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A control-oriented model of the current profile in Tokamak plasma

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Abstract. This paper proposes a control-oriented approach to the tokamak plasma current profile dynamics. It is established based on a consistent set of simplified relationships, in particular for the microwave current drive sources, rather than exact physical modelling. Assuming that a proper model for advanced control schemes can be established using the so-called *cylindrical approximation* and neglecting the diamagnetic effects, we propose a model that focuses on the flux diffusion (from which the current profile is inferred). Its inputs are some real-time measurements available on modern tokamaks and the effects of some major actuators, such as the magnetic coils, Lower Hybrid (LHCD), Electron and Ion Cyclotron Frequency (ECCD and ICRH) systems, are particularly taken into account. More precisely, the non-inductive current profile sources are modelled as 3-parameters functions of the control inputs derived either from approximate theoretical formulae for the ECCD and bootstrap terms or from experimental scaling laws specifically developed from Hard X-ray Tore Supra data for the LHCD influence. The use of scaling laws in this model reflects the fact that the operation of future reactors will certainly depend upon a great number of scaling laws and specific engineering parameters. The discretisation issues are also specifically addressed, to ensure the robustness with respect to discretisation errors and the efficiency (in terms of computation time) of the associated algorithm. This model is compared with experimental results and the CRONOS solver for Tore Supra Tokamak.

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1. Introduction

In the coming years the main challenge in the fusion community will be the development of experimental scenarios for ITER, the International Tokamak Experimental Reactor. Amongst them, the so-called advanced tokamak steady-state ones will play a significant role, since they will allow to reproduce and study (on a smaller scale), the conditions that are expected to be obtained in a fusion plant of reduced size and costs [1]. In these scenarios a particular emphasis is given to the current density profile and to the way of producing the plasma current I_p : due to the intrinsic limited availability of magnetic flux in the fusion devices, needed to sustain a purely inductive current, I_p will have to be mainly generated by non-inductive sources. In particular, the importance of the real-time safety factor profile (q -profile) control is emphasized in [2], where an interesting overview on recent advances and key issues in real-time tokamak plasma control is provided. A Proportional-Integral (PI) feedback control strategy, based on a simple linear model, is also proposed and its efficiency is illustrated by experimental results, which motivate further research developments in this direction.

The control of so-called “advanced” plasma regimes [1, 3, 4] for steady state high performance tokamak operation is a challenge, in particular because of the non-linear coupling between the current density and the pressure profiles. In a burning plasma, the alpha-particle power will also be a strong function of these profiles, and, through its effect on the bootstrap current, will be at the origin of a large (though ultra-slow) redistribution of the current density. The possible destabilization of adverse Toroidal Alfvén Eigenmodes (TAE) - such as the drift kinetic modes that are anticipated to appear at high values of the central safety factor [5] - as well as potential thermal instabilities due to the ITB dynamics will further complicate the issue. This motivates the need for further investigation of plasma profiles shaping to guarantee and control steady-state operation of the plasmas.

As far as experiments are concerned, real-time control of the internal inductance parameter (a measure of the current profile shape) has been achieved with LHCD on Tore Supra [6]. Improvement of plasma performance through active modification of the current density and pressure profiles in advanced plasma regimes with ITB's, through heating and current drive, or by inducing sheared plasma rotation, has also been the goal of intense research for example on TFTR [7], JT-60U [8, 9, 10], DIII-D [11], Alcator C-Mod [12] and JET [13, 14, 15]. Regarding the real-time (closed loop) control issues, some experimental investigations were carried on JET, especially on the regulation of lumped parameters characterizing the pressure profile in ITB discharges [16], for fixed magnetic flux configuration, of the full safety factor profile during the ITB preforming phase [17, 18] for non-inductive steady-state regime (using a linear relationship between the q -profile and the actuators), and, more recently, of the full q -profile during the main heating phase of the discharges.

The former control approaches have shown the interest of appropriate control methods to improve the plasma performances. Nevertheless, they are based on identified linear models of the plasma and/or semi-empirical tuning of the gains of a proportional-integrator controller, rendering the real-time control particularly sensitive to the operating conditions. The aim

of our work is then to propose a new, control-oriented model of the tokamak plasma that best reproduces the main influence of power and voltage modulations on the dynamics of the plasma profiles. This model does not pretend to have the accuracy of complex solvers (such as CRONOS, EFIT or EQUINOX), but has to represent the main control inputs influences on the plasma dynamics and to provide for some outputs of major interest for real-time control. It is then a first step towards model-based control of the plasma profile.

We focus on the flux diffusion dynamics and include some key physical knowledge on the tokamak plasma as well as the use of experimental results, which allows to represent the plasma behaviour for a large range of operating conditions and provides for a simplified and computationally efficient estimation of the main dynamics. Indeed, some approximate formulas are used to compute the resistivity and bootstrap current while the temperature and density profiles are estimated thanks to dedicated scaling laws. The non-inductive current profile sources are modelled as Gaussian distributions depending on the control inputs derived either from approximate theoretical formulas for ECCD or from experimental scaling laws specifically developed from Hard X-ray Tore Supra data for the LH term. The input-output relationships are detailed and special care is given to the discretisation issues. Such a model, essential for the phase of controller design (similarly to the numerous works done on plasma shape control), can then be used to quickly test some control laws for various operating conditions, to investigate the influence of specific parameters and to provide for a real time indication of not directly measurable quantities (such as the currents and q -factor profiles).

In order to keep the proposed plasma description as general as possible and to allow for advanced control methods, the model is presented as a non-linear system. Indeed, non-linear control and stability analysis is a field on intense research that can be drawn back to the end of the 19th century, with Lyapunov stability theory [19]. Numerous results have been obtained during the 20th century, on stability analysis (i.e. absolute stability, passivity and small-gains theorems, or input-output stability) as well as constructive control approaches (i.e. backstepping, non-linear adaptive control, feedforwarding or non-linear model-predictive control). An interesting historical survey of these topics is presented in [20] and in [21], which proposes an overview of non-linear model-predictive control (one of the most widely used control method in industry). Nowadays, numerous textbooks are available, presenting non-linear control from a global point of view [22, 23, 24] or focused on implementation issues [25, 26], differential geometric analysis [27, 28] or specific control methods [29, 30, 31], to cite some of the main references in this field. Our aim is then to propose a general input-output simplified description that allows for different control strategies (including the non-linear approaches) rather than focusing on a specific method.

This paper is organized as follows. First, the magnetic flux diffusion equation, with its initial and boundary conditions, is presented in Section 2. The estimation of the temperature and density profiles using some scaling laws based on experimental results is proposed in Section 3. Section 4 details the influence of the previous profiles on the flux diffusion, through the resistivity and the bootstrap current. The discretisation of the poloidal flux dynamics is investigated in Section 5, where an implicit-explicit discretisation scheme in time with a variable step in space is proposed. The inductive (magnetic coils) and non-inductive (ECCD

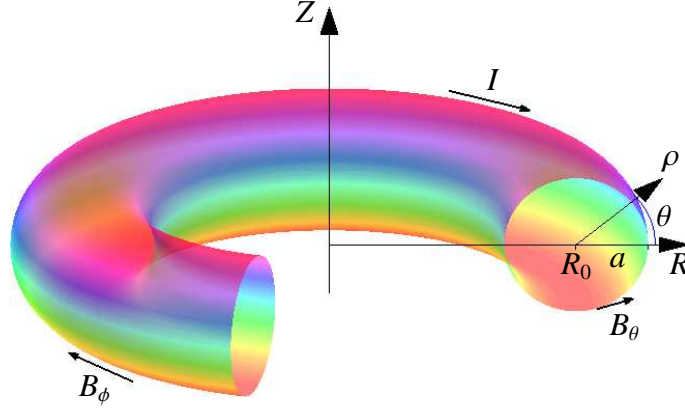


Figure 1. Plasma coordinates and sign convention.

and LHCD systems) inputs are described in Section 6. Section 7 details the computation of some model outputs of main interest. Finally, the numerical results obtained with the simulator associated with this model are compared with some experimental data from Tore Supra facility and with CRONOS code outputs in Section 8.

2. Magnetic flux diffusion

The notations and units of the main physical variables are summarized in Table 1. The physical variable considered here is the flux $\psi(R, Z)$ of the magnetic field $B(R, Z)$ passing through a disc centred on the toroidal axis at height Z and with a surface $S = \pi R^2$, where R is the large plasma radius, as depicted in Figure 1. It is defined in flux per radian as

$$\psi(R, Z) \doteq \frac{1}{2\pi} \int_S \mathbf{B}(R, Z) \cdot d\mathbf{S}$$

The dynamics of the poloidal flux is set by a diffusion equation, obtained from [32, 33] as

$$\frac{\partial \psi}{\partial t}(\rho, t) = D(\rho, t) \frac{\partial^2 \psi}{\partial \rho^2} + G(\rho, t) \frac{\partial \psi}{\partial \rho} + S(\rho, t) \quad (1)$$

where $D(\rho, t)$ and $G(\rho, t)$ are transport coefficients, $S(\rho, t)$ is a source term and ρ is the toroidal flux coefficient indexing the magnetic surfaces, defined as $\rho = (2\phi/B_{\phi_0})^{1/2}$, where $\phi(\rho, t)$ is the toroidal flux per radian and $B_{\phi_0}(t)$ is the central magnetic field. The transport coefficients and the source term are given by‡

$$D(\rho, t) = \frac{\eta_{\parallel} C_2}{\mu_0 C_3}, \quad G(\rho, t) = \frac{\eta_{\parallel} \rho}{\mu_0 C_3^2} \frac{\partial}{\partial \rho} \left(\frac{C_2 C_3}{\rho} \right) \quad \text{and} \quad S(\rho, t) = \frac{\eta_{\parallel} V'}{F C_3} \langle \mathbf{j}_{ni} \cdot \mathbf{B} \rangle = \frac{\eta_{\parallel} V' B_{\phi_0}}{F C_3} j_{ni}$$

where $\eta_{\parallel}(\rho, t)$ is the resistivity, $\mu_0 = 4\pi \times 10^{-7} H/m$ is the permeability of free space, $j_{ni}(\rho, t)$ is the non-inductive current source, including both the bootstrap effect and the microwave current drive, F is the diamagnetic function, $V(\rho, t)$ is the plasma volume and $V' = \partial V / \partial \rho$.

‡ In order to simplify the equations, the space and time dependencies are specified in the definitions of the variables and omitted otherwise.

Furthermore,

$$C_2 = V' \left\langle \frac{\|\rho\|^2}{R^2} \right\rangle, \quad C_3 = V' \left\langle \frac{1}{R^2} \right\rangle, \quad j_{ni}(\rho, t) \doteq \frac{\langle \mathbf{j}_{ni} \cdot \mathbf{B} \rangle}{B_{\phi_0}} \quad \text{and} \quad \langle A \rangle \doteq \frac{\partial}{\partial V} \int_V A \, dV$$

where $\langle A \rangle$ denotes the average of A on the flux surface which contains V .

We suppose that the diamagnetic effect (due to the poloidal currents) can be neglected, which implies that ρ can be considered as a geometric coefficient. We also assume that the so-called *cylindrical approximation* of the plasma geometry (large aspect ration) can be used as a basis to establish some control schemes using this model. The former approximation implies that $\rho \ll R_0$, $V = 2\pi^2\rho^2R_0$ and $V' = 4\pi^2\rho R_0$. Using both hypotheses, the transport coefficients can be computed with

$$F \doteq \frac{\mu_0 I_{tor}}{2\pi} \approx R_0 B_{\phi_0} \quad \text{and} \quad C_2 = C_3 = 4\pi^2 \frac{\rho}{R_0}$$

where I_{tor} is the toroidal coils current. Note that the cylindrical approximation could be relieved using some approximate expressions for C_2 , C_3 and V thanks to analytical formulas for shifted circles or numerical computations based on the 2D equilibrium description.

