows the asymptotic dashed line of the DP with $I_c = I_c^{dis}$, where $I_c^{dis} = J_c^{dis} W d$. At high vortex velocities L_r becomes very short, most of the sample is in the OP, and the $V - I$ approaches the asymptotic line of the OP with $I_c = I_c^{ord}$, where $I_c^{ord} = J_c^{ord} W d$. In the crossover region, due to a continuous decrease with current of the total I_c , a nonlinear $V - I$ characteristic is obtained. The curvature in the crossover region depends on the parameters η , L_0 , and V_0 . Our numerical simulations show that with rapidly decreasing L_r one may even obtain a negative slope resulting in S-shaped $V - I$ characteristics.

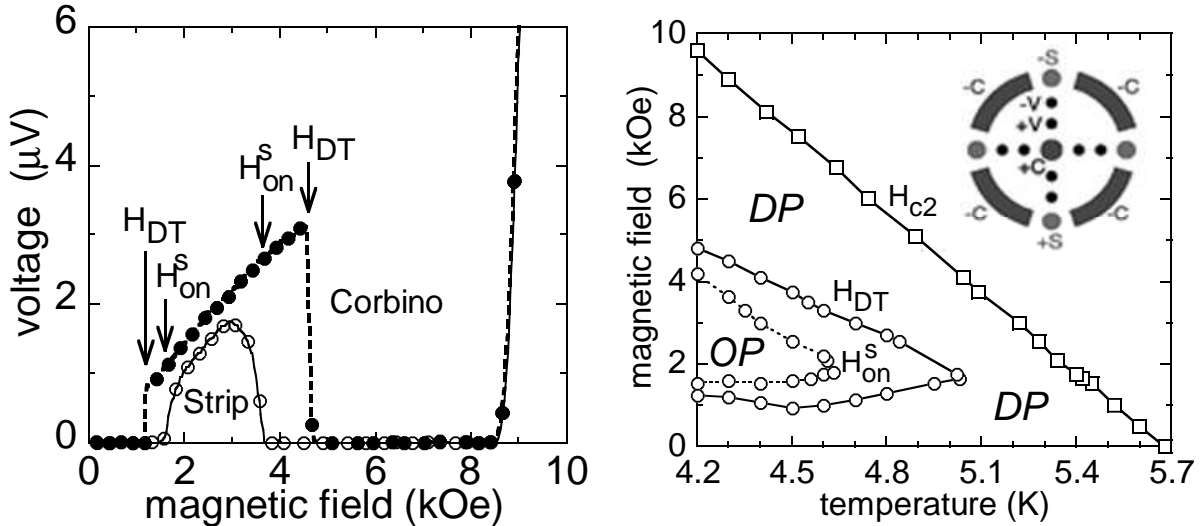


Figure 2. a) dc voltage seen in the same sample in Corbino and strip geometry. The current flow in Corbino and strip has been adjusted to provide equal current density in the vicinity of voltage contacts for both geometries. b) Phase diagram of vortex matter in Fe-doped NbSe-2. Dynamic coexistence of DP and OP occurs in the area contained between the H_{DT}^o and H_{on}^s lines. Inset: contact configuration enabling measurements in both, Corbino and strip geometry. By applying the current to the +S, -S contacts, the vortices penetrate through the edge and flow across the sample, similarly to the standard strip configuration. In contrast, by applying the current to the +C, -C contacts, the vortices circulate in the bulk without crossing the edges, as in a Corbino disk. In both configurations the voltage and the corresponding noise are measured across the same contacts +V, -V.

3. ORDER-DISORDER PHASE TRANSITION

In the Corbino disk geometry the vortices circulate in the bulk without crossing sample edges. In such arrangement the contamination by DP is avoided and the true bulk properties of the vortex matter can be investigated. In order to perform transport and noise measurements in both the Corbino and strip-like geometry on the same crystal we have prepared a special contact configuration, see inset to fig. 2b.¹⁷ The experiments discussed here were executed using Fe-doped (200 ppm) 2H-NbSe₂ single crystal $2.2 \times 1.5 \times 0.04$ mm³ large with $T_c=5.7$ K.¹⁷ Similar results were obtained on a number of additional crystals in various configurations. Figure 2a shows the dc voltage response V vs. the magnetic field applied parallel to the crystal c -axis at 4.4 K in the strip and Corbino disk configuration. Since in the Corbino disk the current density varies across the sample, we have applied different driving currents in two geometries in order to have the same average current density between +V,-V contacts in both arrangements. As a result, the measured V and the corresponding vortex velocity are identical at high fields. Upon decreasing the field from above $H_{c2}(T)$, the voltage decreases rapidly and vanishes in the PE region (4 to 8 kOe), where I_c of the sample is large due to the presence of the strongly pinned DP. The voltage appears again at intermediate fields between the phase transition fields H_{DT} . In this field range the voltage in the Corbino disk increases linearly with H , consistently with the well known flux-flow behavior, indicating that the flowing lattice is in the ordered phase. The sharp drop of the voltage response at each H_{DT} is due to an abrupt disorder-driven transition of the equilibrium OP into a highly pinned equilibrium DP. The existence of two transition fields indicates the reentrant behavior of the equilibrium DP in the iron doped NbSe₂.^{17,22} The area of the phase coexistence in the phase diagram, see fig. 2b, appears always on the Bragg glass side of the transition. Therefore at low fields we face a mirror-like image of high fields behaviour.

