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► **To cite this version:**

Claude Stolz. General Relationships between Micro and Macro Scales for the Non-linear Behaviour of Heterogeneous Media. John Gittus; Joseph Zarka. Modelling Small Deformations of Polycrystals, Springer, pp.89-115, 1986, 10.1007/978-94-009-4181-6_4 . hal-00112500

HAL Id: hal-00112500

<https://hal.science/hal-00112500v1>

Submitted on 31 Oct 2018

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General Relationships between Micro and Macro Scales for the Non-linear Behaviour of Heterogeneous Media

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ABSTRACT

This chapter is mainly concerned with the determination of general relationships between microscopic and macroscopic mechanical properties for elastoplastic material with or without damage. The overall properties are determined in terms of the unknown properties of each constituent phase of the heterogeneous body. At first we must define a representative volume element (RVE) of the heterogeneous material for which the macroscopic mechanical fields are some spatial average of the microscopic one. The determination of local quantities is achieved by solving some particular boundary value problem on the RVE, from which macroscopic quantities are derived. The essential structure of micro-macro relationships is presented in the case of elastoplastic material. A generalisation is given to take the temperature field into account. We present also a model of damage and its averaging process. Finally we discuss the determination of macroscopic temperature through continuum thermodynamics.

INTRODUCTION

There are two main steps in the determination of the overall properties of a material in terms of the known properties of the constituent phases. First, the complex geometry of the n -phase body and the micro-

mechanical behaviour of each of the phases being given, one has to solve a complicated boundary value problem. The determination of the local mechanical fields (stress σ , strain ε , plastic strain ε^p) is achieved by a localization process that requires some particular boundary conditions, from which macroscopic fields (stress Σ , strain E, \dots) are derived. A comprehensive review of methods to solve some particular localization process is given by Willis (1981), Walpole (1969) and Hashin (1983).

The second step is concerned with the derivation of relationships between microscopic tensors and macroscopic tensors, which differ only by a length scale. Generally the macroscopic tensor is some spatial average of the microscopic one. Such a relationship is presented in continuum thermodynamics by Francfort *et al.* (1983) and Germain *et al.* (1983). This theoretical approach is summarized in the last section of this chapter.

This chapter is mainly concerned with the second basic problem, i.e. the determination of general relationships between microscopic and macroscopic fields for elastoplastic materials and for some model of damage. The essential structure of micro-macro relationships in elastoplastic materials is given in the previous works of Hill (1952, 1965) and Mandel (1964, 1971). After a general review and a second part concerned with the determination of the macroscopic elastic modulus of a heterogeneous material, we generalize the above-mentioned works and also our own previous results in plasticity to take the temperature field into account in Section 4.

In Section 5 we shall discuss the micromechanics of damage and its global average. Damage phenomena are due to microcracking in the body, for instance debonding between dissimilar materials, or at grain boundaries in polycrystals, and to the growth of holes or microcavities. Even if we assume small strain, the evolution of damage implies change of geometry, which is a non-linear and irreversible process.

In the last section we present a discussion about the determination of macroscopic temperature.

2. PRELIMINARY CONCEPTS

We consider a volume V , in which we distinguish two different scales, the micro one where the material properties vary from point to point like a highly heterogeneous medium, and the macro one where the properties are those of a homogeneous continuum.

To describe a heterogeneous medium it is essential to define a volume element which is small enough to allow us to distinguish the microscopic heterogeneities and sufficiently large to represent with accuracy the overall behaviour. This volume element is called a representative volume element (RVE); for example, the RVE of a periodic composite is simply the elementary cell (Suquet, 1982). For a randomly distributed composite of a polycrystalline aggregate it is necessary to have a minimum of information about the geometry of the constituent phases and to make assumptions like statistical homogeneity or ergodicity in order to define the RVE in a statistical sense (Beran, 1978; Fokin, 1979; Kröner, 1980; Willis, 1981; Hashin, 1983).

The problem is to characterize the overall behaviour only from a knowledge of the local constitutive equation of each constituent phase of the heterogeneous medium. On the microscopic level the mechanical properties vary from point to point with the local scale y while the average quantities vary smoothly with the macroscopic scale x .

With every microscopic quantity f (stress σ , mass per unit volume ρ , deformation ε , heat flux q , ...) we can associate its macroscopic value \bar{f} by an averaging process on the RVE, extended eventually in the cases for which RVE contains holes or rigid inclusions:

$$\bar{f} = \langle f \rangle = \frac{1}{V} \int_V f(y) dv_y \quad (2.1)$$

It is clear that eqn (2.1) defines a unique macro state quantity for each micro state.

Conversely, starting with a macro state, the definition of a suitable corresponding micro state requires complementary information or a localization process to determine the nearest possible micro state of the real one. For the choice of a representative volume element suitable boundary conditions must be prescribed and must satisfy some requirements (Francfort *et al.*, 1983; Germain *et al.*, 1983).

In particular, for study of the macroscopic behaviour these boundary conditions can be homogeneous; in this case one prescribes homogeneous stress conditions ($T_d = \Sigma \cdot \vec{n}$ on ∂V) or homogeneous strain conditions ($U = E \cdot y$ for $y \in \partial V$) (where Σ and E are two symmetric tensors).

For these boundary conditions, a local stress distribution σ and a local deformation ε are developed over the volume V .

In the case of homogeneous loading the stress σ verifies the equation of equilibrium and the boundary conditions

$$\left. \begin{aligned} \operatorname{div} \sigma &= 0 \quad \text{over } V \\ \sigma \cdot \vec{n} &= T^d \quad \text{on } \partial V \end{aligned} \right\} \quad (2.2)$$

In the other case the local deformation ε derives from a local displacement u which verifies

$$\left. \begin{aligned} \varepsilon_{ij} &= \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \quad \text{over } V \\ u &= U \quad \text{on } \partial V \end{aligned} \right\} \quad (2.3)$$

We require that the Hill-Mandel macrohomogeneity condition is fulfilled by all field σ^* with $\sigma^* = \langle \sigma^* \rangle$ and by all ε^* kinematically admissible so

$$\bar{\sigma}^* \bar{\varepsilon}^* = \langle \sigma^* \varepsilon^* \rangle \quad (2.4)$$

With these conditions it is obvious that, in the case of homogeneous loading,

$$\Sigma = \bar{\sigma} \quad (2.5)$$

and the microdisplacement u fluctuates around the homogeneous displacement U such that

$$\int_{\partial V} (U - u) \otimes n \, da = 0 \quad (2.6)$$

and

$$E = \langle \varepsilon \rangle$$

Dually, if $u = U$ over ∂V it is clear that

$$E = \frac{1}{V} \int_{\partial V} \frac{1}{2} (u \otimes n + n \otimes u) \, da = \langle \varepsilon \rangle = \bar{\varepsilon} \quad (2.7)$$

and the microstress is such that

$$\int_{\partial V} (\bar{\sigma} n - \sigma n) \otimes y \, da = 0 \quad (2.8)$$

and the macrostress $\Sigma = \bar{\sigma} = \langle \sigma \rangle$.