Remark 1 *A detailed analysis of this model, and more particularly concerning the choice of the coordinates, is presented in [34]. Simulations of the diffusion equation expressed in cylindrical and toroidal coordinates (taking into account the Shafranov shift) are compared with some experimental results. This comparison is performed through the value of $q(1, t)$ and shows that the proposed model fits well with the experimental results (the cylindrical approximation leads to a steady-state error of 10% and the toroidal model has an error of 2%). Other results show that the geometrical coefficients C_2 and C_3 are identical for both approximations up to a normalized radius of 0.8 and differs when approaching the plasma edge to reach a difference of 15%.*

With the previous approximations, the dynamics (1) of ψ simplifies to

$$\frac{\partial \psi}{\partial t}(\rho, t) = \frac{\eta_{\parallel}}{\mu_0} \frac{\partial^2 \psi}{\partial \rho^2} + \frac{\eta_{\parallel}}{\mu_0 \rho} \frac{\partial \psi}{\partial \rho} + \eta_{\parallel} R_0 j_{ni}$$

where ψ , η_{\parallel} and j_{ni} are both space (through ρ) and time dependent. The spatial index $\rho \in [0, a]$, where a is the minor plasma radius corresponding to the Last Closed Magnetic Surface (LCMS, constant if the diamagnetic effect is neglected) depicted in Figure 1, can be replaced by the normalized variable $x = \rho/a$. The diffusion equation considered finally writes as

$$\frac{\partial \psi}{\partial t}(x, t) = \frac{\eta_{\parallel}(x, t)}{\mu_0 a^2} \left(\frac{\partial^2 \psi}{\partial x^2} + \frac{1}{x} \frac{\partial \psi}{\partial x} \right) + \eta_{\parallel}(x, t) R_0 j_{ni}(x, t). \quad (2)$$

The initial and boundary conditions of this equation are detailed in the next subsections.

a	radius of the LCMS	m
\mathbf{B}_ϕ	toroidal magnetic field	T
\mathbf{B}_θ	poloidal magnetic field	T
B_{ϕ_0}	toroidal magnetic field (at the centre of the plasma)	T
C_R	conductivity reduction due to electron-electron collisions	
c	speed of light in free space, 3×10^8	m/s
e	electron charge, 1.6022×10^{-19}	C
f_t	fraction of trapped particles in the banana regime	
F	diamagnetic function	$T \times m$
I	plasma current at x	A
I_p	total plasma current	A
I_{tor}	toroidal coils current	A
j_{ni}	non inductive effective current density	A/m^2
$\ln \Lambda$	Coulomb logarithm	
M	average ion mass	
m_e	electron mass, 9.1096×10^{-31}	kg
n_e	electron density profile	m^{-3}
\bar{n}_e	electron line average density	m^{-2}
$N_{ }$	parallel refraction index	
P	loss power	W
P_{cd}	ECCD power	W
P_{icrh}	ICRH power	W
P_{lh}	LH power	W
P_{tot}	total input power	W
R	major plasma radius	m
R_0	magnetic centre location	m
T_e	temperature profile	eV
x	normalized radius	
\bar{Z}	effective value of the plasma charge	C
α_e	electron thermal speed	m/s
α_{Ti}	ratio of ion versus electron temperature	
ϵ	inverse aspect ratio (a/R_0)	
ϵ_0	permittivity of free space, 8.854×10^{-12}	F/m
$\eta_{ }$	plasma resistivity	$\Omega \times m$
γ_i	exponential peaking coefficient of the variable i	
κ	elongation	
μ_0	permeability of free space, $4\pi \times 10^{-7}$	H/m
ν_{*e}	electron collisionality parameter	
ϕ	magnetic flux of the toroidal field	T/m^2
ψ	magnetic flux of the poloidal field	T/m^2
τ_e	electron collision time	s
τ_{th}	thermal energy confinement time	s

Table 1. Most relevant physical variables and units

2.1. Initial value

The initial value of the poloidal flux $\psi(x, t_0)$ is determined from the initial safety factor profile $q(x, t_0)$ as follows. Defining the toroidal flux $\phi(x, t)$ as the magnetic flux per radians (to be consistent with the definition of ψ) passing through a poloidal surface centered at R_0 and with radius ρ , we have that

$$\phi(x, t) \doteq \frac{1}{2\pi} \int_{S_{pol}} \mathbf{B} \cdot d\mathbf{S}_{pol} = -\frac{1}{2\pi} \int_{S_{pol}} B_\phi \cdot dS_{pol} \approx -\frac{B_{\phi_0} a^2 x^2}{2}.$$

The safety factor is consequently defined as

$$q(x, t) \doteq \frac{d\phi}{d\psi} = \frac{\partial\phi/\partial x}{\partial\psi/\partial x} = -\frac{B_{\phi_0} a^2 x}{\partial\psi/\partial x}$$

and, integrating $\partial\psi/\partial\rho$ in space at time t_0 , we have that

$$\psi(x, t_0) = a^2 B_{\phi_0} \int_x^1 \frac{r}{q(r, t_0)} dr + \psi(1, t_0). \quad (3)$$

The choice of the constant term is motivated by the fact that $\psi(1, t)$ can be measured on the LCMS and can also constitute a boundary condition. The initial safety factor profile is given by

$$q(x, t_0) = (q(0, t_0) - q(1, t_0))(1 - x^{\gamma_q}) + q(1, t_0)$$

where $q(1, t)$ is computed as follows. First, Ampere's law is introduced to compute the plasma current $I(x, t)$ and q -profile as

$$I(x, t) = -\frac{2\pi x}{\mu_0 R_0} \frac{\partial\psi}{\partial x} \quad \Rightarrow \quad q(x, t) = \frac{2\pi a^2 x^2 B_{\phi_0}}{\mu_0 R_0 I}. \quad (4)$$

The safety factor on the LCMS is then $q(1, t) = (2\pi a^2 B_{\phi_0}) / (\mu_0 R_0 I_p)$ where $I_p(t) \doteq I(1, t)$ is the total plasma current.

For simulation purposes, an arbitrary initial safety factor profile can be chosen and the poloidal flux will converge to its actual value modulo a constant bias. The convergence property is inherited from the stability property of the diffusion equation and the bias is of minor importance since the variables of main interest (q and current profiles) depend on the flux gradient $\partial\psi/\partial x$. Further developments of this model for estimation purposes may use the real-time measurements of $\psi(1, t)$ to minimize the error between the modelled flux value on the LCMS and the real one (this is equivalent to design an observer for the flux profile that uses the measurements on the LCMS).

2.2. Boundary conditions

Specific boundary conditions have to be considered both at the plasma centre and on the LCMS. At the centre of the plasma, the spatial variation of the flux is zero:

$$\frac{\partial\psi}{\partial x}(0, t) = 0. \quad (5)$$

On the LCMS two exclusive conditions can be considered:

- on the flux variation, from (4),

$$\frac{\partial \psi}{\partial x}(1, t) = -\frac{R_0 \mu_0 I_p(t)}{2\pi} \quad (6)$$

- on the flux rate

$$\frac{\partial \psi}{\partial t}(1, t) = V_{loop}(t). \quad (7)$$

The last two boundary conditions are set by the tension applied to the coils, since a local control loop on the poloidal coil allows to set this tension according to the desired plasma current I_p or the desired loop voltage V_{loop} . This will be detailed in subsection 6.1.

To summarize the main results of this section, under the hypotheses that

H1) the diamagnetic effect is neglected,

H2) the plasma is described in cylindrical coordinates (large aspect ratio approximation),

the dynamics of the poloidal flux is described by (2) with the initial condition (3), the central boundary condition (5) and the edge boundary condition (6) or (7).

3. Temperature and density profiles

A first, classical approach to compute the temperature profile is based on the diffusion equation (i.e. for the electron temperature $T_e(\rho, t)$ expressed in cylindrical coordinates [35])

$$\frac{3}{2} \frac{\partial}{\partial t} [n_e T_e] = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\rho n_e \chi_e(\rho, t) \frac{\partial T_e}{\partial \rho} \right) - \frac{3n_e T_e}{2\tau_d} + S_T(\rho, t)$$

where $n_e(\rho, t)$ is the electron density, $\chi_e(\rho, t)$ is the electron thermal diffusivity, τ_d is a constant damping time modelling the losses and $S_T(\rho, t)$ is the source term. Denoting the electron pressure profile as $p_e(x, t)$, a simplified model can be set thanks to the relationship [36]

$$\chi_e = \alpha_B \frac{T_e}{B_{\phi_0}} \frac{a \nabla p_e}{p_e} q^2$$

with $\alpha_B = 2.5 \times 10^{-4}$. The source term has an amplitude such that

$$\int_0^1 S_{T,s}(x, t) dx = P_s$$

where the s subscript refers to the heating system considered (LHCD or ICRH) and P_s is the associated power input.

Considering the high level of uncertainty induced by diffusion models, such as the one presented above, to compute the temperature profile, we choose to use the empirical model proposed in [37], based on some experimental measurements. This model is established for *Tore Supra* operating in *L-Mode* but could easily be extended to other tokamaks or operating conditions by following the guidelines of the identification algorithm with appropriate experimental data. The main idea is to first estimate the normalized (with respect to $T_e(0, t)$) temperature profile shape with a set of sigmoid functions (these functions are close to 1 when

$x = 0$ and close to 0 when $x = 1$), which shape parameters are related to the tokamak global parameters with scaling laws. The thermal energy confinement is then introduced to compute the confinement time τ_{th} with a scaling law similar to ITERL-96P(th) [38]. The main advantage of this approach is to consider specifically the influence of LHCD and ICRH systems on the profile shape, as well as to provide for a simplified and fast computation method to estimate the global temperature behaviour. The resulting accuracy is sufficient for the proposed control-oriented model. Indeed, from a physical point of view, the dynamics of ψ (on which this paper is focused) has a time constant that is one order of magnitude larger than the temperature one. This difference of time scales motivates the fact that the global energy and steady-state variations are more important than the temperature transient behaviour in the time-variation of ψ . For *Tore Supra* tokamak operating in *L-mode*, the temperature estimation is described as follows.

The electron temperature profile is estimated with a sigmoid function as

$$T_e(x, t) \approx \frac{\alpha(t)}{1 + e^{-\beta(t)(x-\gamma(t))}} A_{Te}(t)$$

where the normalized shape of the profile $T_e(x, t)/T_e(0, t)$ is estimated with a sigmoid function defined by its amplitude $\alpha(t)$, dilatation $\beta(t)$ and translation (inflection point) $\gamma(t)$. The amplitude of the profile is $A_{Te}(t)$ and computed from the plasma thermal energy, as detailed below. The extra degree of freedom introduced in the time-variation of α (which would ideally be 1) is motivated by the fact that, for the computation of the resistive properties of the plasma, the minimization of the estimation error over the complete profile is more important than an accurate estimation of the central temperature.

The shape parameters are set with the switched model

$$\{\alpha, \beta, \gamma\} = \begin{cases} \{\alpha_{lh}, \beta_{lh}, \gamma_{lh}\} & \text{if } P_{lh} \neq 0 \\ \{\alpha_{\omega}, \beta_{\omega}, \gamma_{\omega}\} & \text{else.} \end{cases}$$

This model then distinguishes the LHCD heating effect from the ohmic and ICRH ones. Selecting the most significant terms, the shape parameters are related to the global and engineering parameters with

$$\begin{cases} \alpha_{lh} = e^{-0.87} I_p^{-0.43} B_{\phi_0}^{0.63} N_{\parallel}^{0.25} \left(1 + \frac{P_{icrh}}{P_{tot}}\right)^{0.15} \\ \beta_{lh} = -e^{3.88} I_p^{0.31} B_{\phi_0}^{-0.86} \bar{n}_e^{-0.39} N_{\parallel}^{-1.15} \\ \gamma_{lh} = e^{1.77} I_p^{1.40} B_{\phi_0}^{-1.76} N_{\parallel}^{-0.45} \left(1 + \frac{P_{icrh}}{P_{tot}}\right)^{-0.54} \\ \alpha_{\omega} = e^{-0.37} I_p^{-0.46} B_{\phi_0}^{0.23} \bar{n}_e^{0.22} \\ \beta_{\omega} = -e^{1.92} I_p^{0.38} \bar{n}_e^{-0.33} \\ \gamma_{\omega} = e^{-0.15} I_p^{1.03} B_{\phi_0}^{-0.51} \left(1 + \frac{P_{icrh}}{P_{tot}}\right)^{-0.46} \end{cases}$$

where $N_{\parallel}(t)$ is the parallel refraction index, $P_{icrh}(t)$ is the ICRH power, $P_{lh}(t)$ is the LHCD power, $P_{tot}(t)$ is the total input power and $\bar{n}_e(t)$ is the electron line average density. The units of the parameters used in the scaling laws are $[s, MA, T, 10^{19} m^{-3}, MW]$ for $[time, current, density, power]$. Note that N_{\parallel} and P_{icrh} have more effect on the profile shape associated with LHCD than P_{lh} , which still appears implicitly in P_{tot} . Indeed, identifying the exponent parameters with either $(1 + P_{icrh}/P_{tot})$ or $(1 + P_{lh}/P_{tot})$ in the scaling law leads to the conclusion that the first term gives the minimum cost function. This can be physically explained by the fact that the presence (or absence) of ICRH has more effect on the shape than some modulations in P_{lh} . A more accurate model could be obtained by distinguishing the case when LHCD is operated alone from the case when both LHCD and ICRH are used.

