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Discussion on: “Sensor Gain Fault Diagnosis for a Class of Nonlinear Systems”

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1 Introduction

The paper by Y. Wang and D. H. Zhou [1] presents an approach of sensor gain fault detection of nonlinear systems. The first step of this approach consists on the location of the sensor gain faults that can be estimated. The proposed algorithm is based on the computation of the failure matrix D such that the zeros of the linear part of the system $(A, 0, C, D)$ are stable. The second step is the simultaneous estimation of the state and the fault vectors using the singular systems representation given in [2]. Finally, the sensor gain faults are estimated using an adaptive estimator. This paper is an interesting contribution to the sensor gain faults diagnosis of nonlinear systems provided that the proposed approach gives both the location and the estimation of the failure. This discussion focuses on the existence conditions of the simultaneous estimation of the state and the fault vector and on the selection of the conditionally identifiable faults. It is shown first that the detectability of the pair (A, C) is not necessary and only the measurement provided by the conditionally detectable sensors are necessary to estimate the state of the system. An estimation of the fault vector f is then given by the output of the observer using the conditionally identifiable sensors. Thereafter, we claim that the simultaneous estimation scheme can be simplified using a low order observer and without using descriptor systems formulation. An n^{th} -order state observer and a q^{th} -order functional observer which estimates the conditionally identifiable faults are then proposed. Finally, an algorithm to determine the matrix D based on a detectability condition is exhibited.

2 On the existence conditions of the observer

This section is devoted to the analysis of the existence conditions of the observer proposed in [1] when the singular systems description is used. More precisely, the necessary condition of the linear part of the system is investigated using an output transformation. The singular state-space formulation is therefore not necessary.

2.1 Problem reformulation using an output transformation

In this section, it is assumed that the conditionally identifiable sensor gain faults, i.e. the matrix D , have been computed using the algorithm proposed by Y. Wang and D. H. Zhou [1]. The considered system is given by eq. (12) in the paper [1]

$$\dot{x} = Ax + g(x, u, t) + Bu \quad (1a)$$

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$$y = Cx + Df_D \quad (1b)$$

with $x \in \mathbb{R}^n$, $f_D \in \mathbb{R}^q$, $y \in \mathbb{R}^m$ and $\text{rank } D = q$. As in [1] (Assumption 2), $g(x, u, t)$ is assumed to be globally Lipschitz with respect to x :

$$\|g(x_1, u, t) - g(x_2, u, t)\| \leq \lambda \|x_1 - x_2\|, \forall u, \forall t \geq 0 \quad (2)$$

where $\lambda > 0$ is the Lipschitz constant.

First, we propose an output transformation to isolate the free fault component y_1 of the measurement equation to the faulty measurement y_2 . Thereafter, it will be shown that only y_1 is necessary to estimate the state x and y_2 is only used to deduce the sensor fault estimation f using the state estimation. Recall that the matrix D is of full column rank, i.e. $\text{rank } D = q$, with at most only one '1' in each row. Then there exist two non singular permutation matrices $V \in \mathbb{R}^{m \times m}$ and $W \in \mathbb{R}^{q \times q}$ such that

$$VDW = \begin{bmatrix} 0 \\ I_q \end{bmatrix}, VC = \begin{bmatrix} C_1 \\ C_2 \end{bmatrix}, \begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = Vy \text{ and } f = W^T f_D \quad (3)$$

Using this output transformation, the system (1) is then equivalent to

$$\dot{x} = Ax + g(x, u, t) + Bu \quad (4a)$$

$$y_1 = C_1 x \quad (4b)$$

$$y_2 = C_2 x + f \quad (4c)$$

with $y_1 \in \mathbb{R}^{m_1}$ ($m = m_1 + q$). In the sequel and without loss of generality, we assume that the system is of the form (4). Notice that equations (4b) and (4c) correspond to the structure of matrix D given by eq. (7) in [1].

