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Optical determination of viscoelastic properties of nematic OHMBBA

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Résumé. — Nous avons mesuré des paramètres viscoélastiques du nématique OHMBBA en fonction de la température. Nos expériences se basent sur la technique homodyne avec laquelle on peut détecter la densité spectrale de la lumière laser diffusée par des cristaux liquides. On peut décrire le coefficient de la viscosité de torsion en fonction de la température, du paramètre d'ordre et d'une énergie d'activation. Nous obtenons le rapport entre les constantes élastiques de divergence et de torsion par deux méthodes : 1) en déterminant la section efficace de diffusion en fonction du vecteur d'onde de diffusion et 2) en faisant une analyse de la densité spectrale dans le mode mélangé (torsion plus divergence). Les résultats obtenus avec ces deux méthodes concordent, mais ils diffèrent des résultats obtenus avec la technique de Freedericksz. Nous discutons ce désaccord brièvement.

Abstract. — Experimental values are reported for the splay/twist viscoelastic ratios of OHMBBA in the nematic region as a function of temperature. In the experiments the homodyne self-beat technique was used to detect noise intensity spectra of laser light scattered by the nematic liquid crystal. The measured rotational viscosity can be described as a function of the temperature, the order parameter and an activation energy. The splay/twist ratio of the elastic constants was determined by measuring the scattered cross section as a function of the scattering wave vector and by making a noise analysis in the mixture region. The results obtained with each method are in agreement, but differ from Freedericksz transition data. This discrepancy is discussed.

1. Introduction. — Light scattered by local director fluctuations of an aligned nematic liquid crystal (NLC) yields information about the viscoelastic properties of that crystal [1, 2, 3]. In this paper we describe light scattering experiments on OHMBBA, which produce data about the splay/twist elastic ratio and the splay and the twist viscoelastic ratios.

To our knowledge no viscosity data have been published so far. However, we were able to compare values for the elastic constants with those obtained from measurements of Freedericksz transitions [4].

OHMBBA (o-hydroxy-p-methoxybenzylidene-p'butylaniline) has the following molecular structure :



Its nematic range is from $T_{SN} = 44$ °C to $T_{NI} = 64.6$ °C at 1 atm.

The splay/twist viscoelastic ratios were obtained from the line broadening of the scattered laser light, caused by orientational fluctuations of the director [5].

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These ratios were determined as a function of temperature in the entire nematic range and at 1 atm. pressure. In addition it seemed worthwhile to study the dependence of these ratios on orientational order, since the literature data on this subject are ambiguous [6, 7]. From our measurements we could also determine the total scattering cross section, from which in turn we found the splay/twist curvature elastic constants. These ratios were also determined from noise measurements done in the mixture region, where a mixture of splay and twist distortion fluctuations can be observed. In this region the splay/twist mixture component dominates over the pure splay and pure twist component. In the so-called mixture mode the splay/twist mixture component is at its maximum at a specific scattering angle, θ_{mix} , which can be determined. Since θ_{mix} is a function of well-known optical parameters and the splay/twist elastic ratio, the latter can be determined by measuring θ_{mix} . In the theory of light scattering in nematics it is tacitly assumed that the sample dimensions are very large with respect to the wavelength of light. In this paper, however, the dimensions of the scattering volume are taken to be finite.

2. Experimental arrangement for the investigation of scattered light. — The experimental arrangement, shown in figure 1, is a normal homodyne self-beat set-up, which is strictly the same as that used by van Eck et al. [8]. See their paper for a detailed description. The light source is a 5 mW He-Ne laser ($\lambda_0 = 632.8$ nm, Spectra Physics model 120). The unfocussed light beam has a cross section of 1 mm². The scattered light is detected by a photomultiplier tube (PMT) placed about 0.50 m from the scattering centre. The set-up is placed in a darkened room, and with the help of a set of diaphragms, the detection of stray-light is avoided. Since the diaphragm in front of the PMT has a diameter of 4 mm, the solid angle of observation has a constant value of about 5×10^{-5} sterad. The fluctuating anode current of the PMT is fed into a real-time frequency analyser (Brüel and Kjaer, type 3347), which displays the noise spectrum in the frequency range 12.5 Hz to 63 kHz.



Fig. 1. — Experimental set-up.

The sample we used contained OHMBBA which was planar orientated simply by rubbing the glass walls of the sample. The space between the glass walls was 50 µm and was maintained by tungsten ribbon and a special epoxy resin (Lekutherm E 320). The sample was placed between heating stages (Mettler PF 52), which kept the temperature constant within 0.01 °C. The sample temperature was not influenced by absorption of laser light. This was ascertained by varying the intensity of the light source and by measuring the influence of the light scattering exactly in the nematicisotropic transition region. No change in the scattering pattern was observed.