To determine the central temperature, the plasma thermal energy $W_{th}(t)$ can be written as

$$W_{th}(t) = W_e(t) + W_i(t) = \frac{3e}{2} \int_V (n_e T_e + n_i T_i) dV = \frac{3e}{2} \int_V (1 + \alpha_{Ti} \alpha_{ni}) n_e T_e dV$$

where $n_i(x, t) \approx \alpha_{ni}(t) n_e(x, t)$ is the ions density, $T_i(x, t) \approx \alpha_{Ti}(t) T_e(x, t)$ is the ions temperature, and $W_{th}(t)$ and $W_{e,i}(t)$ are the electrons and ions energies, respectively. The density ratio is given $\alpha_{ni}(t) \approx (7 - \bar{Z}(t))/6$, where $\bar{Z}(t)$ is the effective plasma charge, averaged on the small plasma radius. The ratio of ion to electron temperature is established from measurements taken at the centre of the plasma and obtained from the scaling law

$$\alpha_{Ti}(t) \approx 1 - 0.31 \left(\frac{I_p}{B_{\phi_0}} \right)^{-0.38} \bar{n}_e^{-0.90} \left(1 + \frac{P_{icrh}}{P_{tot}} \right)^{-1.62} \left(1 + \frac{P_{lh}}{P_{tot}} \right)^{1.36}.$$

The electrons density $n_e(x, t)$ is approximated with

$$n_e(x, t) \approx \frac{\gamma_n + 1}{\gamma_n} (1 - x^{\gamma_n}) \bar{n}_e(t)$$

where γ_n is the density peaking. From the previous approximations and the cylindrical coordinates hypothesis, the temperature profile amplitude is related to W_{th} thanks to the relationship $A_{Te}(t) = \mathcal{A}(t) W_{th}(t)$ with

$$\mathcal{A}(t) \doteq \left[6\pi^2 a^2 R_0 e (1 + \alpha_{Ti} \alpha_{ni}) \int_0^1 n_e(x, t) x \frac{\alpha(t)}{1 + e^{-\beta(t)(x-\gamma(t))}} dx \right]^{-1}$$

and W_{th} is estimated with

$$\begin{cases} \tau_{th}(t) &= 0.135 I_p^{0.94} B_{\phi_0}^{-0.15} \bar{n}_e^{0.78} \left(1 + \frac{P_{lh}}{P_{tot}} \right)^{0.13} P_{tot}^{-0.78} \\ \frac{dW_{th}}{dt} &= P_{tot} - \frac{1}{\tau_{th}} W_{th}, \quad W_{th}(0) = P_{tot}(0) \tau_{th}(0) \end{cases}$$

where $\tau_{th}(t)$ is the thermal energy confinement time with the scaling law established in [37]. The scaling law ITERL-96P(th) is more general (based on measurements from different tokamaks) and can also be used in this scheme. In that case, τ_{th} is given by

$$\tau_{th,ITER} = 0.14 I_p^{0.96} B_{\phi_0}^{0.03} \bar{n}_e^{0.40} P_{tot}^{-0.73}.$$

Remark 2 For a real-time use of this model, the temperature profile can also be accurately measured directly from the Electron Cyclotron Emission (ECE diagnostic) for $x = 0 - 0.8$ and the density profile can be obtained from combined interferometers (these measurements were used to set the proposed scaling laws). In this case, the model can be used to provide, in real-time, for physical quantities that can not be measured directly, such as the safety factor, currents and current densities (associated with the different sources), and induced voltage profiles. The normalized inductance, confinement efficiency and Grad-Shafranov shift would also be available, as detailed in Section 7.

4. Resistivity and bootstrap current

The diffusion term in (2) is provided by $\eta_{||}$ and the bootstrap current $j_{bs}(x, t)$ is an autogenerated source that introduces a non-linearity in the diffusion equation. Both of them introduce a coupling, which is varying in time and space, between the magnetic flux diffusion presented in Section 2 and the temperature and density profiles of Section 3.

4.1. Resistivity model

This parameter is computed using the results on neoclassical conductivity proposed in [39], where an approximate analytic approach is presented. First of all, the electron thermal velocity and Braginskii time are computed from the temperature and density profiles as [40]

$$\alpha_e(x, t) = \sqrt{\frac{eT_e}{m_e}} \quad \text{and} \quad \tau_e(x, t) = \frac{12\pi^{3/2}m_e^{1/2}\epsilon_0^2}{e^{5/2}\sqrt{2}} \frac{T_e^{3/2}}{n_e \ln \Lambda}$$

where $e = 1.6022 \times 10^{-19} C$ is the electron charge, $\epsilon_0 = 8.854 \times 10^{-12} F/m$ is the permittivity of free space, $m_e = 9.1096 \times 10^{-31} kg$ is the electron mass and $\ln \Lambda(x, t)$ is the Coulomb logarithm, obtained from $\ln \Lambda(x, t) = 31.318 + \ln(T_e / \sqrt{n_e})$. The parallel conductivity is then given by

$$\frac{\sigma_{||}(x, t)}{\sigma_0} = \Lambda_E \left(1 - \frac{f_t}{1 + \xi v_{*e}} \right) \left(1 - \frac{C_R f_t}{1 + \xi v_{*e}} \right)$$

with

$$\begin{aligned} \sigma_0(x, t) &= \frac{n_e e^2}{m_e} \tau_e, \quad \Lambda_E(\bar{Z}) = \frac{3.40}{\bar{Z}} \left(\frac{1.13 + \bar{Z}}{2.67 + \bar{Z}} \right), \quad v_{*e}(x, t) = \frac{R_0 q}{(x\epsilon)^{3/2} \alpha_e \tau_e}, \\ f_t(x) &= 1 - (1 - x\epsilon)^2 (1 - (x\epsilon)^2)^{-1/2} (1 + 1.46 \sqrt{x\epsilon})^{-1}, \quad \xi(\bar{Z}) = 0.58 + 0.20\bar{Z} \\ \text{and } C_R(\bar{Z}) &= \frac{0.56}{\bar{Z}} \left(\frac{3.0 - \bar{Z}}{3.0 + \bar{Z}} \right). \end{aligned}$$

where $v_{*e}(x, t)$ is the electron collisionality parameter, $f_t(x)$ is the fraction of trapped particles in banana regime and $C_R(\bar{Z})$ is the conductivity reduction due to electron-electron collisions. The resistivity is finally inferred from $\sigma_{||}$ as $\eta_{||}(x, t) \doteq 1/\sigma_{||}$.

Remark 3 The validity of this approach is investigated in [41], where various models of conductivity (Hirsmann analytic formula, Hirshman formulation and Shaing formulation) are

compared with experimental results. The model presented here (Hirshman analytic formula) is valid for low density, for arbitrary aspect ratio and banana regime (the collisionality goes to zero), or for finite collisionality and $\epsilon \ll 1$.

4.2. Bootstrap current source

This current is generated by trapped particles and may be the main source of non inductive current in specific scenarios (high bootstrap experiments). We present here the model derived by Hirshman [42] and presented in a comparative perspective in [43]. It is a single ion, collisionless regime model, which writes in our framework as

$$\frac{\langle \mathbf{j} \cdot \mathbf{B} \rangle_{bs}}{\langle \mathbf{B} \cdot \nabla \phi \rangle} = \frac{p_e}{\langle 1/R^2 \rangle} \left\{ A_1 \left[\frac{1}{p_e} \frac{dp_e}{d\psi} + \frac{p_i}{p_e} \left(\frac{1}{p_i} \frac{dp_i}{d\psi} - \alpha_i \frac{1}{T_i} \frac{dT_i}{d\psi} \right) \right] - A_2 \frac{1}{T_e} \frac{dT_e}{d\psi} \right\}$$

where $p_i(x, t)$ is the pressure due to ions and

$$A_1(x, t) = x_t \left[0.754 + 2.21\bar{Z} + \bar{Z}^2 + x_t (0.348 + 1.243\bar{Z} + \bar{Z}^2) \right] / D_e$$

$$A_2(x, t) = x_t (0.884 + 2.074\bar{Z}) / D_e, \quad \alpha_i(x) = \frac{1.172}{1.0 + 0.462x_t}$$

$$D_e(x, t) = 1.414\bar{Z} + \bar{Z}^2 + x_t (0.754 + 2.657\bar{Z} + 2\bar{Z}^2) + x_t^2 (0.348 + 1.243\bar{Z} + \bar{Z}^2)$$

where $x_t(x)$ is the ratio of trapped to circulating particles $f_t/(1-f_t)$. Considering the cylindrical coordinates approximation and defining the bootstrap current as

$$j_{bs} \doteq \frac{\langle \mathbf{j} \cdot \mathbf{B} \rangle_{bs}}{B_{\phi_0}} = \frac{1}{R_0} \frac{\langle \mathbf{j} \cdot \mathbf{B} \rangle_{bs}}{\langle \mathbf{B} \cdot \nabla \phi \rangle}$$

we have

$$j_{bs}(x, t) = \frac{p_e R_0}{\partial \psi / \partial x} \left\{ A_1 \left[\frac{1}{p_e} \frac{\partial p_e}{\partial x} + \frac{p_i}{p_e} \left(\frac{1}{p_i} \frac{\partial p_i}{\partial x} - \alpha_i \frac{1}{T_i} \frac{\partial T_i}{\partial x} \right) \right] - A_2 \frac{1}{T_e} \frac{\partial T_e}{\partial x} \right\}$$

The relationships $p_e = en_e T_e$ and $p_i = en_i T_i$ are introduced to express the bootstrap current in terms of temperature and density profiles as

$$j_{bs}(x, t) = \frac{eR_0}{\partial \psi / \partial x} \left\{ (A_1 - A_2)n_e \frac{\partial T_e}{\partial x} + A_1 T_e \frac{\partial n_e}{\partial x} + A_1 (1 - \alpha_i)n_i \frac{\partial T_i}{\partial x} + A_1 T_i \frac{\partial n_i}{\partial x} \right\}$$

Another possibility is to estimate the fraction of the total current due to the bootstrap effect with the fitting law proposed in [44].

5. Discretisation of the poloidal flux dynamics

Considering the dynamics obtained in (2), we wish to discretise

$$\dot{\psi}(x, t) = \frac{\eta_{\parallel}(x, t)}{\mu_0 a^2} \left(\psi''(x, t) + \frac{1}{x} \psi'(x, t) \right) + \eta_{\parallel}(x, t) R_0 j_{ni}(x, t) \quad (8)$$

where $\dot{\psi} \doteq \partial \psi / \partial t$ and $\psi' \doteq \partial \psi / \partial x$. Applying the spatial and temporal discretisation methods (A.1)-(A.3) described in Appendix A, the previous equation writes as (i.e. in the explicit case)

$$\begin{aligned} \dot{\psi}(x_i, t)_{ex} &= \frac{\eta_{\parallel i, j}}{\mu_0 a^2} (d_2 \psi_{i+1, j} - d_3 \psi_{i, j} + d_4 \psi_{i-1, j}) + \frac{d_1 \eta_{\parallel i, j}}{\mu_0 a^2 x_i} (\psi_{i+1, j} - \psi_{i-1, j}) + \eta_{\parallel i, j} R_0 j_{ni, j} \\ &= \eta_{\parallel i, j} (e_1 \psi_{i+1, j} - e_2 \psi_{i, j} + e_3 \psi_{i-1, j} + R_0 j_{ni, j}) \end{aligned}$$

with

$$e_1(i) = \frac{d_2(i)x_i + d_1(i)}{\mu_0 a^2 x_i}, \quad e_2(i) = \frac{d_3(i)}{\mu_0 a^2} \quad \text{and} \quad e_3(i) = \frac{d_4(i)x_i - d_1(i)}{\mu_0 a^2 x_i}$$

where the subscript $i = 1 \dots N$ denotes the spatial discretisation points and j refers to the time samples. Similarly, for the implicit case we have that

$$\dot{\psi}(x_i, t)_{im} = \eta_{\parallel i, j+1} \left(e_1 \psi_{i+1, j+1} - e_2 \psi_{i, j+1} + e_3 \psi_{i-1, j+1} + R_0 j_{ni, j} \right).$$

Note that we used $j_{ni, j}$ instead of $j_{ni, j+1}$ in the previous computation. This is motivated by the fact that $j_{ni, j}$ is a non-linear function of $\psi_{1 \dots N, j}$ (bootstrap effect and LH source when the boundary condition is set on V_{loop}). A formulation with $j_{ni, j+1}$ would then prevent the use of a linear computation method that takes the sources at time j as an input. Taking the time step sufficiently small compared to the system dynamics, this approximation introduces a negligible error that is worth the computation simplification and is compensated by the fact that the dynamics considered is stable.