2.2 State and sensor fault estimation using a singular systems framework

2.2.1 Existence conditions of the observer

Using the approach given in [2], the authors rewrite system (4) as a singular system as follows

$$E\dot{\bar{x}} = M\bar{x} + g(x, u, t) + Bu \quad (5a)$$

$$y = H\bar{x} \quad (5b)$$

with

$$\bar{x} = \begin{bmatrix} x \\ f \end{bmatrix}, E = \begin{bmatrix} I_n & 0 \end{bmatrix}, M = \begin{bmatrix} A & 0 \end{bmatrix}, H = \begin{bmatrix} C_1 & 0 \\ C_2 & I_q \end{bmatrix}$$

It is easy to see that system (5) is observable at infinity [3] since $\text{rank} \begin{bmatrix} E \\ H \end{bmatrix} = \dim \bar{x} = n + q$. It follows from this property that the necessary condition for the existence of an observer is reduced to the following detectability condition [3, 4]

$$\text{rank} \begin{bmatrix} \mu E - M \\ H \end{bmatrix} = n + q, \forall \mu \in \mathbb{C}, \text{Re}(\mu) \geq 0 \quad (6)$$

which can be expressed (see [2]) as minimum phase condition by the use of the expressions of matrices E , M and H

$$\begin{aligned} \text{rank} \begin{bmatrix} \mu E - M \\ H \end{bmatrix} &= \text{rank} \begin{bmatrix} \mu I_n - A & 0 \\ C & D \end{bmatrix} = n + q, \forall \mu \in \mathbb{C}, \text{Re}(\mu) \geq 0 \\ \iff \text{rank} \begin{bmatrix} \mu I_n - A & 0 \\ C_1 & 0 \\ C_2 & I_q \end{bmatrix} &= n + q, \forall \mu \in \mathbb{C}, \text{Re}(\mu) \geq 0 \end{aligned} \quad (7)$$

$$\iff \text{rank} \begin{bmatrix} \mu I_n - A \\ C_1 \end{bmatrix} = n, \forall \mu \in \mathbb{C}, \text{Re}(\mu) \geq 0 \quad (8)$$

The detectability of the singular system (5) is then reduced to the detectability of the pair (A, C_1) which is more tractable than condition (13) in [1]. Thus, the detectability of the pair (A, C) given by Assumption 1 in [1] is not necessary. Note first that the detectability of the pair (A, C) implies the detectability of the pair (A, C_1) and the converse is not true. For linear systems, i.e. $g(x, u, t) = 0$, the detectability of the pair (A, C_1) is a necessary and sufficient condition for observer design. In addition, as it will be shown in section 4, detectability condition (8) is more tractable for the computation of the matrix D .

2.2.2 On the relations between the choice of the generalized inverse and the observer's structure

This section is devoted to the choice of the generalized inverse of the matrix $\begin{bmatrix} E \\ H \end{bmatrix}$. It will be shown that the system description (5) makes it possible to light the parts of y_1 and y_2 in the observer design. The proposed observer given in [1] (eq. (20)) can be rewritten as follows

$$\dot{z} = Nz + L_1 y_1 + L_2 y_2 + Pg(\hat{x}, u, t) + PBu \quad (9a)$$

$$\hat{x} = z_1 + Q_{11} y_1 + Q_{12} y_2 \quad (9b)$$

$$\hat{f} = z_2 + Q_{21} y_1 + Q_{22} y_2 \quad (9c)$$

with $z_1 \in \mathbb{R}^n$, $z_2 \in \mathbb{R}^q$ and

$$z = \begin{bmatrix} z_1 \\ z_2 \end{bmatrix}, P = \begin{bmatrix} P_1 \\ P_2 \end{bmatrix}, Q = \begin{bmatrix} Q_{11} & Q_{12} \\ Q_{21} & Q_{22} \end{bmatrix}$$

where matrices P and Q are given by the generalized inverse of the full rank matrix $\begin{bmatrix} E \\ H \end{bmatrix}$

$$\begin{bmatrix} P & Q \end{bmatrix} = \begin{bmatrix} E \\ H \end{bmatrix}^\dagger \quad \text{such that} \quad \begin{bmatrix} E \\ H \end{bmatrix}^\dagger \begin{bmatrix} E \\ H \end{bmatrix} = I_{n+q} \quad (10)$$