Some other boundary conditions can be used; in particular, for periodic structures (Sanchez-Palencia, 1974; Suquet, 1982), the elementary cell V generates the geometry of the whole by periodicity, all

the local fields are periodic functions and the Hill-Mandel macro-homogeneity condition is a necessary condition resulting from periodicity.

The construction of the macroconstitutive law from the microscopic behaviour can proceed as follows: starting from some macroscopic quantities, using a localization process to determine local fields, then the averaging process determines the missing macro quantities.

3. OVERALL PROPERTIES OF AN ELASTIC COMPOSITE MATERIAL

The main difficult problem is to determine effectively the overall property of a composite material. We shall restrict our discussion to some methods for the determination of the overall moduli for an elastic material.

The heterogeneous body is characterized by n phases with different elastic properties. The polycrystal aggregate is a particular case of a heterogeneous body, where the phases differ in the orientation of each crystal. Self-consistent theories which apply to polycrystal aggregates need knowledge of the properties of each grain (Hill, 1965; Berveiller and Zaoui, 1979). Kröner (1977, 1980), by a statistical approach, has compared the homogenization method of periodic media with the self-consistent scheme. The periodic model is a representative model of perfect order; one needs to solve a boundary value problem in a single cell, and the self-consistent method is more appropriate to model perfect disorder,

3.1. Bounds of the Elastic Modulus for a Heterogeneous Body

The medium is assumed to be elastic; each phase r has an elastic constitutive law with modulus Λ_r ($\varepsilon = \Lambda_r \sigma$, $\pi_r = \Lambda_r^{-1}$). We suppose that the characteristic function ϕ_r of each phase is known:

$$\left. \begin{aligned} \phi_r(y) &= 0 & y \text{ does not belong to phase } r \\ \phi_r(y) &= 1 & y \text{ belongs to phase } r \end{aligned} \right\} \quad (3.1)$$

We have the equality

$$\frac{1}{V} \sum_{r=1}^n \int_V \phi_r(y) \, dv_y = 1 \quad (3.2)$$

and the concentration of the r phase is

$$c_r = \frac{1}{V} \int_V \phi_r(y) dv_y \quad (3.3)$$

Several works (Beran and Molyneux, 1966; Hashin and Shtrikman, 1962; Hill, 1963) are related to the bounds of the moduli using minimum principles. For all displacements u^* kinematically admissible with given boundary conditions on ∂V the real field minimizes the energy:

$$U(u^*) = \frac{1}{V} \int_V \frac{1}{2} \varepsilon^* \pi \varepsilon^* dv_y \quad (3.4)$$

then for a localization process, which describes a homogeneous deformation on ∂V ($u^* = \bar{\varepsilon} \cdot y, y \in \partial V$), the following inequality holds:

$$\bar{U} < \frac{1}{2V} \bar{\varepsilon} \cdot \sum_r \int_V \pi_r \phi_r(y) dv_y \cdot \bar{\varepsilon} \quad (3.5)$$

From the macrohomogeneity hypothesis we have

$$\bar{U} = \frac{1}{2} \bar{\varepsilon} \bar{\pi} \bar{\varepsilon} = \frac{1}{2} \bar{\sigma} \bar{\varepsilon} = \frac{1}{2} \bar{\sigma} \bar{\varepsilon} \quad (3.6)$$

and, noting $\bar{\pi}$ the overall modulus ($\bar{\sigma} = \bar{\pi} \bar{\varepsilon}$), one can show that $\pi_v - \bar{\pi}$ is positive semi-definite, where the estimate π_v for the overall modulus is the Voigt average (Voigt, 1889):

$$\pi_v = \sum_{r=1}^n c_r \pi_r \quad (3.7)$$

Dually, we use the minimum of complementary energy for a localization process which prescribes homogeneous tensions on ∂V :

$$\bar{U} < \frac{1}{2V} \bar{\sigma} \sum_{r=1}^n \int_V \Lambda_r \phi_r(y) dv \bar{\sigma} \quad (3.8)$$

Then, with the macrohomogeneity hypothesis, noting $\bar{\Lambda}$ the overall modulus ($\bar{\sigma} = \bar{\Lambda} \bar{\sigma}$), the inequality shows that $\Lambda_v - \bar{\Lambda}$ is positive semi-definite and Λ_v^{-1} is an estimate of $\bar{\pi}$ in the Reuss sense:

$$\pi_R = \Lambda_v^{-1} = \left(\sum_{r=1}^n c_r \Lambda_r \right)^{-1} \quad (3.9)$$

The two estimates π_v and π_R are lower and upper bounds. The best estimates are such that the localization process approaches the real solution. In the case of periodic media the answer is clear; for such a material Ω , with many elementary cells, if homogeneous tension or homogeneous deformation are applied on $\partial\Omega$, far from the boundary, the field solution of the boundary value problem is a periodic field; the averages of stress or strain on V are equal to the prescribed value. The real localization process is the periodic localization process, so the overall moduli obtained with homogeneous prescribed macrostress or macrostrain are equal.

For other composites, it is necessary to have complementary information. The calculus of overall properties is related to the determination of fields which satisfy equilibrium equations; perfect bonding across phase interfaces and some simplifications must be made to derive explicit results.

In the self-consistent scheme, for example, we consider that the inclusions are spherical or ellipsoidal, and when the medium is statistically uniform the equivalent body is assumed to be isotropic. To estimate the overall moduli, we can consider that each inclusion is embedded in a homogeneous matrix with the overall moduli Λ as elastic properties, and subject to a homogeneous field at infinity. The interaction problem between a matrix and a spherical or ellipsoidal inclusion is well known (Eshelby, 1957, 1961). The microstress in the inclusion is homogeneous and an explicit result can be given in the formal equation

$$\sigma(r) = \Sigma + J_r : (E - \varepsilon(r)) \quad (3.10)$$

The interaction is described by J_r , which depends on the overall moduli Λ , on the inclusion geometry and on orientation (Berveiller and Zaoui, 1979).

If we take the statistical average and the local behaviour into account,

$$\left. \begin{aligned} \sigma_r &= \Lambda_r \varepsilon_r \\ \Sigma &= \langle \sigma_r \rangle \quad \text{and } E = \langle \varepsilon_r \rangle \\ \Sigma &= \Lambda E \end{aligned} \right\} \quad (3.11)$$

we have the equation

$$\Lambda = \langle \Lambda_r (\Lambda_r + J_r)^{-1} (\Lambda + J_r) \rangle \quad (3.12)$$

with unknown Λ . Usually this equation is complex to solve; the

determination of J , is not the easiest thing to do. Each phase seems to see the other phases through the homogeneous material; we have not given a good description of the interactions between all the inclusions. Some developments due to Berveiller and Zaoui (1979), Fokin (1979) and Andrieux (1983) can be used to solve this problem with greater accuracy.