The voltage response of the strip configuration is restricted to a narrower field range contained between high and low onset H_{on}^s fields. The strip voltage between strongly suppressed relative to the Corbino, indicating stronger effective pinning as a result of an intermixture of the DP with the OP due to the EC mechanism. Figure 2b shows the phase diagram of the iron doped NbSe₂ determined in the course of transport measurements of Corbino and strip geometry.

4. DYNAMIC CREATION AND ANNIHILATION OF METASTABLE VORTEX PHASE AS A SOURCE OF EXCESS NOISE

The generation of the metastable DP is a random process due to the non-uniform penetration of vortices through the surface barrier. As a result, the degree of vortex-lattice disorder and the corresponding value of J_c^{dis} at the sample edge are random functions of time. Similarly, annealing of the flowing DP is a random process that can be taken into account by considering L_r to be a random variable. Since J_c^{dis} is typically an order of magnitude larger than J_c^{ord} ,¹⁷ random variations δJ_c^{dis} and δL_r will result in large fluctuations of the integrated critical current of the sample, causing large voltage noise.

4.1. Simplified model of the noise

The $V(I)$ curve in the vicinity of the peak effect can be correctly approximated by $V(I) = R_f[I - I_c(V)]$, where I_c given by Eq. 2. In the small signal approximation we separate voltage fluctuations into two terms:

$$\delta V(I) \approx \frac{\partial V(I)}{\partial I_c} \delta I_c + \frac{\partial V(I)}{\partial R_f} \delta R_f. \quad (3)$$

Neglecting, for simplicity, the critical current dependence on voltage, i.e., assuming that the $V(I)$ characteristics is linear above I_c one finds by differentiating the $V(I)$ equation that

$$\frac{\partial V}{\partial I_c} = -\frac{\partial V}{\partial I} \equiv -R_d, \quad (4)$$

and (3) becomes

$$\delta V(I) = -R_d \delta I_c + \frac{V(I)}{R_f} \delta R_f. \quad (5)$$

Since experimentally L_r is usually smaller than W we can approximate¹⁶ (2) by $I_c \simeq L_r d(J_c^{dis} - J_c^{ord}) + W d J_c^{ord}$. In this approximation the fluctuation of the total critical current is

$$\delta I_c \approx d \delta \tilde{J}_c(0) L_r + d \tilde{J}_c(0) \delta L_r. \quad (6)$$

From Eg. 5 we obtain that

$$\delta V(I) \approx -d R_d \tilde{J}_c(0) L_r \left[\frac{\delta \tilde{J}_c}{\tilde{J}_c} + \frac{\delta L_r}{L_r} \right] + V(I) \frac{\delta R_f}{R_f}. \quad (7)$$

We write now the power spectral density (PSD) of the voltage noise as

$$S_V \approx d^2 R_d^2 \tilde{J}_c^2(0) L_r^2 S_{in/ann} + V^2 S_{r_f}, \quad (8)$$

where $S_{r_f} = S_{R_f}/R_f^2$ is the normalized spectral density of the flux-flow resistance fluctuations and $S_{in/ann}$ is the normalized spectral density of the vortex injection/annealing noise. The most important conclusion that will enable us to understand the excess noise dependence on applied magnetic field and current flow is that the noise intensity is proportional to the product of $R_d^2 \tilde{J}_c^2(0) L_r^2$.

4.2. Experimental results

The most direct test of the EC mechanism is the confrontation of the Corbino disk noise with that of the strip arrangement, as shown in fig. 3. In the Corbino the excess noise is almost entirely absent indicating that the randomness in motion of the vortex lattice within the bulk of the sample does not, by itself, create excess noise. The absence of the noise in the Corbino clearly indicates the dominant role of the edge contamination in the noise process. The residual small and narrow peaks in the Corbino noise in fig. 3 can be ascribed to small deviations from a perfect Corbino disk configuration. Since L_r diverges at H_{DT} , any small non-radial part of the current may result in some injection of the metastable DP, giving rise to noise. Similarly, small inhomogeneities in the quenched disorder may result in a slightly position-dependent H_{DT} . In this case, in a narrow field region in the vicinity of the mean-field H_{DT} some parts of the sample are in the equilibrium DP, whereas others are in the