All generalized inverses of full rank matrices can be parametrized by matrices α with $\det \alpha \neq 0$ and β such that [5]

$$\alpha \begin{bmatrix} E \\ H \end{bmatrix} = \begin{bmatrix} E_1 \\ E_2 \end{bmatrix} \quad \text{with} \quad \det E_1 \neq 0 \quad \text{and} \quad \begin{bmatrix} E \\ H \end{bmatrix}^\dagger = [(E_1^{-1} - \beta E_2 E_1^{-1}) \quad \beta] \alpha \quad (11)$$

Applying relation (11) with

$$\alpha = \begin{bmatrix} I_n & 0 & 0 \\ 0 & 0 & I_q \\ 0 & I_{m_1} & 0 \end{bmatrix}, \begin{bmatrix} E_1 \\ E_2 \end{bmatrix} = \begin{bmatrix} I_n & 0 \\ C_2 & I_q \\ C_1 & 0 \end{bmatrix}, E_1^{-1} = \begin{bmatrix} I_n & 0 \\ -C_2 & I_q \end{bmatrix} \quad \text{and} \quad \beta = \begin{bmatrix} \beta_1 \\ \beta_2 \end{bmatrix} \quad (12)$$

yields

$$\begin{bmatrix} E \\ H \end{bmatrix}^\dagger = \begin{bmatrix} I_n - \beta_1 C_1 & \beta_1 & 0 \\ -C_2 - \beta_2 C_1 & \beta_2 & I_q \end{bmatrix} = \begin{bmatrix} P_1 & Q_{11} & Q_{12} \\ P_2 & Q_{21} & Q_{22} \end{bmatrix} \quad (13)$$

Then, for all generalized inverses of $\begin{bmatrix} E \\ H \end{bmatrix}$, we have $Q_{12} = 0$ and $Q_{22} = I_q$. In addition, matrices Q_{11} and Q_{21} are arbitrary since $Q_{11} = \beta_1$ and $Q_{21} = \beta_2$.

Using relations (24) and (25) in [1] and the generalized inverse (13), one obtains

$$\begin{aligned} [L_1 \quad L_2] &= F + NQ = F + (PM - FH)Q = F(I - HQ) + PMQ \\ &= \begin{bmatrix} F_{11} & F_{12} \\ F_{21} & F_{22} \end{bmatrix} \begin{bmatrix} I_n - C_1 \beta_1 & 0 \\ -C_2 \beta_1 - \beta_2 & 0 \end{bmatrix} + \begin{bmatrix} (I_n - \beta_1 C_1)A\beta_1 & 0 \\ -(C_2 + \beta_2 C_1)A\beta_1 & 0 \end{bmatrix} = [L_1 \quad 0] \end{aligned} \quad (14)$$

or equivalently $L_2 = 0$ for all generalized inverses of matrix $\begin{bmatrix} E \\ H \end{bmatrix}$, and the observer (9) becomes

$$\dot{z} = Nz + L_1 y_1 + Pg(\hat{x}, u, t) + PBu \quad (15a)$$

$$\hat{x} = z_1 + \beta_1 y_1 \quad (15b)$$

$$\hat{f} = z_2 + \beta_2 y_1 + y_2 \quad (15c)$$

Notice that, for all generalized inverses of $\begin{bmatrix} E \\ H \end{bmatrix}$, only measurement y_1 is needed in the state observer (15a) and for the estimation \hat{x} in (15b) while the measurement y_2 is used to deduce the fault estimation.