The first estimates (Voigt and Reuss estimates) are established using the minimum energy principle, and the bounds are obtained for extremal values associated with homogeneous boundary conditions. A successful method is to determine a suitable displacement field to have a better estimate. For this reason it is convenient to introduce a homogeneous comparison material with modulus Λ_0 and to set the local modulus Λ equal to Λ_0 with some perturbation $\delta\Lambda$:

$$\Lambda = \Lambda_0 + \delta\Lambda \quad (3.13)$$

If ε is the real deformation over V , the stress polarization

$$p = \sigma - \Lambda_0\varepsilon = \delta\Lambda.\varepsilon \quad (3.14)$$

verifies

$$\operatorname{div}(p + \Lambda_0\varepsilon) = 0 \quad \text{over } V \quad (3.15)$$

and if we know the Green's function for the comparison material we have

$$u(x) = u_0(x) + \int_V G(x,y) \operatorname{div} p(y) \, dv_y \quad (3.16)$$

The deformation ε is the sum of the homogeneous deformation $E = \varepsilon_0$ and the last term of eqn (3.16), due to heterogeneity. In this integral formulation we can substitute the variational expression. Such methods are presented by Willis (1981) and Hashin and Shtrikman (1962*ab*, 1963). These authors have obtained bounds for overall moduli by different approximations of p and different averaging processes.

3.2. The Case of a Macrohomogeneous Body

In the last section we saw that the estimate of the elastic modulus is not the same when one prescribes macrohomogeneous strain or stress over V . But when the body can be considered as macrohomogeneous in the sense of Hill (1952, 1965) and Mandel (1964) the difference between the two estimates is negligible.

So when one prescribes homogeneous boundary conditions in stress ($T^d = \Sigma \cdot \vec{n}$ on ∂V , with Σ a symmetric tensor) the local stress is obtained as the solution of an elastic linear problem:

Equation of equilibrium:

$$\operatorname{div} \sigma = 0 \quad \text{over } V$$

$$\sigma \cdot \vec{n} = T^d \quad \text{on } \partial V$$

Elastic constitutive law:

$$\varepsilon = \Lambda^0(y) : \sigma \quad (\forall y \in V)$$

Existence of a local displacement u such that

$$\varepsilon_{ij} = \frac{1}{2} \left(\frac{\partial u^j}{\partial x^i} + \frac{\partial u^i}{\partial x^j} \right)$$

(3.17)

and we can prove the existence of a localization tensor A_{ijpq} such that

$$\sigma_{ij} = A_{ijpq} \Sigma_{pq} \quad (3.18)$$

The tensor A is the elastic localization tensor introduced by Mandel (1964) in the case of a localization process in homogeneous macrostresses.

As $\langle \sigma \rangle = \Sigma$ for all prescribed Σ , we have

$$\langle A_{ijpq} \rangle = \frac{1}{2} (\delta_{ip} \delta_{jq} + \delta_{iq} \delta_{jp}) \quad (3.19)$$

At fixed subscripts (p, q) A_{ijpq} satisfies the equations of equilibrium

$$A_{ijpq,j} = 0 \quad (3.20)$$

with the boundary conditions

$$A_{ijpq} n_j = \frac{1}{2} (\delta_{ip} \delta_{jq} + \delta_{iq} \delta_{jp}) \cdot n_j \quad (3.21)$$

and the deformation

$$\varepsilon_{ij} = \Lambda_{ijkl}^0 A_{klpq} \quad (3.22)$$

satisfies the condition of compatibility.

With the help of a macrohomogeneity condition, for all prescribed Σ we have

$$\Sigma E = \langle \sigma \varepsilon \rangle \quad (3.23)$$

The macroscopic modulus $\Lambda (E = \Lambda \Sigma)$ is determined as a function of the local one ($\varepsilon = \Lambda^0 \sigma$) by replacing σ in eqn (3.23) by $A \Sigma$:

$$\Lambda_{pqrs} = \langle A_{ijpq} \Lambda_{ijkl}^0 A_{klrs} \rangle = \overline{A \Lambda^0 A} \quad (3.24)$$

In the following we consider only the case of a macrohomogeneous body.

4. STUDY OF A THERMOELASTOPLASTIC MATERIAL

4.1. The Macroscopic Constitutive Law

In this example we consider a thermoelastoplastic material and we assume that there is no effect of viscosity. The absolute temperature T is given and the total deformation ε is the sum of an elastic part ε^e and an irreversible part ε^p :

$$\varepsilon = \varepsilon^e + \varepsilon^p \quad (4.1)$$

The irreversible part has a standard evolution; the rate $\dot{\varepsilon}^p$ is normal to a yield surface delimited by a convex function ϕ of the stress σ :

$$\dot{\varepsilon}^p = \frac{\partial \phi}{\partial \sigma} \quad (4.2)$$

The reversible part ε^e is related to σ and to the increase of the temperature from its initial value T_0 :

$$\varepsilon^e = \Lambda^0 \sigma + \alpha(T - T_0) \quad (4.3)$$

4.2. Global Domain of Elasticity

At the local level there exists an elastic domain \mathcal{C} defined by $\mathcal{C} = \{\sigma / \phi(\sigma) \leq 0\}$. At the macro level there exists an elastic domain \mathcal{E} defined as follows.

Let two macrostresses Σ and Σ^* belong to \mathcal{E} , at each point of V ; the corresponding microstresses σ and σ^* are elements of \mathcal{C} and the difference $\sigma - \sigma^*$ is deduced from $\Sigma - \Sigma^*$ by means of a localization process with purely elastic behaviour.

So it is obvious that

$$\sigma - \sigma^* = A(\Sigma - \Sigma^*) \quad (4.4)$$

where A is the localization tensor introduced in the last section.

4.3. On the Decomposition of the Macroscopic Deformation

Let Σ be the real macrostress and σ the corresponding micro one. At the initial temperature T_0 , the local response in purely elastic behaviour is

$$\sigma_E = A \Sigma \quad (4.5)$$

The stress field $r = \sigma - \sigma_E$ is a self-equilibrated stress and is the sum of two self-equilibrated stresses:

$$r = r_p + r_\theta \quad (4.6)$$

such that the two microdeformations

$$\left. \begin{aligned} \varepsilon_1 &= \Lambda^0 r_\theta + \alpha(T - T_0) \\ \varepsilon_2 &= \Lambda^0 r_p + \varepsilon^p \end{aligned} \right\} \quad (4.7)$$

are kinematically admissible.