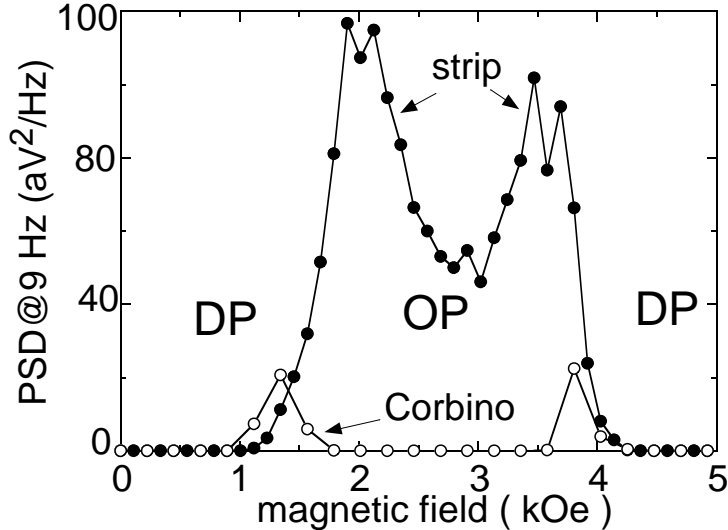


Figure 3. Power spectral density of noise at 9 Hz in Corbino (open symbols) and strip (full symbols) geometry.

OP. When the entire lattice is set in motion the DP drifts into regions of the OP, where it becomes metastable, and may cause noise in this narrow field region.

In contrast, the strip noise is very pronounced. The peak of the noise around 3.5 kOe is a result of the large L_r in the vicinity of the phase transition. The second noise peak at about 2 kOe marks the reentrant phase transition at which L_r becomes large again on approaching H_{DT} . This low-field peak was not previously observed since the noise studies were carried out on undoped NbSe₂⁸⁻¹⁰ which does not show a pronounced reentrant disorder-driven transition. The existence of two demonstrates that the excess noise is not a mere result of the fact that I_c increases with H at the PE since at low fields the same excess noise is found in the region where I_c decreases with H . Furthermore, the same value of I_c is attained at three values of H : above the reentrant H_{DT} where I_c decreases with H , below the high field H_{DT} where I_c increases with H , and in the upper part of the PE, above the high field H_{DT} where I_c decreases again with H . The excess noise occurs only in the first two cases, where the metastable DP contaminates the equilibrium OP. In the third case, above H_{DT} , the DP is the thermodynamically stable phase and therefore no ‘wrong’ phase is generated at the edges.

Figure 4 shows the intensity of the noise $S_V^{1/2}$, seen at a selected frequency of 3 Hz, as a function of bias current, along with the $V - I$ characteristics for two different values of applied magnetic field. In each case, the onset of the noise coincides with the onset of dc current induced dissipation. With increasing current the $I - V$ curve shows an upturn and eventually approaches a linear flux-flow behavior at elevated currents. The noise displays a large peak and vanishes rapidly at higher currents. Assuming for simplicity that δJ_c^{dis} is current independent, the dominant parameters effecting the noise intensity are the relaxation length L_r and the differential resistance dV/dI , see eq. (8). The initial buildup of the noise with increasing current follows the initial growth of R_d . The subsequent decay of the noise is the result of a decrease of L_r with increasing vortex velocity. Indeed, above 28 mA the $V - I$ characteristic approaches the linear behavior of the OP, indicating that most of the sample volume is in the OP and that L_r is small. Since the ordered part of the sample does not contribute to the noise, the noise vanishes as the width of the DP near the edge shrinks to zero. The specific details of the above qualitative description are expected, however, to be significantly more complicated because of several factors, including the conceivable current dependence of δJ_c^{dis} and the fact that δV is often comparable to V , resulting in a highly nonlinear and apparently non-Gaussian response,^{8,9} for which the above oversimplified analysis is not valid.

The above considerations facilitate the analysis of the general behavior of the strip noise shown in fig. 5. At low currents, 18 mA, vortex motion occurs only in the central field region far away from H_{DT} . In the vicinity of the transition the integrated I_c of the strip is larger than the driving current due to the large L_r . As a result, the excess noise is present only in the central field range. At 23 mA, the field range of the observable vortex motion

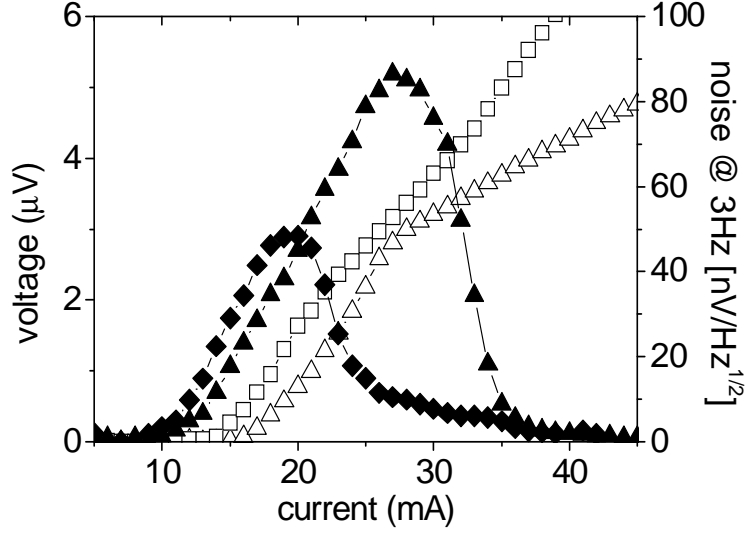


Figure 4. $V - I$ characteristics (open symbols) and spectral intensity of the noise at a fixed frequency of 3 Hz (full symbols) at the frequency of 3 Hz as a function of bias current at 4.2 K: triangles - 2 kOe, diamonds - 3 kOe.