If the Moore-Penrose generalized inverse is used as in [1] (see eq. (19) in [1]), one obtains

$$\begin{aligned} [P \ Q] &= \begin{bmatrix} E \\ H \end{bmatrix}^\dagger = \left(\begin{bmatrix} E^T & H^T \end{bmatrix} \begin{bmatrix} E \\ H \end{bmatrix} \right)^{-1} \begin{bmatrix} E^T & H^T \end{bmatrix} \\ &= \begin{bmatrix} (I_n + C_1^T C_1)^{-1} & (I_n + C_1^T C_1)^{-1} C_1^T & 0 \\ -C_2 (I_n + C_1^T C_1)^{-1} & -C_2 (I_n + C_1^T C_1)^{-1} C_1^T & I_q \end{bmatrix} = \begin{bmatrix} P_1 & Q_{11} & Q_{12} \\ P_2 & Q_{21} & Q_{22} \end{bmatrix} \end{aligned} \quad (16)$$

which corresponds to

$$\beta = \begin{bmatrix} \beta_1 \\ \beta_2 \end{bmatrix} = \begin{bmatrix} \beta_1 \\ -C_2 \beta_1 \end{bmatrix} = \begin{bmatrix} (I_n + C_1^T C_1)^{-1} C_1^T \\ -C_2 (I_n + C_1^T C_1)^{-1} C_1^T \end{bmatrix} = \begin{bmatrix} Q_{11} \\ Q_{21} \end{bmatrix} \quad (17)$$

A more simple generalized inverse can be chosen as follows

$$[\bar{P} \ \bar{Q}] = \begin{bmatrix} E \\ H \end{bmatrix}^\dagger = \begin{bmatrix} \bar{P}_1 & \bar{Q}_{11} & \bar{Q}_{12} \\ \bar{P}_2 & \bar{Q}_{21} & \bar{Q}_{22} \end{bmatrix} = \begin{bmatrix} I_n & 0 & 0 \\ -C_2 & 0 & I_q \end{bmatrix} \quad (18)$$

which corresponds to the case $\beta = 0$ and the observer (9) or (15) can be simplified as

$$\dot{z} = Nz + L_1 y_1 + L_2 y_2 + \bar{P}g(\hat{x}, u, t) + \bar{P}Bu \quad (19a)$$

$$\hat{x} = z_1 \quad (19b)$$

$$\hat{f} = z_2 + y_2 \quad (19c)$$

In comparison with the observer (15), the measurement y_1 does not act in an explicit way on the outputs \hat{x} and \hat{f} of the observer.

Using again relations (24) and (25) in [1] and the generalized inverse (18), the observer (19) is given by

$$N = \bar{P}M - FH = \begin{bmatrix} I_n \\ -C_2 \end{bmatrix} \begin{bmatrix} A & 0 \end{bmatrix} - \begin{bmatrix} F_{11} & F_{12} \\ F_{21} & F_{22} \end{bmatrix} \begin{bmatrix} C_1 & 0 \\ C_2 & I_q \end{bmatrix} = \begin{bmatrix} A - F_{11}C_1 - F_{12}C_2 & -F_{12} \\ -C_2A - F_{21}C_1 - F_{22}C_2 & -F_{22} \end{bmatrix} \quad (20)$$

and

$$[L_1 \ L_2] = F + N\bar{Q} = \begin{bmatrix} F_{11} & F_{12} \\ F_{21} & F_{22} \end{bmatrix} + \begin{bmatrix} A - F_{11}C_1 - F_{12}C_2 & -F_{12} \\ -C_2A - F_{21}C_1 - F_{22}C_2 & -F_{22} \end{bmatrix} \begin{bmatrix} 0 & 0 \\ 0 & I_q \end{bmatrix} = \begin{bmatrix} F_{11} & 0 \\ F_{21} & 0 \end{bmatrix} \quad (21)$$

Remark 1. For all generalized inverses of matrix $\begin{bmatrix} E \\ H \end{bmatrix}$ we have $Q_{12} = 0$ and $L_2 = 0$ then y_2 is not used in the dynamics of the observer nor in the state estimation \hat{x} . y_2 acts only on the fault estimation \hat{f} (observers output) what suggests using only relations (4a) and (4b) to estimate x . In addition, for the choice of the generalized inverse given by (18), the measurement y_1 affects the estimations of x and f after being filtered in (19a), i.e. the measurement noises in y_1 are filtered in (19). This is not the case if the Moore-Penrose generalized inverse is chosen as in [1].