By definition the macroscopic elastic deformation due to the difference in absolute temperature $T - T_0$ and to the given macrostress Σ is the deformation deduced from a purely elastic unloading with return of the temperature to its initial value (Mandel, 1971; Halphen, 1977).

The local deformation defined by

$$\varepsilon_E = \Lambda^0 \sigma_E + \varepsilon_1 \quad (4.8)$$

is related to the macro one E_E by the lemma of macrohomogeneity and

$$E_E = \langle \varepsilon_E \rangle \quad (4.9)$$

and for all stresses σ' statically admissible with $\Sigma' = \langle \sigma' \rangle$ we have

$$\Sigma' E_E = \langle \sigma' \varepsilon_E \rangle \quad (4.10)$$

For the particular choice of $\sigma' = A \Sigma'$, and taking into account that r_θ is self-equilibrated, we can split E_E into two terms:

$$E_E = \overline{{}^1 A \Lambda^0 A} \Sigma' + \overline{{}^1 A \alpha} (T - T_0) \quad (4.11)$$

We recognize the macroscopic modulus $\overline{\Lambda} = \overline{{}^1 A \Lambda^0 A}$ and the result obtained is in agreement with the definition of the macroscopic elastic deformation.

In the same way, the global deformation $E = \langle \varepsilon \rangle$ must satisfy eqn (4.10), and for the difference $E_p = E - E_E$ we have the definition of the irreversible macroscopic deformation:

$$E_p = \overline{{}^1 A \varepsilon_p} \quad (4.12)$$

The irreversible part of the macrodeformation is not the mean of the micro one because the field of plastic deformation is not kinematically admissible (Mandel, 1964, 1971; Hill, 1965).

The relations (4.11) and (4.12) describe the form of the stress-strain relation, and moreover these equations are true for quasi-static evolutions. If there exists a viscoplastic potential ϕ for the rate of the plastic deformation, such that

$$\dot{\varepsilon}^p = \frac{\partial \phi}{\partial \sigma} \quad (4.13)$$

it is obvious that at the macro level the mean potential (Mandel, 1971; Rice, 1971)

$$\Phi(\Sigma, r) = \overline{\phi(\sigma)} \quad (4.14)$$

is the macroviscoplastic potential associated with \dot{E}^p : ($\sigma = A\Sigma + r$)

$$\left. \begin{aligned} \frac{\partial \Phi}{\partial \Sigma} &= \overline{\frac{\partial \phi}{\partial \sigma} \frac{\partial \sigma}{\partial \Sigma}} = \overline{{}^t A \frac{\partial \phi}{\partial \sigma}} \\ \frac{\partial \Phi}{\partial r} &= \overline{\dot{\varepsilon}^p} = \overline{\frac{\partial \phi}{\partial \sigma}} \end{aligned} \right\} \quad (4.15)$$

and we obtain

$$\dot{E}^p = \overline{{}^t A \dot{\varepsilon}^p} \quad (4.16)$$

4.4. Analysis of the Dissipation

At the micro level, the second law of thermodynamics gives the rate of dissipation:

$$d = \rho T \dot{s} + \text{div } q - q \cdot \xi \geq 0 \quad (4.17)$$

Using the conservation of energy,

$$\rho \dot{e} = \sigma \dot{\varepsilon} - \text{div } q \quad (4.18)$$

and knowing the relation between the thermodynamical potentials e and $w(\varepsilon^e, I)$, $e = w - Ts$, we can deduce

$$d = \sigma \dot{\varepsilon}^p - q \xi \geq 0 \quad (4.19)$$

We have assumed that q is defined by $q = -\partial\omega/\partial\xi$ where ω is a convex function of ξ , therefore the term $-q \cdot \xi$ is positive, and when we admit the decomposition of the dissipation rate in two parts, the term due to the irreversible mechanism is also positive, $\sigma \dot{\varepsilon}^p \geq 0$. By integration over V the total plastic dissipation rate $\mathcal{D}_p = \overline{\sigma \dot{\varepsilon}^p}$ can be given in terms of macroscopic variables:

$$\mathcal{D}_p = \Sigma \dot{E}^p - \frac{d}{dt} W_b \geq 0 \quad (4.20)$$

where $W_b = \frac{1}{2} r \overline{\Lambda_0} r$ is the energy of the self-equilibrated stresses. The last result is obtained by application of eqn (4.10); for the plastic deformation rate and the real stresses $\sigma = A\Sigma + r$.

The physical meaning of this result is that perfect plastic behaviour at the micro level presents hardening behaviour on the macro scale.

5. THE CASE OF A SOLID HAVING LOCALLY DAMAGED ZONES

5.1. Description of the Model of Damage

It is observed that the reduction of material rigidity is generally due to the evolution of defects such as cavities, cracks, etc. Under external loading, these zones cannot support tensile stresses. It is proposed to characterize the damaged material only by the property that the stress tensor vanishes in the damaged zone. Therefore the stress vector must vanish on the boundary ∂z_i of any damaged zone z_i ($\sigma \cdot \vec{n} \equiv 0$ on ∂z_i). If the volume V contains many damaged parts with total volume $z(t)$, a function of the time t , the volume of the sound material is $\Omega(t) = V - z(t)$; we note $\partial\Omega_i$, the common boundary between Ω and z . The mechanical properties of the sound material are defined by the thermodynamical potential.

The definition of the average must be changed because f is only defined in Ω :

$$\bar{f} = \langle f \rangle_{\Omega} = \frac{1}{V} \int_{\Omega} f \, dv \quad (5.1)$$

We suppose that the mass per unit volume is constant:

$$\forall x \in \Omega \quad \rho(x) = \rho_0 \quad (5.2)$$

Our study is concerned with the behaviour of material introduced by Bui and co-workers (Bui and Ehrlacher, 1980; Bui *et al.*, 1981) to study fracture, pictured in Fig. 1.

To determine the evolution of damaged zones, it is necessary to introduce a rupture criterion. Rupture occurs when a threshold value (in stress, deformation or energy) is reached; when the strain is increasing the stress vanishes.

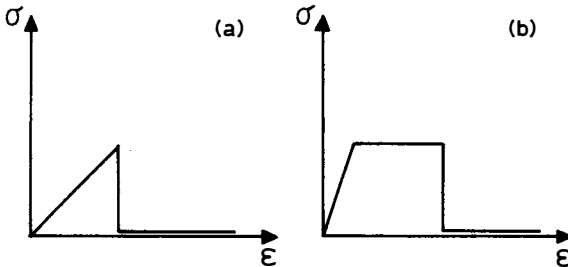


Fig. 1. (a) Elastic-brittle or (b) elastoplastic-brittle behaviour.