and of the corresponding noise expands and two noise peaks become already apparent. In the central region the DP is less stable, L_r drops with I , and hence the noise decreases rapidly with the current. Closer to the transition fields, however, the metastable DP is much more stable and therefore even at 23 mA L_r remains large and noise is still increasing with current. At 36 mA most of the sample is already in the OP and the noise in the central field range has accordingly dropped by two orders of magnitude. The strong excess noise is restricted now only to the narrow regions adjacent to the transition fields where the metastable DP survives even at high vortex velocities.

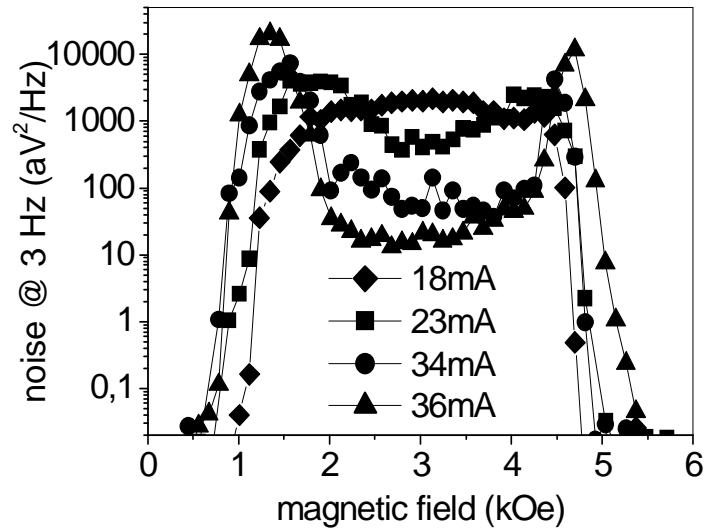


Figure 5. Power spectral density of the strip noise at a fixed frequency of 3 Hz in a function of magnetic field at various bias currents. $T=4.2$ K.

4.3. Velocity vs. density fluctuations

Electric field due to magnetic flux motion with a velocity v , neglecting voltages induced by variations of the flux threading the loop composed of voltage measuring leads, can be written simply as $\mathbf{E} = -\mathbf{v} \times \mathbf{B}$. The voltage fluctuations $\delta V(t) = V(t) - \bar{V}$, where $\bar{V} = vBl$ is the dc voltage, can be due either to the fluctuations of magnetic field $\delta \mathbf{B} = \Phi_0 \delta n \frac{\mathbf{B}}{B}$, fluctuations of the vortex density n , or to the fluctuations of the vortex velocity \mathbf{v} . In a small signal approximation

$$\delta V \approx l(\delta B v + B \delta v). \quad (9)$$

The first term contains density fluctuations $\delta n = n(t) - \bar{n}$, where $\bar{n} = B/\Phi_0 Wl = N/Wl$ is the equilibrium vortex density and N is the total number of vortices. Vortex density fluctuations can be therefore directly evaluated by measuring the associated magnetic field noise. The second term describes velocity fluctuations $\delta v = v(t) - \bar{v}$, where the equilibrium vortex velocity $\bar{v} = \bar{V}/Bl$. Alternatively, the fluctuating component of the voltage due to current driven vortex motion is given by (3). Direct confrontation of Eq. (9) with Eq. (5) suggest to associate vortex density fluctuations with the fluctuations of the flux-flow resistance δR_f and fluctuations of the vortex velocity with the fluctuations of the critical current $\delta \tilde{J}_c(0)$.

In the experiments we have measured simultaneously the voltage and magnetic field noise by placing our NbSe₂ crystal with attached current and voltage leads directly on the top surface of the 2DEG Hall sensor array. A dedicated 2DEG Hall sensor array based on AlGaAs/GaAs heterostructures has been grown on undoped semi-insulating oriented GaAs substrates by means of molecular beam epitaxy.²³ The employed sensor configuration consisted of eleven $10 \times 10 \mu\text{m}^2$ Hall sensors, connected in series with a $30 \mu\text{m}$ separation between them. The active 2DEG layer resides only about $0.1 \mu\text{m}$ below the structure surface. The sensitivity of our Hall sensors to the applied magnetic field was close to $100 \text{ m}\Omega/\text{gauss}$. Hall sensor bias current causing onset of the excess shot noise was well above $200 \mu\text{A}$ level enabling us to operate safely at high currents what significantly improved the signal to noise ratio. The ultimate sensitivity of our flux detection system was typically better than $10^{-3} \text{ gauss}/\text{Hz}^{1/2}$ at the frequencies above 5 Hz. The entire arrangement was immersed in a specially designed low noise variable temperature cryostat equipped with an external μ -metal magnetic screen and a persistent mode superconducting coil. In each experimental run the sample has been slowly cooled in zero field to the required temperature before application of the magnetic field and bias current.