Remark 2 (The Moore-Penrose generalized inverse with block-diagonal measurement output matrix). Without loss of generality, assume that $\text{rank } C = m$ or $\text{rank } C_1 = m_1$ and $\text{rank } C_2 = q$ with $m = m_1 + q$. Then there exists a non singular matrix $G \in \mathbb{R}^{n \times n}$ such that

$$\begin{bmatrix} \bar{C}_1 & 0 \\ 0 & \bar{C}_2 \end{bmatrix} = \begin{bmatrix} C_1 \\ C_2 \end{bmatrix} G, \tilde{x} = \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{bmatrix} = G^{-1}x, \tilde{A} = G^{-1}AG, \tilde{g}(\tilde{x}, u, t) = G^{-1}g(x, u, t), \tilde{B} = G^{-1}B \quad (22)$$

then the system (4) is equivalent to

$$\dot{\tilde{x}} = \tilde{A}\tilde{x} + \tilde{g}(\tilde{x}, u, t) + \tilde{B}u \quad (23a)$$

$$y_1 = \tilde{C}_1\tilde{x}_1 \quad (23b)$$

$$y_2 = \tilde{C}_2\tilde{x}_2 + f \quad (23c)$$

with $\tilde{x}_1 \in \mathbb{R}^{n_1}$, $\tilde{x}_2 \in \mathbb{R}^{n_2}$ et $n = n_1 + n_2$. The Moore-Penrose generalized inverse (16) gives

$$\begin{aligned} \begin{bmatrix} \tilde{P} & \tilde{Q} \end{bmatrix} &= \begin{bmatrix} E \\ H \end{bmatrix}^\dagger = \left(\begin{bmatrix} E^T & H^T \end{bmatrix} \begin{bmatrix} E \\ H \end{bmatrix} \right)^{-1} \begin{bmatrix} E^T & H^T \end{bmatrix} \\ &= \left[\begin{array}{cc|cc} (I_{n_1} + \tilde{C}_1^T \tilde{C}_1)^{-1} & 0 & (I_{n_1} + \tilde{C}_1^T \tilde{C}_1)^{-1} \tilde{C}_1^T & 0 \\ 0 & I_{n_2} & 0 & 0 \\ \hline 0 & -\tilde{C}_2 & 0 & I_q \end{array} \right] = \begin{bmatrix} \tilde{P}_1 & \tilde{Q}_{11} & \tilde{Q}_{12} \\ \tilde{P}_2 & \tilde{Q}_{21} & \tilde{Q}_{22} \end{bmatrix} \end{aligned} \quad (24)$$

and the observer (15) becomes

$$\dot{\tilde{z}} = \tilde{N}\tilde{z} + \tilde{L}_1 y_1 + \tilde{P}\tilde{g}(\tilde{x}, u, t) + \tilde{P}\tilde{B}u \quad (25a)$$

$$\hat{\tilde{x}} = \tilde{z}_1 + \tilde{Q}_{11} y_1 \quad (25b)$$

$$\hat{f} = \tilde{z}_2 + y_2 \quad (25c)$$

Using (13), the observation error $\bar{e} = \hat{\tilde{x}} - \tilde{x}$ can be rewritten as

$$\bar{e} = z + (QH - I_{n+q})\tilde{x} = \begin{bmatrix} z_1 \\ z_2 \end{bmatrix} + \left(\begin{bmatrix} Q_{11} & 0 \\ Q_{21} & I_q \end{bmatrix} \begin{bmatrix} C_1 & 0 \\ C_2 & I_q \end{bmatrix} - \begin{bmatrix} I_n & 0 \\ 0 & I_q \end{bmatrix} \right) \begin{bmatrix} x \\ f \end{bmatrix} = \begin{bmatrix} z_1 + (Q_{11}C_1 - I_n)x \\ z_2 + (Q_{21}C_1 + C_2)x \end{bmatrix} \quad (26)$$