To define an accurate localization process, the boundary condition ($\sigma \cdot n = 0$ on $\partial\Omega_i$) must be taken into account. All the stresses σ must verify the equation of equilibrium and the new boundary conditions $\sigma n = 0$ at each point of $\partial\Omega_i(t)$. For the sake of simplicity, we assume that the heat flux is zero on $\partial\Omega_i$, and the damaged zones are considered to have no heat conductivity.

The localization process gives a new fourth rank tensor A of elastic concentration. This tensor has the properties (3.20)–(3.22) over Ω and verifies the boundary conditions $A_{ijpq} \cdot n_j = 0$ at each point of $\partial\Omega_i$.

One can define the general relations between the micro and macro deformations and stresses as follows:

$$\left. \begin{aligned} E &= \overline{{}^t A \varepsilon} = \bar{\varepsilon} - \frac{1}{2V} \int_{\partial\Omega_i} (u \otimes n)_s \, ds \\ \dot{E} &= \overline{{}^t A \dot{\varepsilon}} = \bar{\dot{\varepsilon}} - \frac{1}{2V} \int_{\partial\Omega_i} (v \otimes n)_s \, ds \\ \Sigma &= \bar{\sigma} \end{aligned} \right\} \quad (5.3)$$

The local compliance Λ^0 ($\varepsilon = \Lambda^0 \sigma$) is related to the macro compliance ($E = \Lambda \Sigma$) by the equation

$$\Lambda = \overline{{}^t A \Lambda_0 A} \quad (5.4)$$

because the field $\Lambda_0 A$ is kinematically admissible and A is statically admissible with $A \cdot \vec{n} = \vec{0}$ on $\partial\Omega_i$.

However, the tensor A depends on the actual volume $\Omega(t)$ of the sound material and its rate \dot{A} is related to the propagation of the damaged zones (Bui *et al.*, 1982).

5.2. Determination of the Evolution of the Damaged Zone for a Thermoelastic Material

Consider a thermoelastic material with free energy $w(\varepsilon, T)$ which depends only on the deformation ε and the absolute temperature T . At each point of V we define the energy density e and the entropy s per unit mass. For simplicity we assume that damaged zones have no heat conductivity and that they are inert ($e = 0, s = 0, v = 0$).

The first law of thermodynamics is the conservation of energy, at the macro level:

$$\dot{\bar{e}} + \dot{\bar{K}} = P_{\text{cal}} + P_{\text{ext}} \quad (5.5)$$

The variation of internal energy and kinetic energy $\overline{K} = \frac{1}{2}\overline{\rho u^2}$ is equal to the heat flux and the power of external loading. We consider only quasi-static evolution so that the contribution of kinetic energy is negligible. The heat flux determines P_{cal} :

$$P_{cal} = - \int_{\partial V} q \cdot \vec{n} da \quad (5.6)$$

and by means of the equilibrium equation we have, for the power of external loading,

$$P_{ext} = \overline{\sigma \dot{\epsilon}} - \int_{\partial\Omega_i} \sigma n v da \quad (5.7)$$

The localization process depends on the evolution of damaged zones and all the quantities are changed with the variation of Ω . If f is a regular mechanical quantity and defined on Ω , we have the equation

$$\dot{\overline{f}} = \overline{\dot{f}} - \frac{1}{V} \int_{\partial\Omega_i} f c da \quad (5.8)$$

where c is the normal velocity of the boundary $\partial\Omega_i$. So we have the local equation corresponding to (5.5):

$$\left. \begin{array}{l} \rho_0 \dot{\epsilon} = \sigma \dot{\epsilon} - \text{div } q \quad \text{over } \Omega \\ \vec{q} \vec{n} = -\rho_0 e c \quad \text{on } \partial\Omega_i \text{ with } \phi \geq 0 \end{array} \right\} \quad (5.9)$$

The production of entropy is necessarily positive:

$$\dot{\overline{s}} + \int_{\partial\Omega_i} \frac{q}{T} \cdot n da \geq 0 \quad (5.10)$$

By eqn (5.8) we can write the inequality (5.10) in another form:

$$\overline{\rho_0 \dot{s} + \frac{1}{V} \text{div } q} - \overline{q \cdot \frac{\nabla T}{T^2}} - \frac{1}{V} \int_{\partial\Omega_i} \left(\frac{q}{T} n + \rho_0 s c \right) da \geq 0 \quad (5.11)$$

For an elastic material we have

$$\rho_0 \dot{s} + \frac{1}{T} \text{div } q = 0 \quad (5.12)$$

With the conductivity law $q = -\partial\omega/\partial\xi$ where $\xi = \nabla T/T$ and ω convex, function of ξ , we have

$$-\frac{1}{T} \overline{q \cdot \nabla \xi} \geq 0 \quad (5.13)$$

Therefore the fracture dissipation rate is equal to the last term of (5.11):

$$\mathcal{D}_f = \frac{1}{V} \int_{\partial\Omega_i} (qn + \rho_0 sc) da \geq 0 \quad (5.14)$$

Using eqns (5.9),

$$\mathcal{D}_f = \frac{1}{V} \int_{\partial\Omega_i} \rho_0 \frac{W}{T} c da \geq 0 \quad (5.15)$$

Per unit of area the thermodynamical force associated with c has the dimensions of entropy. We assume a brittle criterion (Nguyen, 1978; Suquet, 1982; Stolz, 1984):

$$\left. \begin{aligned} \mathcal{S} &= \frac{W}{T} \leq \mathcal{S}_c & c &= 0 \\ \mathcal{S} &= \mathcal{S}_c & c &\geq 0 \end{aligned} \right\} \quad (5.16)$$

The two criteria $\mathcal{S} = \mathcal{S}_c$ and $\vec{\sigma} \vec{n} = 0$ must be satisfied along the moving part of the boundary $\partial\Omega_i$, and we must introduce the transport condition at a geometrical point of $\partial\Omega_i$ by the convected derivative \mathcal{D}_f :

$$x \in \partial\Omega_i \quad \mathcal{D}_f = \lim_{\Delta t \rightarrow 0} \frac{f(x + c \Delta t, t + \Delta t) - f(x, t)}{\Delta t} \quad (5.17)$$

On $\partial\Omega_i$ the two conditions are written as follows:

$$\left. \begin{aligned} \mathcal{D}(\vec{\sigma} \vec{n}) &= (\dot{\vec{\sigma}} + \vec{c} \vec{n} \cdot \nabla \sigma) \cdot \vec{n} + \sigma \mathcal{D} \vec{n} = 0 \\ T \mathcal{D}(\mathcal{S}) &= \dot{W} - W \frac{\dot{T}}{T} - T \vec{c} \vec{n} \cdot \nabla \mathcal{S} \end{aligned} \right\} \quad (5.18)$$

It is easy to show that, in the plane case (with normal \vec{k}),

$$\mathcal{D} \vec{n} = \frac{dc}{ds} \cdot \vec{\tau} \quad (5.19)$$

$\vec{\tau}$ is the tangent vector to $\partial\Omega_i$ with s the curvilinear coordinate.