Substituting the previous equalities into

$$\left(\frac{\psi_{i, j+1} - \psi_{i, j}}{\delta t} \right) = h \dot{\psi}(x_i, t)_{ex} + (1 - h) \dot{\psi}(x_i, t)_{im}$$

where $h \in [0, 1]$ is the ratio of explicit to implicit time discretisation and δt is the sampling time, a discretised version of (8) finally writes as

$$\begin{aligned} A_{i, i+1, j} \psi_{i+1, j} + A_{i, i, j} \psi_{i, j} + A_{i, i-1, j} \psi_{i-1, j} \\ - B_{i, i+1, j} \psi_{i+1, j+1} - B_{i, i, j} \psi_{i, j+1} - B_{i, i-1, j} \psi_{i-1, j+1} + S_{i, j} = 0 \end{aligned} \quad (9)$$

where A_j and B_j are time-varying $N \times N$ matrices. The notations $A_{i, k, j}$ and $B_{i, k, j}$ are introduced to denote the values of the matrix elements (i, k) at the time sample j , and

$$\begin{aligned} A_{i, i-1, j} &= \eta_{\parallel i, j} e_3 h \delta t, \quad A_{i, i, j} = 1 - \eta_{\parallel i, j} e_2 h \delta t \\ A_{i, i+1, j} &= \eta_{\parallel i, j} e_1 h \delta t, \quad B_{i, i-1, j} = -\eta_{\parallel i, j+1} e_3 (1 - h) \delta t \\ B_{i, i, j} &= 1 + \eta_{\parallel i, j+1} e_2 (1 - h) \delta t, \quad B_{i, i+1, j} = -\eta_{\parallel i, j+1} e_1 (1 - h) \delta t \\ S_{i, j} &= R_0 \delta t \left[h \eta_{\parallel i, j} + (1 - h) \eta_{\parallel i, j+1} \right] j_{ni, j} \end{aligned}$$

for $i = 2, \dots, N - 1$ (the values at 1 and N are given by the boundary conditions) and where δt is the sampling time. Writing the poloidal flux and the sources term in the vector form

$$\psi_j = [\psi_{1, j} \quad \psi_{2, j} \quad \dots \quad \psi_{N, j}]^T \quad \text{and} \quad S_j = [S_{1, j} \quad S_{2, j} \quad \dots \quad S_{N, j}]^T$$

(9) can be expressed, equivalently, in the matrix form

$$A_j \psi_j - B_j \psi_{j+1} + S_j = 0 \quad \Leftrightarrow \quad \psi_{j+1} = B_j^{-1} A_j \psi_j + B_j^{-1} S_j.$$

Note that the matrix B_j is tridiagonal, by construction. An appropriate inversion method such as the one proposed in [45] is therefore recommended to compute B_j^{-1} with reduced computational cost.

The boundary conditions presented in subsection 2.2 may induce some numerical instability due to the discretisation scheme. Some appropriate specific discretisation methods are described below.

At the centre: the proposed discretisation method leads to an ill defined central value of the flux dynamics when $x_1 = 0$ since

$$\frac{\psi'(x_1, t)}{x_1} \rightarrow \frac{0}{0}.$$

Consequently, we use the fact that the diffusion term close to the origin can be approximated by

$$\frac{1}{x} \frac{\partial}{\partial x} \left[x \frac{\partial \psi}{\partial x} \right] \approx \frac{1}{\delta x_2/4} \frac{(\delta x_2/2) \times \psi'_{1/2}}{\delta x_2/2} = \frac{4}{\delta x_2} \psi'_{1/2} \approx \frac{4}{\delta x_2^2} (\psi_2 - \psi_1)$$

with $\delta x_i = x_i - x_{i-1}$ to set the central dynamics as

$$\dot{\psi}(x_1, t) \approx \eta_{\parallel 1}(t) \left[\frac{4}{\mu_0 a^2 \delta x_2^2} (\psi_2 - \psi_1) + R_0 j_{ni 1}(t) \right].$$

The central terms of (9) are then computed with

$$\begin{aligned} A_{1,2,j} &= e_{bc0} h \eta_{\parallel 1,j}, & A_{1,1,j} &= 1 - e_{bc0} h \eta_{\parallel 1,j}, & B_{1,2,j} &= -e_{bc0} (1-h) \eta_{\parallel 1,j+1}, \\ B_{1,1,j} &= 1 + e_{bc0} (1-h) \eta_{\parallel 1,j+1} & \text{and} & & S_{1,j} &= \delta_t R_0 (h \eta_{\parallel 1,j} j_{ni 1,j} + (1-h) \eta_{\parallel 1,j+1} j_{ni 1,j+1}) \end{aligned}$$

where $e_{bc0} = 4\delta_t / (\mu_0 a^2 \delta x_2^2)$.

At the edge, with $\psi'(1, t)$: the constraint on the flux variation $\psi'(1, t) = u(t)$ implies that

$$\frac{\psi_{N,j+1} - \psi_{N-1,j+1}}{\delta x_N} = u_{j+1} \quad \Leftrightarrow \quad -\frac{\psi_{N,j+1}}{\delta x_N} + \frac{\psi_{N-1,j+1}}{\delta x_N} + u_{j+1} = 0.$$

The corresponding matrix coefficients are then

$$A_{N,N-1,j} = A_{N,N,j} = 0, \quad B_{N,N-1,j} = -B_{N,N,j} = -\frac{1}{\delta x_N} \quad \text{and} \quad S_{N,j} = u_{j+1}.$$

The computation of $u(t)$ is directly obtained from (6) as $u(t) = -R_0 \mu_0 I_p / (2\pi)$.

At the edge, with $\dot{\psi}(1, t)$ a last possibility to set the edge boundary condition is to use $\dot{\psi}(1, t) = V_{loop}(t)$. In this case we have

$$\psi_{N,j+1} - \psi_{N,j} - \delta t V_{loop,j} = 0$$

and the matrix coefficients are

$$A_{N-1,N,j} = B_{N-1,N,j} = A_{N,N-1,j} = B_{N,N-1,j} = 0, \quad A_{N,N,j} = B_{N,N,j} = 1 \quad \text{and} \quad S_{N,j} = \delta t V_{loop,j}.$$

6. Model inputs

The model inputs considered in this work are the boundary conditions at the plasma edge ($\psi'(1, t)$ or $\dot{\psi}(1, t)$, see subsection 2.2) and the non inductive currents generated by the LHCD and ECCD systems. Both systems current deposits can be roughly modelled with Gaussian curves, described in Appendix B, whose shape depends on the global plasma parameters and power inputs.

6.1. Inductive current input

The magnetic flux at the boundary $\dot{\psi}(1, t)$ is set by the coils surrounding the plasma and constitutes the inductive current input. This can be described by the classical transformer model where the coils generate the primary circuit while the plasma is the secondary, modelled as a single filament. The dynamics of the coils current $I_c(t)$ is then set by [46]

$$\begin{aligned} L_c \dot{I}_c + M \dot{I}_p + R_c I_c - V_c &= 0 \\ M \dot{I}_c + L_p \dot{I}_p + R_p (I_p - I_{NI}) &= 0 \end{aligned}$$

where R_c and L_c are the coils resistance and internal inductance, R_p and L_p are the plasma resistance and inductance, M is the matrix of mutual inductances, V_c is the input voltage applied to the coils and I_{NI} is the current generated by the non inductive sources. Note that the values of R_c and L_c are given from the coil properties while M is obtained thanks to an equilibrium code (i.e. CEDRES on Tore Supra). The magnetic flux at the plasma boundary close to the coils ψ_{ac} is then obtained with $\dot{\psi}_{ac} = M \dot{I}_c$. Considering the effects of the plasma current and inductance variations, the loop voltage V_{loop} is obtained from [47]

$$V_{loop}(t) = \dot{\psi}(1, t) = -\frac{1}{I_p} \frac{\partial}{\partial t} \left[\frac{L_p I_p^2}{2} \right] + \dot{\psi}_{ac}$$

where $L_p = \mu_0 R_0 l_i / 2$ and l_i is the normalized internal inductance. In practice, a local control law is set on the poloidal coils to adjust the value of V_c according to a desired value of V_{loop} , which can be measured with a Rogowski coil. If the reference is set on the plasma current I_p instead, then V_c is such that the coils provide for the current necessary to complement the non inductive sources.

6.2. ECCD deposit

The total EC current is the sum of several deposits due to several EC beams, which parameters are denoted by the subscript m . Each current deposit is determined by the position of the steering mirror ($R_{ant,m}, Z_{ant,m}$), its orientation in the poloidal and toroidal plane ($\phi_{pol,m}, \phi_{tor,m}$), and the emission power $P_{cd,m}$, as presented in Figure 2. The results presented in this section are derived from [48] and [49]. The assumption is that the wave is absorbed by the plasma (and generates current) for

$$R_c > R > R_m^*$$

where

$$R_c = n_h \frac{e \mu_0 n_b n_t I_{ind}}{4 \pi^2 m_e f} \quad \text{and} \quad R_m^* = \frac{R_{ant,m}}{\sqrt{2} |\sin \phi_{tor,m}|} \left[1 - \sqrt{1 - \frac{4 R_c^2}{R_{ant,m}^2} \sin^2 \phi_{tor,m}} \right]^{1/2}$$

with $n_h = 1, 2$ the harmonic considered, n_b the number of toroidal coils, n_t the number of wire loops per coil, f the antenna frequency (in GHz) and I_{ind} the coil induction current. For high magnetic field (O-mode) the first harmonic is absorbed ($n_h = 1$) while for low magnetic field

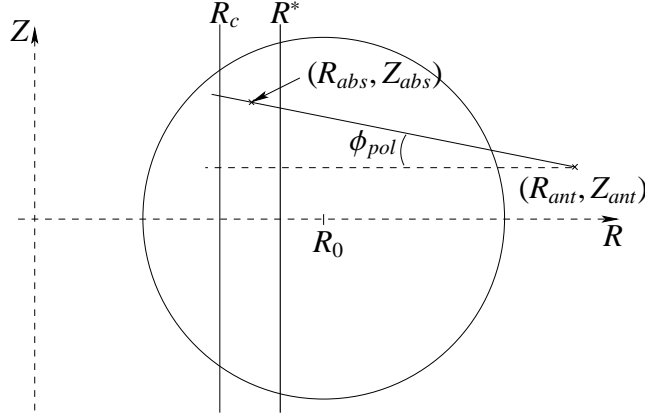


Figure 2. Poloidal deposit of the ECCD antenna (one mirror).

(X-mode) the deposit is generated by the second harmonic. The maximum is considered to happen at $R_{abs,m} = (R_c + R_m^*)/2$ and the Z coordinate of each point is computed from

$$Z_m(R) = Z_{ant,m} + (R_{ant,m} - R) \tan \phi_{pol,m}$$

The flux coordinates of the deposit are then obtained from

$$\rho_m(R) = \left| \frac{R - R_0}{Z_{ant,m} + (R_{ant,m} - R) \tan \phi_{pol,m}} \right|.$$

The global efficiency factor $\gamma_{cd,m}(t)$ is computed as

$$\gamma_{cd,m}(t) = \frac{\Gamma_1 T_e(x_{abs,m})}{T_e(x_{abs,m}) + 10^5} \left\{ 1 - \Gamma_2 \left[\frac{\rho_m(R_{abs,m}) + R_{abs,m} - R_0}{R_{abs,m}} \right]^{\Gamma_3} \right\}$$

where

$$x_{abs,m} = \rho_m \frac{R_{abs,m}}{a}, \quad \Gamma_1 = \frac{6}{5 + \bar{Z}}, \quad \Gamma_2 = \frac{4(2 + \bar{Z})}{3(1 + \bar{Z})} \quad \text{and} \quad \Gamma_3 = \frac{5 + \bar{Z}}{2(1 + \bar{Z})}$$

and the amplitude of the current deposit $I_{cd,m}(t)$ is obtained from

$$\gamma_{cd,m} = \frac{I_{cd,m}}{P_{cd,m}} R_0 \bar{n}_e \times 10^{-20} \quad \Leftrightarrow \quad I_{cd,m} = \frac{\gamma_{cd,m} P_{cd,m}}{R_0 \bar{n}_e \times 10^{-20}} = 2\pi a^2 \int_0^1 x j_{cd,m}(x, t) dx$$

where $j_{cd,m}(x, t)$ is the current density induced by ECCD.

The next step is to express the coefficients of the Gaussian fitting curve

$$j_{cd,m} = \vartheta_{cd,m} e^{-(\mu_{cd,m} - x)^2 / 2\sigma_{cd,m}}$$

in terms of the engineering parameters derived previously. The mean and the variance are obtained as

$$\mu_{cd,m} = \frac{\rho_m(R_{abs,m})}{a} \quad \text{and} \quad \sigma_{cd,m} = -\frac{(\mu_{cd,m} - \rho_m(R_c)/a)^2}{2 \ln \beta}$$

where β is chosen such that $j_{cd,m}(x_c) = \vartheta_{cd,m}\beta \approx 0$ (i.e. $\beta = 1/10$, which is equivalent to set the Gaussian curve close to zero at R_c). The maximum value of the current deposit is consequently computed as

$$\vartheta_{cd,m} = \frac{\gamma_{cd,m} P_{cd,m}}{R_0 \bar{n}_e} \left[2\pi a^2 \int_0^1 x e^{-(\mu_{cd,m}-x)^2/2\sigma_{cd,m}} dx \right]^{-1}.$$

Finally, the ECCD source is positive if the antenna is directed against the plasma current I_p (which means that it emits in the same direction as the plasma electrons) and the total current density profile induced by ECCD is

$$j_{cd}(x, t) = \sum_{m=1}^6 j_{cd,m}(x, t) \times \text{sign}(\phi_{tor,m}).$$

Example 1 *Tore Supra tokamak ECCD system is currently working with two beams. The current deposit is set with*

$$\max(P_{cd}) = [250 \ 300] \times 10^3, \quad R_{ant} = [3.53 \ 3.53] \quad \text{and} \quad Z_{ant} = [0 \ 0.2].$$

Furthermore, $I_{ind} = 137 \times B_{\phi_0} R_0$, $n_B = 18$ and $n_t = 2028$.