For the Moore-Penrose generalized inverse (16) used in [1], we obtain

$$\bar{e} = \begin{bmatrix} z_1 - ((I_n + C_1^T C_1)^{-1})x \\ z_2 + (C_2(I_n + C_1^T C_1)^{-1})x \end{bmatrix} \quad (27)$$

Then in the observer (15) with generalized inverse (16), z_1 is an estimation of $(I_n + C_1^T C_1)^{-1}x$ and z_2 is an estimation of $-C_2(I_n + C_1^T C_1)^{-1}x = -C_2 z_1$. For the observer (19), the observation error becomes

$$\bar{e} = \begin{bmatrix} z_1 - x \\ z_2 + C_2 x \end{bmatrix} \quad (28)$$

and z_1 is then an estimation of x while z_2 is an estimation of $-C_2 x = -C_2 z_1$. In both cases, z_2 is not useful since it is a linear combination of z_1 . Thus, it seems interesting to estimate either x (n^{th} -order observer) or $C_2 x$ (q^{th} -order observer) without using a singular system framework. That will be the topics of sections 3.1 and 3.2.

2.2.3 On the LMI (eq. (27) in [1]) and sufficient conditions

The parameter $\mu > 0$ in the LMI (eq. (27) in [1]) is not useful since left and right-multiplying this LMI by $\frac{1}{\lambda\sqrt{\mu}}I_{2n+q}$ yields

$$\begin{bmatrix} \bar{X}PM + M^T P^T \bar{X} - RH - H^T R^T + I_{n+q} & \bar{X}P \\ P^T \bar{X} & \frac{-1}{\lambda^2} I_n \end{bmatrix} < 0 \quad (29)$$

Then the observer proposed by Wang et Zhou [1] exists if [6]

1. the function $g(x, t, u)$ verifies the Lipschitz condition (2),
2. there exist matrices R and $\bar{X} = \bar{X}^T > 0$ such that the LMI (29) is satisfied with $F = R^{-1}\bar{X}$ and $N = PM - FH$.

The above conditions are equivalent to the existence of a gain matrix F such that $(PM - FH)$ is stable and $\|(sI_{n+q} - (PM - FH))^{-1}P\|_\infty < \frac{1}{\lambda}$ where

$$\dot{\bar{e}} = (PM - FH)\bar{e} + Pg(\hat{\tilde{x}}, u, t) - g(x, u, t) \quad (30)$$

3 State and sensor fault estimation without the singular systems framework

It was shown in the previous development that the measurement y_2 is not used in the dynamics of the observer nor in the state estimation \hat{x} and a necessary condition is the detectability of the pair (A, C_1) . The main idea is then the synthesis of an n^{th} order observer which dynamics has only y_1 as input and y_2 is used in the observers output \hat{f} .

3.1 n^{th} order observers synthesis

By the use of the preceding arguments and as suggested by the structure of the observer (15) it is rather normal to propose an n^{th} order Kalman like observer of the following form

$$\dot{\hat{x}} = A\hat{x} + g(\hat{x}, u, t) + Bu + L(y_1 - C_1\hat{x}) \quad (31a)$$

$$\hat{f} = y_2 - C_2\hat{x} \quad (31b)$$

It was proved by Rajamani [6] that the dynamical system (31a) is an observer for the system (4a)-(4b) if there exists a gain matrix L verifying $(A - LC_1)$ stable (i.e. the pair (A, C_1) must be detectable) and $\|(sI_n - (A - LC_1))^{-1}\|_{\infty} < \frac{1}{\lambda}$ or equivalently if there exist matrices $X = X^T > 0$ and Z such that the following LMI is satisfied