Taking into account the equilibrium equation

$$\vec{\tau} \cdot \nabla \sigma \cdot \vec{\tau} + \vec{n} \cdot \nabla \sigma \cdot \vec{n} = 0 \quad (5.20)$$

and a particular form of $\sigma = \sigma \vec{\tau} \otimes \vec{\tau} + \sigma_z k \otimes k$, the equations (5.18) become

$$\left. \begin{aligned} \mathcal{D}(\sigma n) &= \dot{\sigma} n + \frac{d}{ds}(c \sigma \cdot \vec{\tau}) = 0 \\ T \cdot \mathcal{D}\mathcal{S} &= \sigma \frac{\dot{\varepsilon}}{\rho} - e \frac{\dot{T}}{T} - T c \cdot \nabla \mathcal{S} = 0 \end{aligned} \right\} \quad (5.21)$$

Knowing at each time t the thermomechanical fields and the geometry of $\Omega(t)$, we search for the rate quantities and the normal velocity c on $\partial\Omega_i$. The rate equations are

$$\left. \begin{aligned} \operatorname{div} \dot{\sigma} &= 0 & \rho T \dot{s} + \operatorname{div} q &= 0 \\ \dot{\varepsilon} &= \frac{1}{2}(\Delta v + \Delta^T v) & \xi &= \Delta \log T & x \in \Omega \\ \dot{\sigma} &= \Lambda_0 \dot{\varepsilon} + A \dot{T} & -\dot{s} &= A^T \dot{\varepsilon} + Z \dot{T} \\ q &= -\frac{\partial \omega}{\partial \xi} \\ (\Lambda_0 &= \rho W''_{,\varepsilon\varepsilon}; & A &= \rho W''_{,T\varepsilon}; & Z &= \rho W''_{,TT}) \end{aligned} \right\} \quad (5.22)$$

with the boundary conditions

$$\left. \begin{aligned} q \cdot n &= Q^d \text{ on } \partial V_q & \dot{T} &= \dot{T}^d \text{ on } \partial V_T \\ v &= v^d \text{ on } \partial V_u & \dot{\sigma} n &= \mathcal{F}^d \text{ on } \partial V_\sigma \end{aligned} \right\} \quad (5.23)$$

($\partial V = \partial V_q \cup \partial V_T = \partial V_u \cup \partial V_\sigma$, $\partial V_q \cap \partial V_T = \emptyset$, $\partial V_\sigma \cap \partial V_u = \emptyset$) and on $\partial\Omega_i$ we have

$$\left. \begin{aligned} c &= 0; & \dot{\sigma} n &= 0; & q \cdot n &= 0 \\ c &\neq 0; & \mathcal{D}(\sigma n) &= 0; & \mathcal{D}(\mathcal{S}) &= 0; & q \cdot n &= -\rho_0 e c \end{aligned} \right\} \quad (5.24)$$

The solution of this problem is a stationary point of the functional (Stolz, 1984):

$$\left. \begin{aligned} \mathcal{J}(v, c, \dot{T}) &= \int_{\Omega} \left[\frac{1}{2} \dot{\varepsilon} \Lambda_0 \dot{\varepsilon} + \dot{T} A \dot{\varepsilon} + \frac{1}{2} \dot{T} z \dot{T} + \frac{d}{dt} \omega \right] dv \\ &- \int_{\partial\Omega_i} \rho \left\langle \sigma \frac{\dot{\varepsilon}}{\rho} - \frac{\dot{T}}{T} e \right\rangle c \, da + \int_{\partial\Omega_i} \frac{c^2}{2} \rho T \vec{n} \cdot \nabla(\mathcal{S}) \, da \\ &+ \int_{\partial V_\sigma} \mathcal{F}^d v \, da - \int_{\partial\Omega} Q^d \frac{\dot{T}}{T} \, da \end{aligned} \right\} \quad (5.25)$$

On the set $V = \{v, \dot{T}/v = v^d \text{ on } \partial V_w, \dot{T} = T^d \text{ on } \partial V_T\}$.

Once the velocity c is determined, we are able to know the variation of all macro quantities by application of eqn (5.8). In the following part we suppose that c is determined, and our point of interest is the macroscopic behaviour of a RVE V , and we reduce our consideration on elastoplastic material, with free energy of the form $w(\varepsilon - \varepsilon^p)$. The influence of temperature could be treated as in the last example (Section 4).

5.3. Evolution of Macroscopic Quantities

Here we determine the evolution of the macroscopic modulus and we decompose the rate of deformation.

By comparison of the two expressions for E and \dot{E} in eqns (5.3), the application of eqn (5.8) shows that

$$\overline{{}^t\dot{A}\varepsilon} - \frac{1}{V} \int_{\partial\Omega_i} {}^tA\varepsilon c \, da = 0 \quad (5.26)$$

for all kinematically admissible ε . One particular field ε is $\Lambda_{ijpq}^0 A_{pqrs}$, so it is obvious to obtain (Bui *et al.*, 1982)

$$\dot{\Lambda} = \overline{{}^t\dot{A}\Lambda_0 A} = \frac{1}{V} \int_{\partial\Omega_i} {}^tA\Lambda_0 A c \, da \quad (5.27)$$

The elastic modulus varies with the propagation of the damaged zones; this variation must appear in the reversible part of the rate of the elastic macroscopic deformation.

When the damaged zone does not propagate in Ω the local stress field is $\sigma = A\Sigma' + r$ where r is a self-equilibrated stress on the actual geometry. For an increasing $\dot{\Sigma}$ of the macrostress from the value Σ such that the damaged zone has a normal velocity c of propagation, the local stresses are $\dot{\sigma}$ with a corresponding rate of deformation

$$\dot{\varepsilon} = \Lambda_0 \dot{\sigma} + \dot{\varepsilon}^p \quad (5.28)$$

in the case of an elastoplastic material. Let $\dot{\sigma}_E$ be the fictitious stresses obtained with purely elastic behaviour with the same velocity of propagation c :

$$\dot{\sigma}_E = A\dot{\Sigma} + \dot{A}\Sigma \quad (5.29)$$

where \dot{A} is related to the variation of the localization tensor A due to the change in the geometry of Ω induced by the damaged zone propagation.