6.3. LHCD deposit

The current profile generated by this system cannot be adequately described with an analytical formula as it is the case for ECCD. Indeed, it strongly depends on the operating conditions and current density profile [50]. A more realistic way to estimate this profile is to use the emission of suprathermal electrons provided by the Hard X-Ray (HXR) measurements [51] to build up a scaling law from engineering control parameters. A classical guess is to suppose that the LH power deposit corresponds to the emission of electrons with an energy ranging from 60 to 80 keV, which is measured with the HXR diagnostic. It is motivated by the fact that LHCD system specifically generates a population of electron in this range of energies. Neglecting the thermal effect, we then consider that the radial Hard X-Ray emission profile corresponds to the current density profile $j_{lh}(x, t)$ [50].

The first step is to determine the shape of the current deposit from the HXR measurements. This can be done empirically from the global parameters thanks to the curve fitting approach described in Appendix C, where the width $w_{hxr}(t)$ and centre of the deposit $\mu_{hxr}(t)$ are estimated as

$$\begin{aligned} \hat{w}_{hxr}(t) &= 0.53 B_{\phi_0}^{-0.24} I_p^{0.57} \bar{n}^{-0.08} P_{LH}^{0.13} N_{\parallel}^{0.39} \\ \hat{\mu}_{hxr}(t) &= 0.20 B_{\phi_0}^{-0.39} I_p^{0.71} \bar{n}^{-0.02} P_{LH}^{0.13} N_{\parallel}^{1.20} \end{aligned}$$

where N_{\parallel} is the parallel refractive index that can be computed from phase difference measurements. Note that a direct measurement of the parameters involved in the scaling law is available in real-time for advanced control schemes.

The total current deposit $I_{lh}(t)$ is computed from the plasma and LHCD parameters thanks to the current drive efficiency $\eta_{lh}(t)$ with the fitting laws proposed in [52] (for Tore Supra and

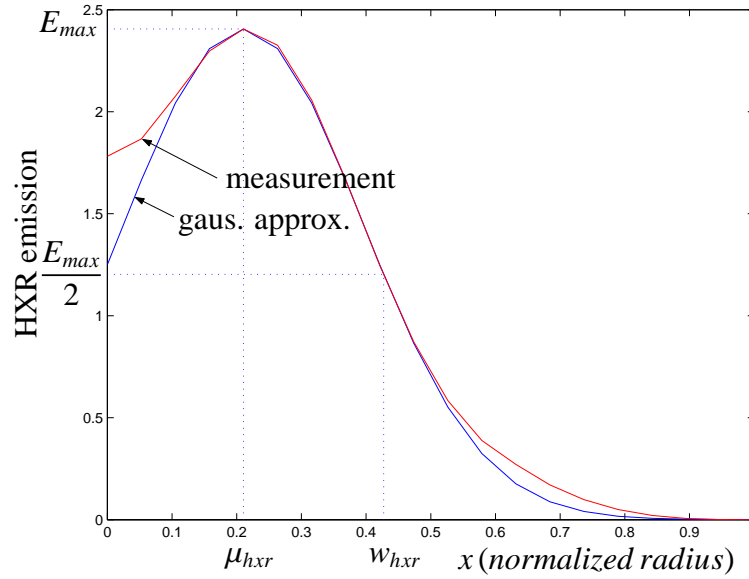


Figure 3. Measured LH deposit vs. its Gaussian approximation.

JET)

$$\eta_{lh}(t) = 3.39D_n^{0.26}\tau_{lh}^{0.46}\bar{Z}^{-0.13} \quad \text{or} \quad \eta_{lh}(t) = 1.18D_n^{0.55}I_p^{0.43}\bar{Z}^{-0.24}$$

where $D_n(t) \approx 2.03 - 0.63N_{||}$ is the normalized directivity. The total current is then obtained as $I_{lh}(t) = \eta_{lh}P_{lh}/(\bar{n}_eR_0)$. The LHCD profile $j_{lh}(x, t)$ is finally described by the Gaussian approximation

$$j_{lh}(x, t) = \vartheta_{lh}e^{-(\mu_{hxr}-x)^2/2\sigma_{lh}}$$

with

$$\sigma_{lh}(t) = \frac{(\mu_{hxr} - w_{hxr})^2}{2 \ln 2} \quad \text{and} \quad \vartheta_{lh}(t) = I_{lh} \left[2\pi a^2 \int_0^1 x e^{-(\mu_{hxr}-x)^2/2\sigma_{lh}} dx \right]^{-1}.$$

Note that the integral term can be computed using numerical integration techniques or with the relationship

$$\int_0^1 x e^{-(\mu_{hxr}-x)^2/2\sigma_{lh}} dx = -\sigma_{lh} \left(e^{-(1-\mu)^2/2\sigma_{lh}} - e^{-\mu^2/2\sigma_{lh}} \right) + \mu \sqrt{\frac{\sigma_{lh}\pi}{2}} \left[\text{erf} \left(\frac{1-\mu}{\sqrt{2\sigma_{lh}}} \right) - \text{erf} \left(\frac{-\mu}{\sqrt{2\sigma_{lh}}} \right) \right]$$

A comparison between the measured and estimated HXR emission profile is presented on Figure 3, where E_{max} is the maximum emission value, for a typical LHCD pulse. The uncertainty on the measured values close to the origin is high, which further supports the choice of a Gaussian curve to fit the measurements.

6.4. Resulting model properties

To summarize the results obtained in the previous sections, the proposed model is mainly based on a physical analysis of the plasma flux diffusion and current sources. This analysis is completed with some scaling laws to compute the LHCD current deposit, and possibly the temperature profiles. The shape of LHCD deposit is based on experimental measurements carried on Tore Supra while its amplitude is established from both Tore Supra

and JET measurements. For control design purposes, the temperature profiles can be roughly approximated thanks to the proposed scaling laws or an analytical model. Another possibility, which should be preferred for advanced control design since it fully uses the available diagnostics, is to consider the temperature profiles as some real-time inputs to the model, provided by ECE.

The use of scaling laws, even if they imply that the model is not fully predictive, is motivated by the fact that a large amount of experimental data is available for the actual tokamaks and their use in the design of future facilities, as illustrated in [38]. The large amount of physical properties included in the model allows reducing the error and operation dependency induced by such laws to a level that is acceptable for control design purposes, where global dependencies are more important than detailed models.

Such an approach is also motivated by the results obtained in [18] and similar works, where encouraging closed-loop performances for the q -profile control were obtained using a simple linearised model identified from experimental data. Even if linear approaches structurally imply a strong dependency on the operating conditions, the previous results have shown the interest of model-based control design to regulate the plasma profiles. Our aim is then to contribute to further progresses in this direction by providing for a model with strong physical dependencies and not restricted to the linear framework, that still allows for real-time implementation and can be used in non-linear control schemes.

7. Model outputs

Several outputs of major interest for control applications are presented in this section, as well as a practical method to compensate for the cylindrical approximation and estimate the security factor and current densities profiles in toroidal coordinates.

7.1. Total current and effective current density

For an arbitrary current denoted with the subscript s to indicate the source (ohmic, LHCD, ECCD or effective), the total current $I_s(x, t)$ is obtained, with the cylindrical approximation, by integrating the current density $j_s(x, t)$ on the surface $\pi a^2 x^2$ as

$$I_s(x, t) = 2\pi a^2 \int_0^x x j_s(x, t) dx.$$

The effective current density of the plasma $j_\phi(x, t)$ is obtained from the spacial derivative of the previous equality and Ampere's law (4) as

$$j_\phi(x, t) = \frac{1}{2\pi a^2 x} \frac{\partial I}{\partial x} = \frac{1}{2\pi a^2 x} \frac{\partial}{\partial x} \left[-\frac{2\pi x}{\mu_0 R_0} \frac{\partial \psi}{\partial x} \right] = -\frac{1}{\mu_0 R_0 a^2 x} \frac{\partial}{\partial x} \left[x \frac{\partial \psi}{\partial x} \right].$$

Note that the toroidal current at the plasma edge $j_\phi(1, t)$ can be used to estimate the model precision since it is usually measured using a continuous Rogowski coil or a discrete set of magnetic coils surrounding the plasma.

7.2. Toroidal induced voltage

It is induced by changes in both the primary circuit current and plasma current, and writes as $V(x, t) = \partial\psi/\partial t$. It is computed using the results of Section 5 as

$$V_{i,j} = h\eta_{\parallel i,j} \left(e_1\psi_{i+1,j} - e_2\psi_{i,j} + e_3\psi_{i-1,j} + R_0 j_{mi,j} \right) \\ + (1-h)\eta_{\parallel i,j+1} \left(e_1\psi_{i+1,j+1} - e_2\psi_{i,j+1} + e_3\psi_{i-1,j+1} + R_0 j_{mi,j+1} \right)$$

for $i = 2 \dots N - 1$ and with the appropriate boundary conditions for $V_{1,j}$ and $V_{N,j}$. Note that the voltage at the edge of the plasma $V(1, t)$ is the loop voltage $V_{loop}(t)$, which is measured with a toroidal loop of wire parallel to the plasma.

7.3. Ohmic current

This current is usefull to analyse the various components of the total current profile and is computed from

$$\langle \mathbf{j} \cdot \mathbf{B} \rangle_{\Omega} = \sigma_{\parallel} \langle \mathbf{E} \cdot \mathbf{B} \rangle = \sigma_{\parallel} E_{\parallel} B_{\phi_0}$$

where $E(x, t)$ is the electric field. Introducing the voltage profile, we obtain, equivalently,

$$j_{\Omega}(x, t) = \frac{\langle \mathbf{j} \cdot \mathbf{B} \rangle_{\Omega}}{B_{\phi_0}} = -\frac{\sigma_{\parallel}}{R} V(x, t) \approx -\frac{\sigma_{\parallel}}{R_0} V(x, t).$$

7.4. Normalized internal inductance

Defined as [40]

$$l_i(x, t) \doteq \frac{\bar{B}_{\theta}^2(x, t)}{B_{\theta}^2(1)} = \frac{2 \int_0^1 B_{\theta}^2(x, t) dx}{B_{\theta}^2(1)}$$

it is expressed is terms of the poloidal flux using Biot-Savart law $B_{\theta}(x, t) = \psi'/(aR_0)$ as

$$l_i(x, t) = \frac{2 \int_0^1 \psi'^2(x, t) dx}{\psi'^2(1, t)} = \frac{8\pi^2}{\mu_0^2 R_0^2 I_p^2} \int_0^1 \psi'^2(x, t) dx.$$

7.5. Confinement efficiency

This is a global parameter that evaluates the confinement of the plasma pressure by the magnetic field. It is defined as the ratio between the average perpendicular pressure and the edge poloidal magnetic pressure [53, 40]

$$\beta_{\theta}(t) \doteq \frac{\langle p \rangle}{B_{\theta}^2(1, t)/2\mu_0} = \frac{4}{\mu_0 R_0 I_p^2} \int_V p dV = \frac{8W_{th}}{3\mu_0 R_0 I_p^2}$$

where the last equality is obtained from the cylindrical approximation.

7.6. Grad-Shafranov (GS) shift and geometrical correction

An alternative to the computation of the GS equilibrium is to approximate the GS shift $\Delta(x, t)$ from the global parameters defined above. This allows for a comparison between the profiles obtained with the cylindrical approximation and those obtained in toroidal coordinates. The central value of the GS shift $\Delta(0, t)$ is approximated with

$$\Delta(0, t) \approx \frac{a^2}{2R_0} \left(\beta_\theta + \frac{li}{2} \right) \left(1 - \frac{a}{R_0} \right).$$

Assigning a profile shape to the GS shift, it is computed as $\Delta(x, t) \approx \Delta(0, t)(1 - x^2)$.

The GS shift can be used to estimate the q -profile in toroidal coordinates $q_{tor}(x, t)$. Indeed, q_{tor} is given by [34]

$$q_{tor}(\rho, t) = -\frac{B_{\phi_0} R_0}{\partial\psi/\partial x} \left[\Delta' + \frac{\rho - (R_0 + \Delta)\Delta'}{\sqrt{(R_0 + \Delta)^2 - \rho^2}} \right].$$

The toroidal approximation is then obtained thanks to the relationship

$$q_{tor}(x, t) = \frac{R_0}{ax} \left[\Delta' + \frac{ax - (R_0 + \Delta)\Delta'}{\sqrt{(R_0 + \Delta)^2 - (ax)^2}} \right] \times q(x, t) \quad (10)$$

where $q(x, t)$ is the safety factor profile considered previously and computed from the dynamics of ψ .