$$\begin{bmatrix} XA + A^T X - ZC_1 - C_1^T Z^T + I_n & X \\ X & \frac{-1}{\lambda^2} I_n \end{bmatrix} < 0 \quad (32)$$

with $L = X^{-1}Z$. Then we have

$$\dot{e} = (A - LC_1)e + g(\hat{x}, u, t) - g(x, u, t) \quad (33)$$

The observation error $e = \hat{x} - x$ is then asymptotically stable. Now, let $e_f = \hat{f} - f$ be the fault estimation error then

$$e_f = (C_2x + f - C_2\hat{x}) - f = -C_2e \quad (34)$$

thus one can see that e_f decays to zero if e is asymptotically stable. Notice that, under the existence conditions given above there exists a reduced-order observer for the Lipschitz nonlinear system (4) (see [7]).

3.2 q^{th} order functional observer

An another approach consists on using a q^{th} order functional observer which estimates C_2x since the estimation of the state x is not necessarily useful to identify the faults f . Using (4c), let ν be the functional to be estimated

$$\nu = C_2x \quad (35)$$

with $\nu \in \mathbb{R}^q$. Without loss of generality, we assume that

$$\text{rank } C = \text{rank} \begin{bmatrix} C_1 \\ C_2 \end{bmatrix} = \text{rank } C_1 + \text{rank } C_2 = m \quad (36)$$

A q^{th} order functional observer can be expressed as follows

$$\dot{w} = Nw + Ly_1 + Pg(\hat{\nu}, u, t) + PBu \quad (37a)$$

$$\hat{\nu} = w + Qy_1 \quad (37b)$$

$$\hat{f} = y_2 - \hat{\nu} \quad (37c)$$

with $w \in \mathbb{R}^q$.

Necessary conditions for the existence of the observer (37) are given by [8]

$$\text{rank} \begin{bmatrix} C_2 A \\ C_1 A \\ C_1 \\ C_2 \end{bmatrix} = \text{rank} \begin{bmatrix} C_1 A \\ C_1 \\ C_2 \end{bmatrix} \quad (38a)$$

$$\text{rank} \begin{bmatrix} \mu C_2 - C_2 A \\ C_1 A \\ C_1 \end{bmatrix} = \text{rank} \begin{bmatrix} C_1 A \\ C_1 \\ C_2 \end{bmatrix}, \forall \mu \in \mathbb{C}, \text{Re}(\mu) \geq 0 \quad (38b)$$

In the case of functional observers for nonlinear Lipschitz systems, the necessary condition (38b) replaces the detectability condition (8). The synthesis of functional observer (37) takes as a starting point the results in [8, 9, 10]. The matrices of the functional observer are given by

$$N = (C_2 A M^\dagger) \mathcal{M}_{\mathcal{N}} - \mathcal{K}_{\mathcal{M}} (\mathcal{I}_{\uparrow+\downarrow\infty} - \mathcal{M} \mathcal{M}^\dagger) \mathcal{M}_{\mathcal{N}} = \mathcal{N}_\infty - \mathcal{K}_{\mathcal{M}} \mathcal{N}_\infty \quad (39a)$$

$$Q = (C_2 A M^\dagger) \mathcal{M}_{\mathcal{Q}} - \mathcal{K}_{\mathcal{M}} (\mathcal{I}_{\uparrow+\downarrow\infty} - \mathcal{M} \mathcal{M}^\dagger) \mathcal{M}_{\mathcal{Q}} = \mathcal{Q}_\infty - \mathcal{K}_{\mathcal{M}} \mathcal{Q}_\infty \quad (39b)$$

$$L = (C_2 A M^\dagger) \mathcal{M}_{\mathcal{L}} - \mathcal{K}_{\mathcal{M}} (\mathcal{I}_{\uparrow+\downarrow\infty} - \mathcal{M} \mathcal{M}^\dagger) \mathcal{M}_{\mathcal{L}} + \mathcal{N}_{\mathcal{Q}} \quad (39c)$$