We have looked for the flux noise manifestations in the entire range of current, magnetic field, and temperature where the excess voltage noise appears. Within the sensitivity of our Hall probe arrangement we could not detect

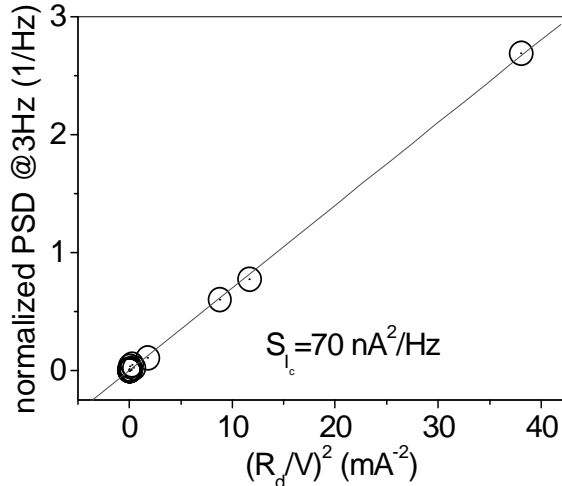


Figure 6. Data points at 2 kOe from fig. 4 plotted as a normalized power spectral density in a function of the R_d^2/V^2 ratio. Observe that the best linear fit to the data crosses the zero indicating that the voltage noise is due entirely to the density fluctuations, see the text.

any fluctuations of the vortex density. Even by biasing the sample at the very maximum of the voltage noise, where the spectral intensity increases more than 4 orders of magnitude above the preamplifier background, we have not seen any difference in the magnetic noise detected with and without current flow.

In the face of the negative result we have carefully checked and verified that the Hall probe is properly coupled to the sample by measuring the Meissner effect at low fields and self-induced ac field response to ac transport current. All tests proved unambiguously that the Hall sensors are properly operating and the absence of the flux noise signal is not due to unskillfully performed experiment.

The absence of the flux noise can be shown to be, in fact, not surprising and consistent with the EC model predictions. Let us rewrite the total spectral density of the voltage noise (5) in terms of the normalized spectral density $S_v = S_V/V^2$.

$$S_v = \frac{1}{R_f^2} S_{R_f} + \frac{R_d^2}{V^2} S_{I_c}, \quad (10)$$

By plotting the normalized voltage noise spectral density as a function of the ratio R_d^2/V^2 one can separate contributions of the fluctuating vortex density and velocity to the total noise. The PSD value for $R_d^2/V^2 = 0$ corresponds to S_{R_f} , which in turn describes vortex density fluctuations, while the slope of the $S_V(R_d^2/V^2)$ plot gives the spectral density of the critical current fluctuations S_{I_c} .

The experimental data relative to 2 kOe in figure 4, re-plotted in the above coordinate system, are shown in fig. 6. The fit of the data to a linear dependence crossing the zero clearly demonstrates that the excess noise caused by the contamination mechanism is entirely dominated by the critical current fluctuations causing strong velocity fluctuations in the flowing vortex system. Any significant density fluctuations would offset the linear fit upward, such that it would cross the y-axis at the value corresponding to S_{R_f} , see eq. (10). This is clearly not the case in fig. 6. The fit crosses the zero within the error of 10 ppm. The slope of the linear fit corresponds to the spectral density of the critical current noise of $70.1 \pm 0.03 \times \text{nA}^2/\text{Hz}$.

4.4. Nongaussianity of the noise and V-I curves

The nongaussian character of the noise is most pronounced at low fields, close to the dissipation onset. We attribute the nongaussian fluctuations to the shape of the $V - I$ curve. In the presentation of the noise model we have pointed out that a rapid decrease of L_r with increasing vortex velocity (driving current) leads to appearance of a negative resistance resulting in S-shaped $V - I$ characteristics. Our numerical simulation shows that this is particularly prone to occur at low currents close to the dissipation onset. When the strip is current biased within