The effective plasma current density is more difficult to express in toroidal coordinates with a GS shift. Indeed, this would require to compute

$$\langle \mathbf{j}_\phi \cdot \mathbf{B}_\phi \rangle = -\frac{FC_{2tor}}{\mu_0 V'_{tor}} \left(\frac{\partial^2 \psi}{\partial \rho^2} + \frac{\partial \ln(C_{2tor})}{\partial \rho} \frac{\partial \psi}{\partial \rho} \right)$$

with

$$C_{2tor} = 4\pi^2 \left(\frac{\rho}{\sqrt{(R_0 + \Delta)^2 - \rho^2}} - \frac{\Delta'}{\sqrt{1 - \Delta'^2}} \right) \frac{\rho}{\rho - (R_0 + \Delta)\Delta'}$$

and $V'_{tor} = 4\pi^2 \rho (R_0 + \Delta + \rho\Delta'/2)$. A simpler way to take into account the geometry issues is to use the definition of the effective current $I_\phi(x, t) = V' \langle B_\phi^2 \rangle / 2\pi\mu_0$ and the ratio $I_{\phi tor}(1, t)/I_{\phi cyl}(1, t) = 1 - \Delta_0(t)/2$ to set the boundary condition (6) as $\psi'(1, t) = -R_0\mu_0 I_p(t)/2\pi \times (1 - \Delta_0(t)/2)$.

8. Simulations and comparisons with experimental results

The control-oriented model derived in this paper is now compared with some experimental measurements and the results obtained with the CRONOS code [54], an integrated modelling tool that solves the transport equations along with the Grad-Shafranov equilibrium in toroidal coordinates. The complexity of this solver prevents any real-time implementation but it is an experimentally-based reference that we can use to validate our results. We refer to our model results with ψ_{sim} , as name and subscript for the associated simulator, and compare them with the experimental (*exp*) and CRONOS signals.

This comparison does not intend to be exhaustive but focuses on two specific cases of main interest. The first one is an ohmic shot with ICRH modulations and illustrates the diffusive behaviour of the plasma model as well as some discretisation issues. The second one is a LHCD shot, to illustrate the impact of the proposed scaling laws related to this system and of a non-inductive current source. In both cases the boundary condition of the diffusion equation is set with the plasma current $I_p(t)$ and a test case with $V_{loop}(t)$ illustrates the LHCD shot. The simulations are carried with 20 uniformly distributed space steps and with a sampling time of 10 ms.

8.1. Ohmic and bootstrap effects

We analyse here the model results on Tore Supra shot 33632, which doesn't involve ECCD nor LHCD. In this shot, the temperature and density profiles are modulated with the ICRH power and the plasma has the following steady-state characteristics: $I_p = 1.0$ MA, $B_{\phi_0} = 3.19$ T and $n_{e0} = 4.5 - 3.0 \times 10^{-19} m^{-3}$.

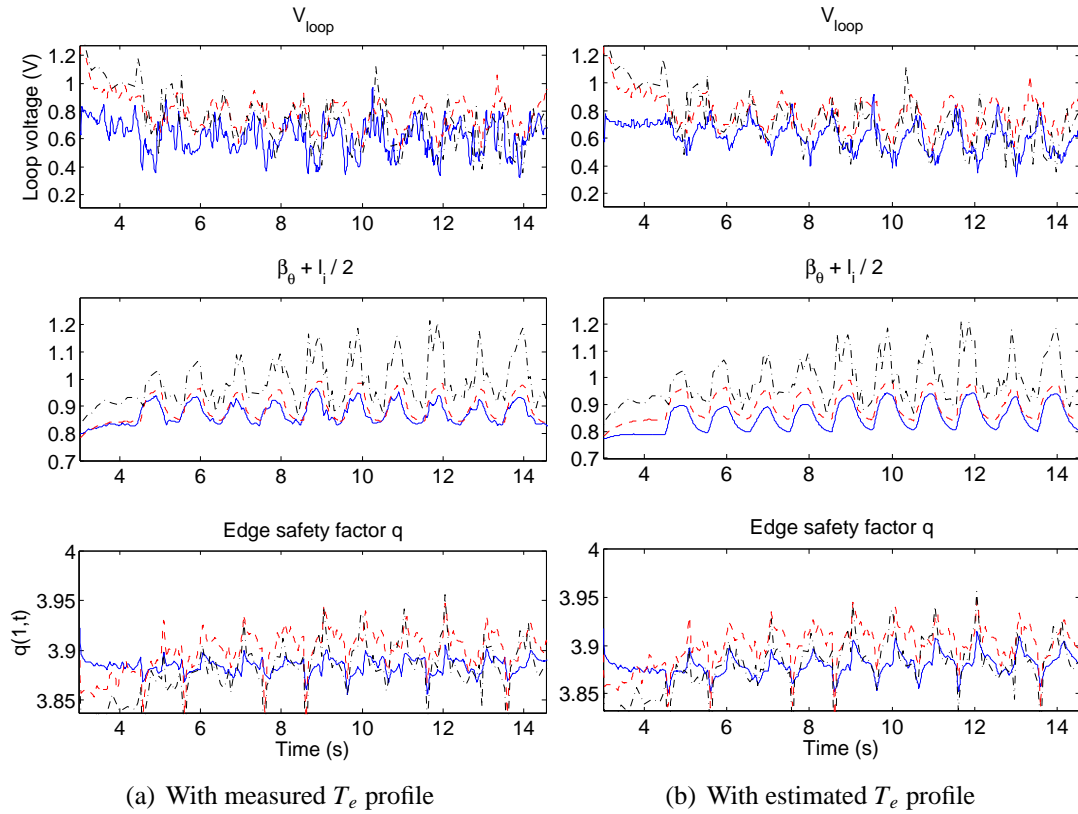


Figure 4. Comparison of ψ_{sim} (—) with experimental measurements (---) and CRONOS signals (-·-) for shot TS-33632, based on the loop voltage (top), the measurement of $\beta_\theta + l_i/2$ (middle) and the safety factor at the edge of the plasma (bottom).

The first comparison is performed on the magnetic measurement and presented in Figure 4, where the top part depicts the loop voltage, the middle part is $\beta_\theta + l_i/2$ and the bottom part is the safety factor at the edge of the plasma $q_{tor}(1, t)$ (computed with the corrected

formula (10)). ψ_{sim} is run both using the temperature and density profiles measurements (Figure 4(a)) and in a fully predictive way (Figure 4(b)). The later case means that ψ_{sim} has only the global parameters of the plasma and P_{icrh} as inputs but doesn't use the temperature and density measurements. The proposed shape scaling laws and ITERL-96P(th) (for the thermal confinement time) set the temperature and density profiles. This test case is a worst-case example since the central safety factor is less than one and there is a high frequency saw tooth effect on the temperature profiles, which is not explicitly taken into account in the temperature model.

The results of ψ_{sim} and CRONOS are equivalent for V_{loop} , except during the current ramp up and ramp down (not represented here) phases, which imply some particular phenomena that we didn't consider. The magnetic measurement of $\beta_\theta + l_i/2$ is best represented with ψ_{sim} , even in the predictive mode. The constant bias on $q(1, t)$ due to the cylindrical approximation (reported in [34]) is successfully compensated by the geometrical correction proposed in Subsection 7.6.

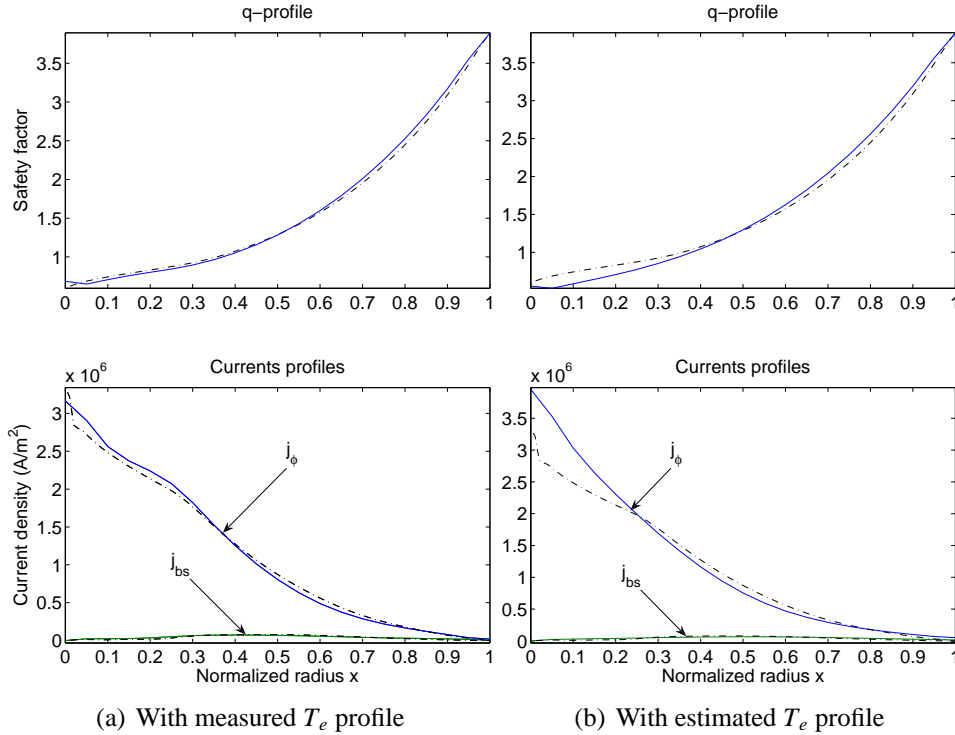


Figure 5. Comparison of ψ_{sim} (—) with CRONOS (---) for shot TS-33632 at $t = 7$ s, based on the safety factor profiles (top) and the current densities (effective j_ϕ and bootstrap j_{bs}) profiles (bottom).

The second comparison is focused on the safety factor and current densities profiles. There is no experimental measurements available for these physical variables so we compare ψ_{sim} with CRONOS only. The difference between the use of the temperature and density profiles, and the use of their approximation is also illustrated and is more significant than in the first comparison. The q -profile is presented on top of Figure 5: we have an almost perfect matching between CRONOS and ψ_{sim} when the measured profiles are used (Figure 5(a)) and

Mode	Discretisation	N	$e_{V_{loop}}$ (%)	Simulation time (s)
Meas. prof.	Uniform	20	7.37	1.09
Predictive	Uniform	100	5.56	8.53
Predictive	Non-uniform	100	5.46	8.81
Predictive	Uniform	20	5.84	1.77
Predictive	Non-uniform	20	5.18	1.76
Predictive	Uniform	10	5.64	1.30
Predictive	Non-uniform	10	4.66	1.27

Table 2. Effect of the spatial distribution

a small difference, located at the centre of the plasma, for the predictive mode (Figure 5(b)). The same conclusion is verified for the effective current density profile, with a more important mismatching at the centre. This illustrates the influence of the temperature on the flux diffusion, through $\eta_{||}$ (which is proportional to $T_e^{3/2}$). Nevertheless, the accuracy of the q -profile may be sufficient for most control applications, especially considering that this specific case study includes saw teeth and that the model can be updated with real-time measurements from the Hard X-rays in advanced control setups.

The impact of the spatial discretisation strategy is presented in Table 2. The non-uniform distribution $\delta x_i = 2/N + \sqrt{ai}$, where a is such that $\sum \delta x_i = 1$, is compared with the uniform distribution for different numbers of discretisation points N thanks to the resulting error on the loop voltage

$$e_{V_{loop}} \doteq \frac{\int_{t_0}^{t_f} (V_{loop-\psi_{sim}}(t) - V_{loop-exp}(t))^2 dt}{\int_{t_0}^{t_f} V_{loop-exp}^2(t) dt}$$

and to the simulation time (obtained when the simulator is built with *Matlab*[®] on an Intel[®] 2CPU - 2 GHz PC operated with Windows NT[®]). In each case, the non-uniform distribution is performing better than the uniform one in terms of the error on V_{loop} , and increasing the number of points does not necessarily decrease the error. This issue would clearly deserve further analysis, as the optimal discretisation would depend on the system properties and dynamics, but will not be investigated in this work. Instead, we proposed a discretisation scheme that allows for various possibilities and refer to [55, 56], where the effects of PDE models discretisation is thoroughly investigated.

8.2. Lower Hybrid effect

The LH system is now introduced in ψ_{sim} and compared with CRONOS and experimental results. The simulator behaviour is tested for the operating conditions of Tore Supra shot 35109, which is characterized by some variations in $N_{||}$, a constant I_p (0.6 MA) and a constant power input (1.8 MW).