If the stress field r is self-equilibrated on $\Omega(t)$ we have, from eqn (5.8),

$$\bar{r} = \frac{1}{V} \int_{\partial\Omega_i} r c \, da \quad (5.30)$$

which shows that \dot{r} is generally not self-equilibrated; we have inside Ω a redistribution of residual stresses. The rate $\dot{\varepsilon}$ and $\Lambda^0 \dot{\sigma}_E$ are two kinematically admissible fields of deformation, then the macroscopic deformations E and E_E are given by the relations (5.3). For all σ' statically admissible with $\Sigma' = \langle \sigma' \rangle$ in the localization process we have

$$\left. \begin{aligned} \overline{\sigma' \dot{\varepsilon}} &= \Sigma' \dot{E} \\ \overline{\sigma' \dot{\varepsilon}} &= \Sigma' \dot{E}_E \end{aligned} \right\} \quad (5.31)$$

For the particular choice of $\sigma' = A \Sigma'$ we have

$$\dot{E}_E = \overline{{}^1 A \Lambda_0 \dot{\sigma}_E} = \Lambda \dot{\Sigma} + \dot{\Lambda} \Sigma \quad (5.32)$$

which defines exactly the variations of the reversible part E_E of the macrodeformation ($E_E = \Lambda \Sigma$).

Moreover, by subtraction in eqns (5.31) (with the same choice $\sigma' = A \Sigma'$) one obtains

$$\dot{E}_{IR} = \overline{{}^1 A \dot{\varepsilon}^p} + \overline{{}^1 A \Lambda_0 \dot{r}} \quad (5.33)$$

The complementary term is due to the redistribution of residual stresses inside Ω , when the geometry changes with the propagation of the damaged zones.

When no damage occurs eqn (5.30) shows that \dot{r} is self-equilibrated and the classical relation (4.20) is recovered. However, the existence of a viscoplastic potential at the microlevel does not ensure the existence of a macro-viscoplastic potential E_{IR} . Only the first term can be deduced from the average potential $\Phi(\Sigma, \rho) = \overline{\phi(\sigma)}$.

5.4. Study of the Dissipation Rate

The global energy \overline{W} is the sum of a reversible part and an embedded energy W_b in the residual stresses r . For a quadratic form $w(\varepsilon - \varepsilon^p)$, the dissipation \mathcal{D} can be decomposed into three terms, the first due to heat conduction, the second due to plasticity $\overline{\sigma \dot{\varepsilon}^p}$ and the third due to fracture \mathcal{D}_r .

So the mechanical part of \mathcal{D} is given by

$$\mathcal{D} = \overline{\sigma \dot{\varepsilon}^p} + \frac{1}{V} \int_{\partial\Omega_i} wc \, ds \geq 0 \quad (5.34)$$

With the hypothesis of macrohomogeneity applied to actual stresses, we can deduce

$$\Sigma \dot{E}_{IR} = \overline{\sigma \dot{\varepsilon}^p} + \overline{\sigma \Lambda_0 \dot{r}} \quad (5.35)$$

with

$$\overline{W} = \frac{1}{2} \overline{\sigma \Lambda_0 \sigma} = \frac{1}{2} \Sigma E_E + \frac{1}{2} \overline{r \Lambda_0 r}$$

and the equation

$$\mathcal{D}_f = \frac{1}{V} \int wc \, da = \overline{\sigma \dot{\varepsilon}} - \overline{\sigma \dot{\varepsilon}^p} - \frac{d}{dt} \left(\frac{1}{2} \Sigma E_E + w_b \right) \quad (5.36)$$

Using the macrohomogeneity hypothesis $\overline{\sigma \dot{\varepsilon}} = \Sigma E$

$$\mathcal{D}_f = \frac{1}{2} (\Sigma \dot{E}_E - \dot{\Sigma E}_E) + \overline{\sigma \Lambda_0 \dot{r}} - \frac{d}{dt} w_b \geq 0 \quad (5.37)$$

where $w_b = \frac{1}{2} \overline{r \Lambda_0 r}$. If the damaged zones do not propagate, $\mathcal{D}_f = 0$ and the macro compliance Λ is constant, we recover $dw_b/dt = \overline{r \Lambda_0 \dot{r}}$, i.e. the variation of the stored energy is only due to residual stresses, as in classical plasticity (Mandel, 1971; Bui *et al.*, 1982).

If there is propagation of damaged zones, the first term $\frac{1}{2} (\Sigma \dot{E}_E - \dot{\Sigma E}_E)$ does not vanish. It is analogous to Irwin's energy release rate for crack propagation (Bui, 1978) and it contributes to the dissipation rate.

6. THERMODYNAMICAL CONSIDERATIONS

6.1. Relationships between Micro and Macro Scales

In the preceding sections we were concerned by means of averaging processes and applications to define what are macroscopic mechanical quantities. We have said nothing about the macroscopic temperature or we have implicitly admitted that the temperature is given or corresponds to the temperature of the equilibrium state.

We have restricted our exposition to macrohomogeneous bodies; can we then give general relations for other materials?

To be specific, one will be concerned with materials that admit thermodynamical potentials, $e(\varepsilon, \alpha, s)$ internal energy or $w(\varepsilon, \alpha, \theta)$ free energy, where ε is the deformation, α the internal variables, θ the absolute temperature and s the entropy. Then the local equation of state may be written e.g.

$$\sigma = \rho \frac{\partial w}{\partial \varepsilon}; \quad s = -\frac{\partial w}{\partial \theta}; \quad A = -\rho \frac{\partial w}{\partial \alpha} \quad (6.1)$$

where σ is the elastic stress (this supposes no viscosity), and A are the thermodynamical forces associated with the variation of the internal variables α .

To determine the field of temperature, we must add to the constitutive equations (6.1) the heat conduction law. Noting $\xi = \nabla(\log \theta)$, we assume the following form for the generalized Fourier relation between heat flux and temperature:

$$q = -\frac{\partial \omega}{\partial \xi} \quad (6.2)$$

when $\omega(\xi)$ is a convex no-negative function of ξ .

As in the first section, it is clear that with every microscopic quantity f we can associate its macroscopic value \bar{f} by an averaging process on the RVE V extended eventually in the cases for which V contains holes, damaged zones, or rigid inclusions:

$$\bar{f} = \langle f \rangle = \frac{1}{V} \int_V f \, dv \quad (6.3)$$

and we have remarked that some constraints are necessary to determine a micro state corresponding to a given macro one. For the choice of a representative volume element suitable boundary conditions must be prescribed and must satisfy special requirements (Francfort *et al.*, 1983; Germain *et al.*, 1983):

R1 — Assume that the macro state $(\bar{\sigma}, \bar{\varepsilon}, \bar{\xi}, \bar{w})$ is given; the microscopic quantities f must then satisfy:

- the local constitutive law;
- the boundary conditions on ∂V ;
- the relation of averaging;

– the equation of equilibrium in stress and flux $\text{div } \sigma = 0$ and $\text{div } q = 0$ over V .