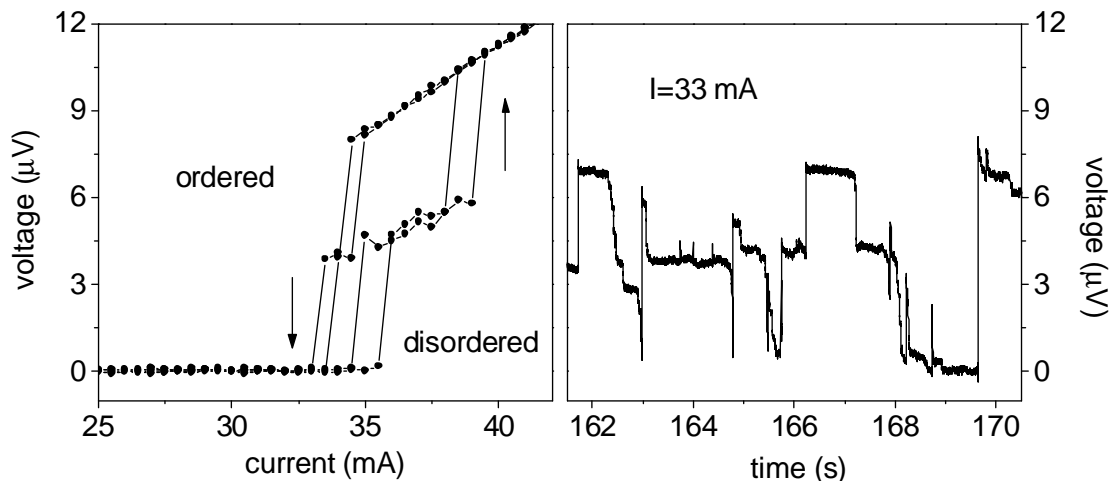


Figure 7. a) Strongly nonlinear double S-shape $V - I$ characteristics. b) The corresponding time record of the voltage seen at the current flow of 33 mA takes form of a 3-level telegraph noise.

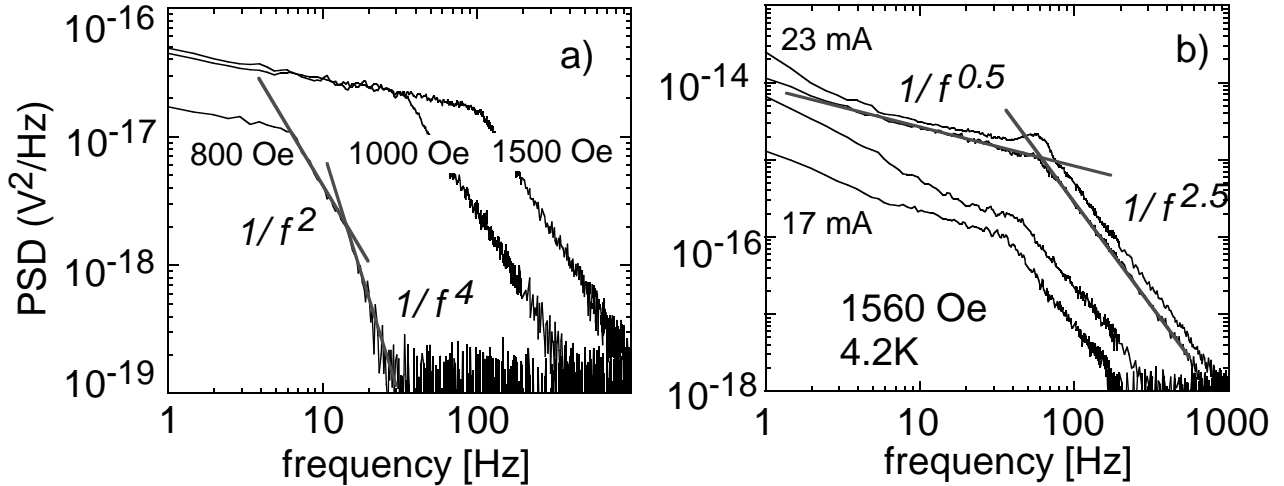


Figure 8. Power spectra at low fields in the vicinity of the reentrant phase transition.

the S-shape range then the vortex system may spontaneously jump between two branches of the $V - I$ curve, see fig. 7, corresponding to random switching between more ordered and more disordered vortex phase. The resulting waveform of the noise will be close to that of extremely non-Gaussian random telegraph signal (RTN). We have observed several manifestations of this type of fluctuations at low fields close to the reentrant transition. The analysis of the phenomena is far from being complete and we present here in fig. 7 just an example of the S-shape $V - I$ characteristics and the corresponding 3-level RTN-like noise waveform.

4.5. Spectral properties

In the entire range of current, magnetic field and temperature the excess noise power spectra display general $1/f^\alpha$ -like power-law behavior, similar to that previously in the vicinity of the PE.⁸⁻¹⁰ The shape of the spectra strongly depends on applied magnetic field and driving current. In general, the noise intensity and the power exponent α vary as a function of applied field, whereas changes in the driving current result only in changes of spectral intensity without affecting the functional form of the spectra. Nevertheless, many spectra demonstrate a pronounced kink associated with an abrupt change in the power-law exponent. The appearance of a kink in the spectra has been previously related to the inverse transit time of the vortices across the sample.^{8,11,12}

At low fields, close to the reentrant phase transition, and at low frequencies below the kink, the spectra can be well fitted to the power law with $\alpha = 0.5$. At high frequencies, above the kink, the power exponent changes to $\alpha = 2.5$, see fig. 8a. When the RTN-like noise appears, and its cutoff frequency is lower than the frequency of the kink, then an exponent $\alpha = 2$ is observed at frequencies between the RTN lorentzian cutoff and the kink frequency. At frequencies above the kink the power exponent increases to $\alpha = 4$, as can be seen in fig. 8b. With further increase of the applied field the noise spectrum becomes close to $1/f$ at low frequencies. In such spectra we observe power law-like dependence with $\alpha = 3$ at frequencies above the kink, see fig. 9a.