The magnetic measurements $V_{loop}(t)$, $\beta_\theta + I_i/2$ and $q(1, t)$ are presented in Figure 6, where experimental measurements, CRONOS and ψ_{sim} are compared. The cases with

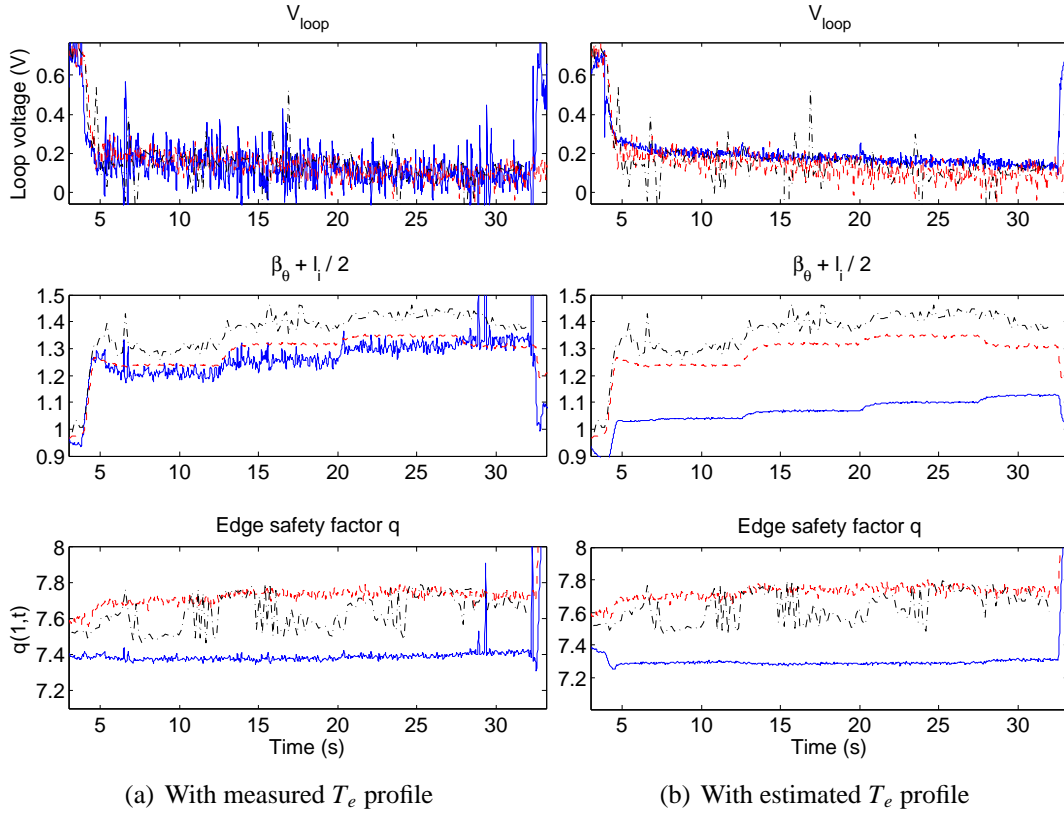


Figure 6. Comparison of ψ_{sim} (—) with experimental measurements (---) and CRONOS signals (-.-) for shot TS-35109, based on the loop voltage (top), the measurement of $\beta_\theta + I_i/2$ (middle) and the safety factor at the edge of the plasma (bottom).

measured and estimated temperature profiles are both considered, in Figures 6(a) and 6(b), respectively. In both cases there is no significant difference on $V_{loop}(t)$ while $q(1, t)$ is slightly underestimated (the correction proposed in Subsection 7.6 only partially compensate the cylindrical approximation effect). The main difference appears on $\beta_\theta + I_i/2$, which is underestimated when the temperature profile is estimated.

The safety factor and current densities profiles for ψ_{sim} (run with measured and estimated temperature profiles) and CRONOS are presented in Figure 7. The q -profile provided by ψ_{sim} has a small difference with CRONOS close to the centre, especially on Figure 7(b). The peculiar behaviour of CRONOS current profiles for $x < 0.5$ may be due to some computational artefacts and should not be taken into account into this comparison. The profile of j_{th} is reasonably well represented as well as the bootstrap profile, which is particularly accurate when the measured temperatures and densities are available.

The last profiles, presented on Figure 8, are obtained using $V_{loop}(t)$ to set the boundary condition. While these profiles are not as close to CRONOS results as those obtained with $I_p(t)$, they are still consistent with the plasma behaviour. The difference between the two cases (I_p and V_{loop}) mainly comes from the fact that the scaling laws are set with I_p , which means that the computation error induced on the plasma current when it is considered as an output is fed back into the model through the inputs and more specially in the predictive mode, as

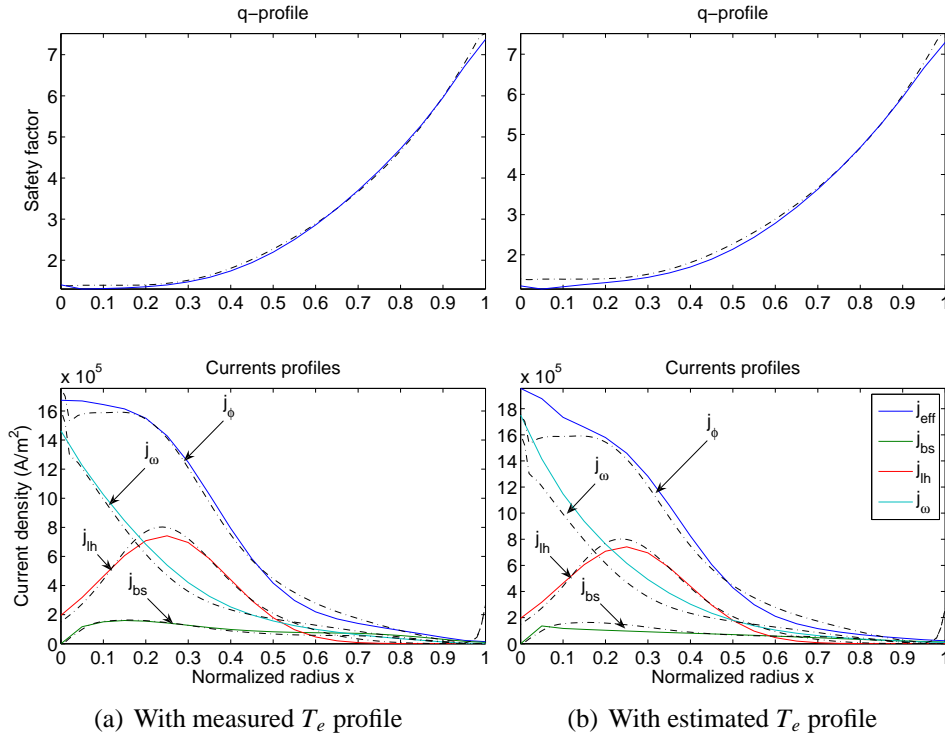


Figure 7. Comparison of ψ_{sim} (—) with CRONOS (---) for shot TS-35109 at $t = 7$ s, based on the safety factor profiles (top) and the current densities (effective j_ϕ , LH j_{lh} , ohmic j_ω and bootstrap j_{bs}) profiles (bottom).

illustrated in Figure 8(b).

To conclude on this comparison between ψ_{sim} and experimental results or CRONOS, the proposed model provide for some satisfactory results (accurate enough for control applications), even with a long sampling time and a small number of discretisation points. The effects of the main control inputs are well represented and the computation time is small (5 s for shot TS-35109). Comparing the errors on the safety factor profiles introduced by the use of the temperature scaling laws show that the model, at least for the q -profile, is not too much sensible to these laws, as long as the orders of magnitude are suitably represented. For the magnetic measurement $\beta_\theta + l_i/2$, the scaling laws introduce a constant bias.

9. Conclusions

We proposed in this work a new, control-oriented, model of the current diffusion in tokamak plasma. The current profile dynamics was modelled by the 1D magnetic flux diffusion equation, using approximate formulae of the neoclassical resistivity coefficient and the bootstrap current. The non-inductive current sources were considered as Gaussian distributions depending on the control inputs, which are derived either from approximate theoretical formulae for the ECCD or from experimental scaling laws specifically developed from Hard X-ray Tore Supra data for the LHCD term (the proposed method is detailed and can easily be applied to other tokamaks, provided that Hard X-ray measurements are available).

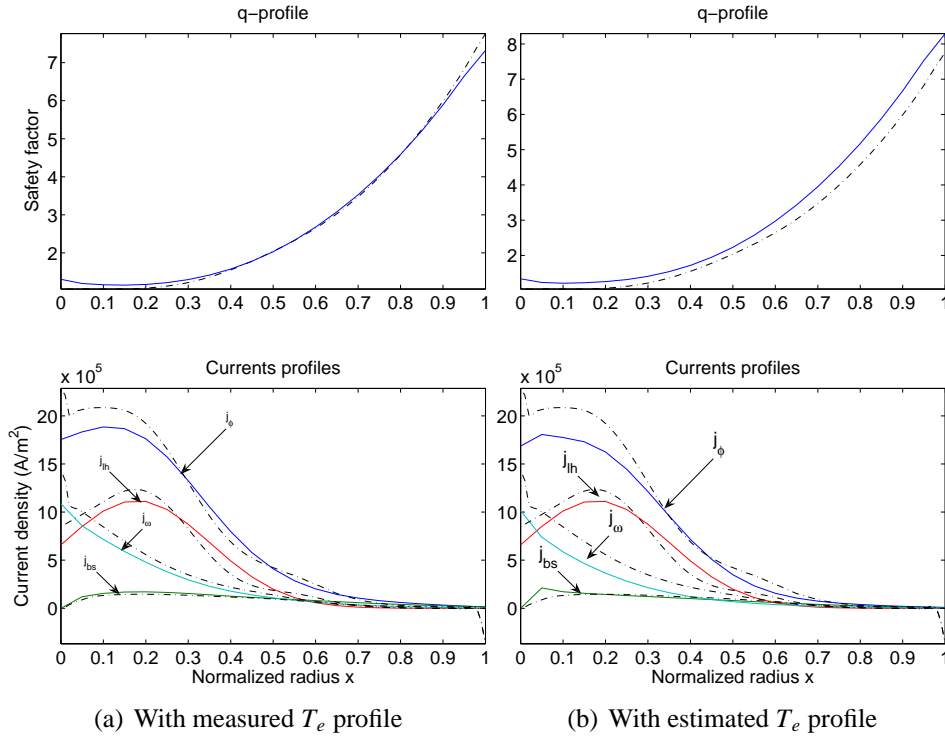


Figure 8. Comparison of ψ_{sim} using V_{loop} as a boundary condition (—) with CRONOS (---) for shot TS-35109 at $t = 28.2$ s, based on the safety factor profiles (top) and the current densities (effective j_ϕ , LH j_{lh} , ohmic j_ω and bootstrap j_{bs}) profiles (bottom).

The input-output relationships and the discretisation issues (in time and space) were detailed to provide for a model that is computationally efficient and robust, and particularly suited for advanced control of the plasma profiles. For example, it can be used directly to estimate the plasma evolution over a short time-range from real-time measurements and included in model-based predictive control schemes. The model structure also suggests that nonlinear analysis may be an interesting tool for further developments in plasma profile control and to estimate the associated performance limitation.

A new simulation tool was developed according to this model, to allow for a comparison with Tore Supra experimental data and CRONOS code outputs. Based on two different shots, this comparison was carried out on the magnetic measurements as well as the safety factor and current densities profiles. The precision of the model and its computational efficiency have shown to be particularly satisfying for future control applications. Such a tool can also estimate the safety factor, current densities, toroidal voltage and confinement efficiency in real time from the global parameters and temperature profiles measurements.

Appendix A. Discretisation method

This section presents a discretisation method that has a variable step in the spatial domain and is implicit-explicit in the temporal domain. The spatial discretisation method is motivated by the fact that an improved resolution may be desired in specific regions (such as the plasma

centre) with a limited number of discretisation points. The choice of these points can be determined by the actuators/sensors placement or by the control objectives. The temporal discretisation method allows for a trade-off between numerical stability and precision. We consider the function $f(x, t)$ and denote by $f_{i,j}$ its value at x_i , $i = 1, \dots, N$, and at time $j\delta t$, where δt is the sampling time and $j \in \mathbb{N}^+$ is the time index considered.