R2 – The Hill–Mandel macrohomogeneity condition must be fulfilled by all fields σ^* , q^* with $\bar{\sigma}^* = \langle \sigma^* \rangle$ and $\bar{q}^* = \langle q^* \rangle$ and by all fields ε^* and ξ^* kinematically and thermally admissible:

$$\left. \begin{aligned} \bar{\sigma}^* \bar{\varepsilon}^* &= \langle \sigma^* \varepsilon^* \rangle \\ \bar{q}^* \bar{\xi}^* &= \langle q^* \xi^* \rangle \end{aligned} \right\} \quad (6.4)$$

We have given particular localization processes for periodic structures and for homogeneous boundary conditions.

R3 – The process of localization must ensure the existence and uniqueness of the microscopic response.

The construction of the macro constitutive law from the microscopic behaviour can proceed as follows:

- starting from some macro quantities;
- using a localization process to determine local fields then the averaging process to determine the missing macro quantities.

6.2. Study of Systems in Equilibrium

In this case the homogeneous deformation $E = \bar{\varepsilon}$, the set of internal variables α and the temperature T of the macroscopic description are prescribed. Near the equilibrium we assume that the temperature is quasi-uniform $\theta = T$ (but the presence of heterogeneity implies that the gradient ξ is not uniform, $\xi \neq \bar{\xi}$).

We wish to find the local quantities $\sigma, \varepsilon, q, \xi$ as functions of the macro state $E, T, \alpha, \Xi = \bar{\xi}$; they are solutions of the boundary value problem (\mathcal{P}):

$$\left. \begin{aligned} E &= \langle \varepsilon \rangle & \sigma &= \rho \frac{\partial w}{\partial \varepsilon}(\varepsilon, \alpha, T) & \text{div}_y \sigma &= 0 \\ \Xi &= \langle \xi \rangle & q &= -\frac{\partial w}{\partial \xi} & \xi &= \nabla \log \theta & \text{div}_y q &= 0 \end{aligned} \right\} \mathcal{P} \quad (6.5)$$

Boundary conditions of localization

For a given localization process this solution is unique (R3). Let

$$\bar{\rho} \bar{w}(E; \alpha, T) = \langle \rho w(\varepsilon, \alpha, T) \rangle \quad (6.6)$$

where ε is the solution of the problem (\mathcal{P}). Using the hypothesis of

macrohomogeneity of Hill (R2), we obtain

$$\bar{\rho} \frac{\partial \bar{w}}{\partial E} = \left\langle \rho \frac{\partial w}{\partial \varepsilon} \frac{\partial \varepsilon}{\partial E} \right\rangle = \left\langle \sigma \frac{\partial \varepsilon}{\partial E} \right\rangle = \langle \sigma \rangle \frac{\partial \varepsilon}{\partial E}$$

and noting that $\varepsilon = E + \eta$ with $\langle \eta \rangle = 0$ for all E , so $\langle \partial \varepsilon / \partial E \rangle = 1$. The equation (6.6) gives the global behaviour

$$\bar{\rho} \frac{\partial \bar{w}}{\partial E} = \langle \sigma \rangle = \bar{\sigma} \quad (6.7)$$

and in the same way it can be proved that

$$\begin{aligned} \bar{s} &= -\partial \bar{w} / \partial T \\ T &= \partial \bar{e} / \partial \bar{s} \end{aligned} \quad (6.8)$$

The global description has the same form as the local one, and the equation (6.7) gives the constitutive stress-strain relation. Similarly it is possible to give the generalized Fourier relation between \bar{q} and $\bar{\xi}$.

If we consider that near a state of equilibrium the two principles of thermodynamics are valid at the microlevel

$$\left. \begin{aligned} \rho \dot{e} &= \sigma \dot{\varepsilon} - \operatorname{div} q \\ \rho \theta \dot{s} + \operatorname{div} q - q \cdot \xi &\geq 0 \end{aligned} \right\} \quad (6.9)$$

we can write the same relations at the macrolevel, if all the equations (6.6)-(6.9) are valid at each time, which means that the thermostatic description and the Gibbs equation are true for the equivalent homogeneous medium if they are valid for each of the constituent phases (Francfort *et al.*, 1983; Germain *et al.*, 1983).

6.3. Non-equilibrium Evolution

When the system is far from an equilibrium state, in particular when the local absolute temperature θ is not uniform on V , the equilibrium equation and the property of macrohomogeneity are not valid. Some complementary terms due to inertia phenomena must be taken into account. However, we can try to define the macroscopic temperature by the concept of a local accompanying equilibrium state.

At each time, the volume element V must be isolated and one has to study the dynamical evolution toward an equilibrium state and find the micro quantities which characterize this equilibrium. When the volume

element V is isolated, quantities such as the strain $E = \bar{\varepsilon}$ and energy \bar{e} , together with some internal parameter α , must be kept constant. Inside the RVE various physical dissipative mechanisms have taken place and each of them is described by the internal variable α . The dimensions of the RVE and the inertia effect define a characteristic time τ , and we must distinguish two kinds of internal parameters α and α' . The first family α can be considered as constant; the second α' , having a relaxation time shorter than τ , must be considered a function of time.

Under the assumption that in this transition towards equilibrium the two principles of thermodynamics are valid, the equilibrium state is the solution of the problem (6.5) where

$$E = \langle \varepsilon_t \rangle, \alpha = \alpha_t \quad \text{for } \alpha \notin \{\alpha'\} \quad \text{and } e = \langle e_t \rangle$$

are prescribed, and we obtain

$$\left. \begin{aligned} \Sigma^e &= \frac{\partial e}{\partial E}(E, \alpha, \alpha'^e, T^e) \\ S^e &= \frac{\partial e}{\partial T}(E, \alpha, \alpha'^e, T^e) \end{aligned} \right\} \quad (6.10)$$

where T^e and α'^e are the values of the macroscopic temperature and the values of internal parameters at the equilibrium state, respectively.

If the actual state is far from the equilibrium, it is obvious that $\Sigma^e \neq \langle \sigma_t \rangle$. Examples are given by Francfort (1982).

The major difficulty in this study is to define correctly the absolute temperature for a macroscopic body which has microheterogeneity. In the first part of this chapter we have studied only the quasi-static evolution of the RVE, for which the absolute temperature is defined as in Section 6.2.

7. CONCLUSION

We have presented some aspects of the general relations between micro and macro scales in heterogeneous media, and we have tried to exhibit some of the most significant lines of research in the mechanical behaviour of composite materials. This domain is still in a state of expansion, not only in solid mechanics but also in fluid mechanics and

in mixtures theory. In the next few years progress may be expected in many directions: better mathematical consistency, deepening of the physical interpretation and significance.

ACKNOWLEDGEMENTS

The author wishes to thank H. D. Bui, K. Dang Van and Q. S. Nguyen for discussion and for guidance.

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