$$P = C_2 - Q C_1 \quad (39d)$$

with

$$M = \begin{bmatrix} C_2 \\ C_1 \\ C_1 A \end{bmatrix}, \mathcal{M}_{\mathcal{N}} = \begin{bmatrix} I_q \\ 0_{m_1 \times q} \\ 0_{m_1 \times q} \end{bmatrix}, \mathcal{M}_{\mathcal{L}} = \begin{bmatrix} 0_{q \times m_1} \\ I_{m_1} \\ 0_{m_1 \times m_1} \end{bmatrix}, \mathcal{M}_{\mathcal{Q}} = \begin{bmatrix} 0_{q \times m_1} \\ 0_{m_1 \times m_1} \\ I_{m_1} \end{bmatrix}$$

where $K_M \in \mathbb{R}^{q \times (m+m_1)}$ is a gain matrix to be computed. Let $e = C_2 x - \hat{v}$ be the estimation error which dynamic's is driven by

$$\dot{e} = N e + P(g(\nu, u, t) - g(\hat{v}, u, t)) \quad (40)$$

The system (37) is a functional observer for the system (4) if conditions (2) and (38) are verified and if there exist matrices $X = X^T > 0$ and Z such that the following LMI is satisfied

$$\begin{bmatrix} X N_1 + N_1^T X - Z N_2 - N_2^T Z^T + I_q & X(C_2 - Q_1 C_1) + Z Q_2 C_1 \\ (C_2 - Q_1 C_1)^T X + C_1^T Q_2^T Z^T & \frac{-1}{\lambda^2} I_n \end{bmatrix} < 0 \quad (41)$$

with $K_M = X^{-1} Z$ and $N = N_1 - K_M N_2$. Note first that the detectability of the pair (N_1, N_2) is equivalent to condition (38b). In addition the LMI (41) is equivalent to the minimization of the \mathcal{H}_∞ norm of the transfert function between $r = g(\nu, u, t) - g(\hat{v}, u, t)$ and e and can be expressed as $\|(sI_q - N)^{-1} P\|_\infty < \frac{1}{\lambda}$ (see [6]).

4 Computation of the matrix D

Following the previous development, we propose an algorithm to compute the matrices D and C_1 . Since the matrices D and \bar{D} are composed of e_i (see notations in [1]), the problem consists in choosing the minimal number of rows c_i of C such that the rank condition (8) is satisfied. The index i of the selected row c_i corresponds to the column vector e_i composing the matrix \bar{D} . Let Ω be the set of unstable eigenvalues of A .

Step 1 for $i = 1 : m$,

$C_t = c_i$;
do TEST
end for i .

Step 2 for $i = 1 : m - 1$,
for $j = i + 1 : m$,
 $C_t = \begin{bmatrix} c_i \\ c_j \end{bmatrix}$;
do TEST
end for j ,
end for i ,

Step 3 for $i = 1 : m - 2$,
for $j = i + 1 : m - 1$,
for $k = j + 1 : m$,
 $C_t = \begin{bmatrix} c_i \\ c_j \\ c_k \end{bmatrix}$;
do TEST
end for k ,
end for j ,
end for i ,
 \vdots

Step m $C_t = C$, no sensor gain fault can be estimated.
STOP.

Step m+1 $C_1 = C_t$;
BREAK.

where

TEST : if $\text{rank} \begin{bmatrix} \mu I_n - A \\ C_t \end{bmatrix} = n, \quad \forall \mu \in \Omega$,
then goto step $m + 1$.

Let us note that if there are q conditionally identifiable sensors, then the maximum number \bar{q} of combinations of rows c_i to be tested is given by the following formula

$$\bar{q} = \sum_{r=1}^{m-q} C_r^m = \sum_{r=1}^{m-q} \frac{m!}{(m-r)!r!} \quad (42)$$

For the case treated in the example in [1], $m = 4$ and $q = 3$ then $\bar{q} = \frac{4!}{3!} = 4$.

5 Conclusion

Through this discussion paper, we provide simple ideas to improve, in a way, the interesting work presented in [1].

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