Appendix A.1. Variable-step spatial differentiation

The sampling interval is defined as $\delta x_i = x_i - x_{i-1}$, with $\delta x_1 = x_1 = 0$. Using Taylor's series, we can write the general formula

$$f(x + \Delta x, t) = f(x, t) + \Delta x f'(x, t) + \frac{\Delta x^2}{2} f''(x, t) + O(3)$$

where $f'(\cdot) \doteq \partial f(\cdot)/\partial x$ and $O(3)$ denotes 3rd and higher order terms. At time $j\delta t$, we have that

$$f_{i+1,j} = f_{i,j} + \delta x_{i+1} f'(x_i, t) + \frac{\delta x_{i+1}^2}{2} f''(x_i, t) + O(3)$$

$$f_{i-1,j} = f_{i,j} - \delta x_i f'(x_i, t) + \frac{\delta x_i^2}{2} f''(x_i, t) + O(3).$$

The first order spatial derivative of $f(\cdot)$ is then computed by subtracting $f_{i+1,j}$ from $f_{i-1,j}$, which gives

$$f'(x_i, t) = \frac{f_{i+1,j} - f_{i-1,j}}{\delta x_{i+1} + \delta x_i} + O(1).$$

Similarly, the second order derivative is obtained by adding $f_{i+1,j}$ and $f_{i-1,j}$:

$$f''(x_i, t) = 2 \frac{f_{i+1,j} - 2f_{i,j} + f_{i-1,j} - (\delta x_{i+1} - \delta x_i) f'(x_i, t)}{\delta x_{i+1}^2 + \delta x_i^2} + O(1).$$

Neglecting $O(1)$, we finally write

$$f'(x_i, t) = d_1(f_{i+1,j} - f_{i-1,j}) \tag{A.1}$$

$$f''(x_i, t) = d_2 f_{i+1,j} - d_3 f_{i,j} + d_4 f_{i-1,j} \tag{A.2}$$

with

$$d_1(i) = \frac{1}{\delta x_{i+1} + \delta x_i}, \quad d_2(i) = \frac{4\delta x_i}{(\delta x_{i+1}^2 + \delta x_i^2)(\delta x_{i+1} + \delta x_i)},$$

$$d_3(i) = \frac{4}{\delta x_{i+1}^2 + \delta x_i^2} \quad \text{and} \quad d_4(i) = \frac{4\delta x_{i+1}}{(\delta x_{i+1}^2 + \delta x_i^2)(\delta x_{i+1} + \delta x_i)}.$$

Note that the same formulas hold if the discretisation grid is time-varying.

Appendix A.2. Variable-step spatial integration

The spatial integration of $f(x, t)$ is performed based on the principle of Simpson's rule, which is to find a polynomial that fits the curve in three points. Such a polynomial is taken in Lagrange basis and writes as

$$P(x) = f_{i,j} \frac{x - x_{i+1}}{x_i - x_{i+1}} \frac{x - x_{i+2}}{x_i - x_{i+2}} + f_{i+1,j} \frac{x - x_i}{x_{i+1} - x_i} \frac{x - x_{i+2}}{x_{i+1} - x_{i+2}} + f_{i+2,j} \frac{x - x_i}{x_{i+2} - x_i} \frac{x - x_{i+1}}{x_{i+2} - x_{i+1}}.$$

The integral between two points x_i and x_{i+2} is then

$$\int_{x_i}^{x_{i+2}} f(x, t) dx \approx \int_{x_i}^{x_{i+2}} P(x) dx \\ \approx \frac{\delta x_{i+2} + \delta x_{i+1}}{6} \left[\frac{2\delta x_{i+1} - \delta x_{i+2}}{\delta x_{i+1}} f_{i,j} + \frac{(\delta x_{i+1} + \delta x_{i+2})^2}{\delta x_{i+1} \delta x_{i+2}} f_{i+1,j} + \frac{2\delta x_{i+2} - \delta x_{i+1}}{\delta x_{i+2}} f_{i+2,j} \right].$$

For the general case where the integration is carried out between the two locations x_m and x_n ,

$$\int_{x_m}^{x_n} f(x, t) dx \approx \sum_{k=0}^{\alpha_{int}-1} \int_{x_{m+2k}}^{x_{m+2k+2}} P(x) dx + \beta_{int} \frac{\delta x_n}{\delta x_n + \delta x_{n+1}} \int_{x_{n-1}}^{x_{n+1}} P(x) dx$$

where

$$\begin{cases} \alpha_{int} = (n - m)/2 & \text{and } \beta_{int} = 0 & \text{if } (n - m) \text{ is even,} \\ \alpha_{int} = (n - m - 1)/2 & \text{and } \beta_{int} = 1 & \text{if } (n - m) \text{ is odd.} \end{cases}$$

This integration method is particularly computationally efficient and useful from a control point of view since it allows to approximate the integral operator with a linear operator as

$$\int_0^{x_i} f(x, t) dt \approx M_{int}(i, 1 : i) \begin{bmatrix} f_{1,j} \\ \vdots \\ f_{i,j} \end{bmatrix}$$

where $M_{int} \in \mathbb{R}^{N \times N}$ is the integration matrix, constructed with the previous equations, and $M_{int}(i, 1 : i)$ denotes the columns 1 to i of row i .

Appendix A.3. Temporal differentiation

It is performed using an *implicit-explicit* scheme, as proposed in [33]. For the general case where the function to be discretised writes as $\dot{f}(x, t) = g(x, t)$, the time derivative $\dot{f}(\cdot)$ is obtained with

$$\left(\frac{f_{i,j+1} - f_{i,j}}{\delta t} \right) = h \left(\frac{f_{i,j+1} - f_{i,j}}{\delta t} \right)_{ex} + (1 - h) \left(\frac{f_{i,j+1} - f_{i,j}}{\delta t} \right)_{im} \quad (\text{A.3})$$

where $h \in [0, 1]$ and

$$\left(\frac{f_{i,j+1} - f_{i,j}}{\delta t} \right)_{ex} = g_{i,j}, \quad \left(\frac{f_{i,j+1} - f_{i,j}}{\delta t} \right)_{im} = g_{i,j+1}.$$

Note that for the special case of the diffusion equation, g typically depends on f' , f'' and the source terms. The temporal discretisation method described here corresponds to the Crank-Nicholson scheme if $h = 0.5$.

Appendix B. Gaussian distribution

The ECCD and LHCD systems generate distributed plasma current deposits, which are represented as Gaussian distribution. The general equation describing such a distribution is given by

$$j'_{ni}(x, t) = j_{ni}(x, t) \frac{\mu(t) - x}{\sigma(t)}$$

where, in the classical probabilistic terminology, $\mu(t)$ is the mean and $\sigma(t)$ is the variance of the function considered. Integrating the previous equation, we have

$$j_{ni}(x, t) = \vartheta(t) e^{-(\mu(t)-x)^2/2\sigma(t)}$$

where $\vartheta(t)$ sets the maximum value of $j_{ni}(x, t)$ (at $x = \mu$). A discretised version is obtained thanks to the central difference method as

$$\frac{j_{ni,i+1,j} - j_{ni,i-1,j}}{\delta x_{i+1} + \delta x_i} = j_{ni,i,j} \frac{\mu_j - x_i}{\sigma_j} \Leftrightarrow j_{ni,i+1,j} = (\delta x_{i+1} + \delta x_i) \frac{\mu_j - x_i}{\sigma_j} j_{ni,i,j} + j_{ni,i-1,j}$$

with the boundary conditions

$$j_{ni,1,j} = \vartheta_j e^{-\mu_j^2/2\sigma_j} \quad \text{and} \quad j_{ni,2,j} = \vartheta_j e^{-(\mu_j-x_2)^2/2\sigma_j}$$

for both CD systems.

Appendix C. Optimal fitting method

Given a set of experimental measurements and an appropriate fitting function, this section describes an optimal identification method to determine the fitting function parameters. Some proper references on numerical solutions by iterative search and gradient methods can be found in [57]. More specifically, a similar design method was used in [58] for the optimal control of systems with stochastic components in the dynamics. We consider here the steady state (time-invariant) behaviour of a physical quantity as a function described by a set of n_m measurements (i.e. the sampling times), which has to be large enough to ensure that the resulting fitting function represents the physical phenomena. The set of measured inputs is

$$\mathcal{I} = \{I_1, I_2, \dots, I_{n_i}\} \in \mathbb{R}^{n_m \times n_i}$$

where n_i is the number of physical quantities that influence the identified one, and the measured outputs are denoted by $y \in \mathbb{R}^{n_m}$. The estimated output is then

$$\hat{y}(\vartheta, i) = f(\mathcal{I}(i), \vartheta), \quad i = 1 \dots n_m$$

where $f(\cdot)$ is the fitting law, $\mathcal{I}(i)$ corresponds to the input measurements of the i^{th} experiment and ϑ is the vector of design parameters.

Appendix C.1. General formulation

A classical identification problem is to find ϑ that minimizes the difference between the measured and estimated data. This is done in this section by choosing a cost function J which reflects the variance of the estimation error from a given set of measurements:

$$J(\vartheta) = \frac{1}{n_m} \sum_{i=1}^{n_m} \|y(i) - \hat{y}(\vartheta, i)\|^2$$

The output error is then minimized for ϑ^* satisfying

$$\vartheta^* = \arg \min_{\vartheta} J(\vartheta)$$

This optimization problem can be solved with a descent algorithm, using the sensitivity of $\hat{y}(i)$ with respect to ϑ , expressed as $S(\vartheta, i) \doteq \partial \hat{y}(i) / \partial \vartheta$. The gradient writes as

$$\nabla J(\vartheta) = -\frac{2}{n_m} \sum_{i=1}^{n_m} (y(i) - \hat{y}(\vartheta, i)) S(\vartheta, i)$$

and the optimal parameter ϑ^* is obtained by moving along the steepest slope $-\nabla J(\vartheta)$ with a step α , which has to be small enough to ensure that $\dot{\vartheta} = -\alpha \nabla J(\vartheta)$ converges to ϑ^* . This step is chosen according to *Newton's method* and writes as $\alpha \doteq (\Psi J(\vartheta) + \nu I)^{-1}$, where ν is a positive constant introduced to ensure strict positiveness and $\Psi J(\vartheta)$ is the pseudo-Hessian, derived using the Gauss-Newton approximation as

$$\Psi J(\vartheta) = \frac{2}{n_m} \sum_{i=1}^{n_m} S(\vartheta, i) S(\vartheta, i)^T$$

The optimal set of fitting parameters is finally obtained with the variation law

$$\vartheta_{l+1} = \vartheta_l - \alpha_l \nabla J(\vartheta_l) \tag{C.1}$$

$$\alpha_l = (\Psi J(\vartheta_l) + \nu I)^{-1} \tag{C.2}$$

for l sufficiently large.

Remark 4 *The convergence speed of the algorithm is inversely proportional to the design parameter ν but choosing this parameter too small may create some oscillations in the algorithm.*

Appendix C.2. Linear regression

The previous method is particularly efficient when the output is estimated with a linear regression technique. Indeed, in that case we can write $\hat{y}(\vartheta, i) = f(\mathcal{I}(i)) \times \vartheta$, $i = 1 \dots n_m$, and the sensitivity function is simplified as

$$S(\vartheta, i) = S(i) = f(\mathcal{I}(i)) \tag{C.3}$$

Consequently, the pseudo-Hessian function ΨJ and α do not depend on the design parameters. A commonly used fitting function is given by

$$\hat{O} = \alpha_0 I_1^{\alpha_1} I_2^{\alpha_2} I_3^{\alpha_3} \dots I_{n_i}^{\alpha_{n_i}}$$

The linear regression is then performed with the output

$$\begin{cases} y = \ln(O) \\ \hat{y}(\vartheta) = \ln(\alpha_0) + \alpha_1 \ln(I_1) + \alpha_2 \ln(I_2) + \dots + \alpha_{n_i} \ln(I_{n_i}) \end{cases}$$

where O is the measured output, and the previous algorithm is applied with

$$\begin{aligned} \alpha &= [\ln(\alpha_0) \quad \alpha_1 \quad \alpha_2 \quad \dots \quad \alpha_{n_i}]^T \\ f(\mathcal{I}) &= [1_{n_m} \quad \ln(I_1) \quad \ln(I_2) \quad \dots \quad \ln(I_{n_i})] \end{aligned} \tag{C.4}$$

where 1_{n_m} is a column vector of n_m ones.

Appendix C.3. LH deposit estimation

The proposed method is applied to the estimation of the lower hybrid current deposit width W_x with the fitting function (with 6 parameters)

$$\hat{w}_{hxr} = \alpha_0 B_{\phi_0}^{\alpha_1} I_p^{\alpha_2} \bar{n}^{\alpha_3} P_{LH}^{\alpha_4} N_{\parallel}^{\alpha_5}$$

The optimal parameter vector is computed from the variation law (C.1)-(C.2) with the sensitivity function (C.3)-(C.4). A set of 111 averaged measurements, performed on Tore Supra shots ranging between the shot numbers 34496 and 36165, determines the values of \mathcal{J} and O . This optimal parameter determination method is also applied to estimate the centre of the deposit profile (radial position of the maximum value) and provide for the coefficients $\alpha_0, \dots, \alpha_5$ of the relationship

$$\hat{\mu}_{hxr} = \alpha'_0 B_{\phi_0}^{\alpha'_1} I_p^{\alpha'_2} \bar{n}^{\alpha'_3} P_{LH}^{\alpha'_4} N_{\parallel}^{\alpha'_5}.$$

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