The increasing current initially does not influence the exponent α and only increases the kink frequency and noise intensity. Nevertheless, at very high currents the annealing process is very rapid and when entire sample is in the OP, $V - I$ characteristic becomes linear, and the power spectrum of the strip noise takes the form of $1/f^{3/2}$. Observe that the same type of the spectral functional dependence appears in the residual noise of the Corbino disk, see fig. 9b. We want to point out that the same $1/f^{3/2}$ spectral dependence has been recently ascribed to the nonequilibrium excitations and thermal fluctuations of quasiparticle density in very fast moving vortex cores.²⁴ Since in our experiments the $1/f^{3/2}$ spectrum appears not only at very high current densities in the strip configuration but also characterizes the Corbino noise at relatively low vortex velocities, we believe

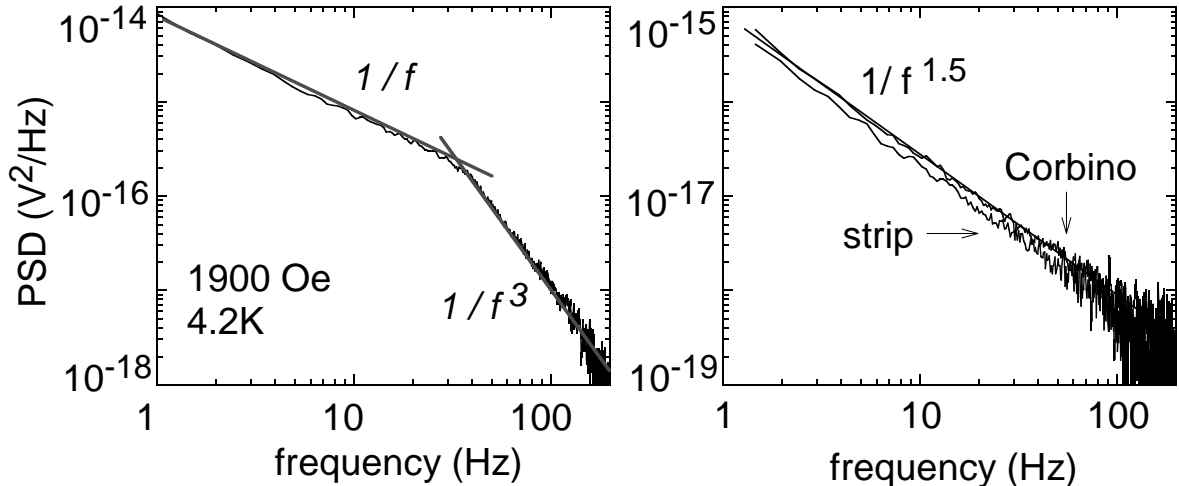


Figure 9. a) Power spectra at high fields. b) Power spectra of the residual noise in Corbino disk and of the strip noise at very high driving currents.

that the $1/f^{3/2}$ noise spectrum should be rather associated with noise due to the motion of the ordered vortex phase.

The observed spectral behavior is consistent with the described model as confirmed by our numerical simulations, and a simplified frequency response model. Treating the strip containing a mixture of vortex phases as a linear time invariant system (LTI) we deduce that the pulse response of our system is of the $1/\tau \exp(t/\tau)$ type, leading to the frequency characteristics identical to that of a first order low-pass filter:

$$H(\omega) = \frac{S_{in}}{1 + (\omega\tau)^2}, \quad (11)$$

where S_{in} is the power spectrum of any input signal that appears at the input terminal of the considered LTI system, including the injection and annealing noise $S_{in/ann}$. The time constant

$$\tau = 2\pi L_r t_t / W \quad (12)$$

determines the cutoff frequency $f_c = 2\pi/\tau$ of the first order filter and t_t is the time of flight of vortices across the sample. The cutoff frequency coincides with the kink frequency f_c at which the power exponent of our spectra changes by a factor of 2.

$$t_t = W/\bar{v} = W \frac{Bl}{\bar{V}} \quad (13)$$

The evolution of the cutoff frequency with applied magnetic field is illustrated in fig. 10a. Observe that for each value of the applied magnetic field (13) enables one to determine the time-of-flight t_t from the measured dc voltage \bar{V} . Figure 10b shows the data points from fig. 10a plotted now as a ratio f_c/f_t vs. t_t , where the time of flight frequency $f_t = 1/t_t$. Note that in the wide range of magnetic fields the ratio is close to 1. It follows from (12) that $f_c = f_t$ when $L_r = W$ indicating that the cut-off frequency is given by the time of flight of vortices across the width L_r , i.e., across the disordered part of the sample. Indeed, the ratio upturns for the magnetic fields at which the relaxation length starts to be smaller than the sample width W . Hence, spectral measurements provide a new way to determine the relaxation length L_r and its evolution with experimental parameters.

5. CONCLUSIONS

The excess flux-flow noise appearing in the vicinity of the peak effect has been ascribed to a new mechanism of edge contamination and has been shown not to result from mere random motion of vortices in the bulk of the

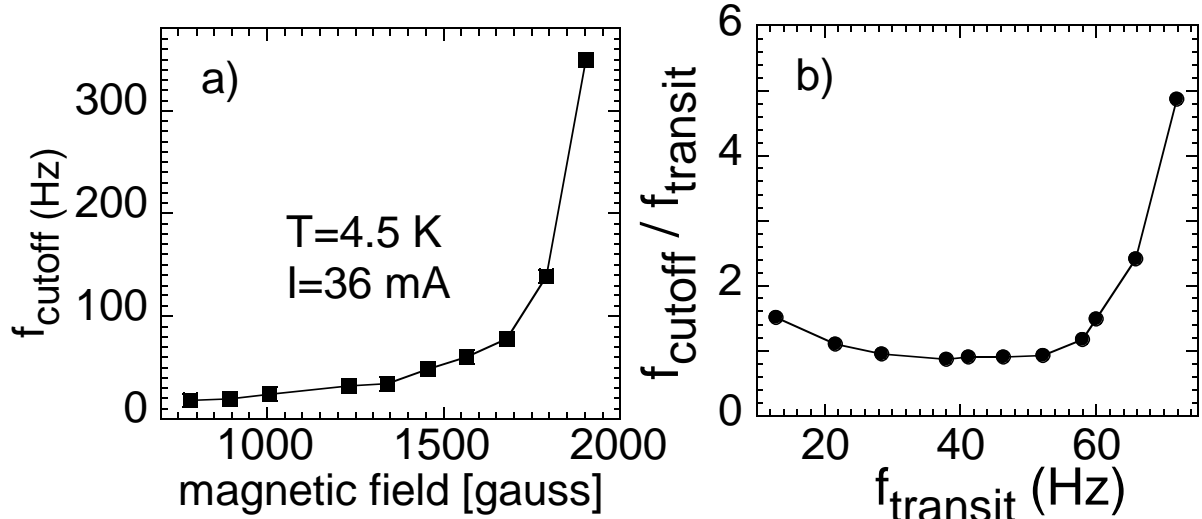


Figure 10. a) Kink frequency as a function of applied magnetic field. b) The data from Fig. 10a plotted as a ratio between the kink and transit frequency $f_t = 1/t_t$ in function of t_t . The ratio close to 1 indicates that the relaxation length L_r exceeds the sample width E .

sample. The main conceptual difference is that in the conventional models only random vortex penetration or irregular vortex motion in the bulk is considered. In contrast, we have described a mechanism where random vortex penetration locally creates a new vortex matter phase, which may sustain a tenfold larger critical current than the equilibrium phase. This ‘contamination’ process is particularly prone to occur near the PE where a ‘wrong’ metastable disordered phase, generated at the sample edges in the presence of a driving current, is sufficiently stable on the relevant experimental time scales. The random generation and annealing processes of the metastable DP result in large fluctuations in the instantaneous I_c of the sample, leading to very large voltage noise. Accordingly, we have demonstrated that the excess noise can be eliminated by preventing the formation of the ‘wrong’ phase in the Corbino disk geometry.

Direct flux noise measurements and re-examination of the voltage noise data brought us to conclusion that the excess flux-flow noise is entirely dominated by vortex velocity fluctuations resulting from the critical current fluctuations. This result may seem surprising to the reader familiar with the experimental evidence of a strong local vortex density noise associated with current driven motion of vortices in high- T_c $\text{Bi}_2\text{Sr}_2\text{CaCu}_2\text{O}_y$ (BSCCO) single crystals.¹⁵ The flux noise in BSCCO system has been detected using a similar 2DEG Hall probe arrangement with a similar sensitivity. The major difference between the investigated low- T_c system and high- T_c BSCCO that may account for such pronounced difference in noise behavior is the fact that in the low- T_c system the noise is associated with order-disorder transitions within the solid state of the vortex matter. In a marked difference, in BSCCO the excess noise can be associated with the melting transition of the vortex matter.^{11–15} Since vortex liquid has higher density than the solid, the local melting transition may result in strong density fluctuations, whereas density difference between the ordered and disordered solid is negligible.

The spectral response of the sample to the injection/annealing noise is equivalent to that of a first order low pass filter response with a cut-off frequency given by the time of flight of vortices across the disordered part of the sample. In order to extract more detailed information from the noise spectra, one needs, however, detailed microscopic theories of the generation, annealing, and disentanglement processes of the driven metastable DP, which are currently unavailable. Since the thermodynamic disorder-driven transition H_{DT} is apparently of first order,¹⁷ one may expect that the annealing process of the ‘supercooled’ disordered phase occurs through a random nucleation and growth mechanism. These important aspects of vortex dynamics have not been addressed previously and call for further theoretical and experimental studies.

We believe that the new noise mechanism may be of importance for various condensed matter systems

exhibiting similar noise associated with a fluctuating pinning force such as incommensurate charge density waves or Wigner crystals in two-dimensional electron gas.

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