The laboratory scattering angle, $\theta_{\rm L}$, i.e. the angle outside the scattering medium, could be varied between 0° and 30°. The polarization vectors i and f of the incoming and detected scattered light respectively could be chosen at will by means of a polarizer and analyser. Appropriate choices for i and f with respect to the orientation of the NLC made it possible for us to measure pure splay and pure twist effects [8]. The configuration we used is shown in figure 2.



Fig. 2. — Scattering diagram of the experimental configuration for splay/twist-mode detection.

Fourier cosine transform of the auto-correlation function of the detected electric field [2]. This autocorrelation function in turn is proportional to the following auto-correlation function

$$A(\mathbf{q}, t) = \langle \delta \varepsilon_{if}^{*}(\mathbf{q}, 0) \, \delta \varepsilon_{if}(\mathbf{q}, t) \rangle, \qquad (1)$$

where

$$\delta \varepsilon_{if}(\mathbf{q}, t) = \mathbf{f} \cdot \delta \varepsilon(\mathbf{q}, t) \cdot \mathbf{i}$$

with i and f the unit vectors marking the directions of polarization of the incoming and scattered laser light respectively. The vector **q** is the scattering wave vector, i.e. $\mathbf{q} = \mathbf{k}_i - \mathbf{k}_f$ (see Fig. 2). The tensor $\delta \boldsymbol{\varepsilon}(\mathbf{q}, t)$ is given by

$$\delta \boldsymbol{\varepsilon}(\mathbf{q}, t) = \frac{1}{V} \int_{V} \mathrm{d}\mathbf{r} \, \mathrm{e}^{i\mathbf{q}\cdot\mathbf{r}} \, \delta \boldsymbol{\varepsilon}(\mathbf{r}, t) \,, \tag{2}$$

where $\delta \varepsilon(\mathbf{r}, t)$ is the local fluctuation of the dielectric tensor with respect to the average thermal equilibrium value ε_0 and V is the scattering volume.

The mean orientation of the rod-like molecules, called the director, is given by the unit vector \mathbf{n}_0 . The frame of reference we have chosen is shown in figure 2; for our configuration we defined the director of the NLC as :

$$\mathbf{n}_0 = (0, 0, n_0),$$

where average values are denoted by the subscript 0. Assuming that fluctuations around \mathbf{n}_0 are small, we have in first order :

$$\delta n_z(\mathbf{r}, t) = 0$$

and for i = x, y:

$$\mathbf{n}_i(\mathbf{r}, t) = \delta \mathbf{n}_i(\mathbf{r}, t)$$
.

For our configuration we now have

$$\delta \varepsilon(\mathbf{q}, t) = \Delta \varepsilon \begin{pmatrix} 0 & 0 & \delta n_x(\mathbf{q}, t) \\ 0 & 0 & \delta n_y(\mathbf{q}, t) \\ \delta n_x(\mathbf{q}, t) & \delta n_y(\mathbf{q}, t) & 0 \end{pmatrix}, (3)$$

where

$$\delta \mathbf{n}(\mathbf{q}, t) = \frac{1}{V} \int_{V} \mathrm{d}\mathbf{r} \, \mathrm{e}^{i\mathbf{q}\cdot\mathbf{r}} \, \delta \mathbf{n}(\mathbf{r}, t) \,, \tag{4}$$

3. Theory. - 3.1 LIGHT SCATTERING BY NLC. - and $\Delta \varepsilon = \varepsilon_{\parallel} - \varepsilon_{\perp}$; ε_{\parallel} and ε_{\perp} are the dielectric cons-The optical spectrum of the scattered light is the tants for electric fields directed parallel and perpendicular to \mathbf{n}_0 respectively. Hence we get for equation (1) :

$$A(\mathbf{q}, t) = (\Delta \varepsilon)^2 \left\{ G_x^2 \left\langle \delta n_x(\mathbf{q}, t) \, \delta n_x^*(\mathbf{q}, 0) \right\rangle + G_y^2 \left\langle \delta n_y(\mathbf{q}, t) \, \delta n_y^*(\mathbf{q}, 0) \right\rangle \right\}, \quad (5)$$

where

$$G_{\alpha} \equiv f_{\alpha} i_{z} + i_{\alpha} f_{z} \qquad (\alpha = x, y).$$
 (6)

The quantity G_{α} is called an optical geometric factor. Thus the optical spectrum is directly related to the auto-correlation function of $\mathbf{n}(\mathbf{q}, t)$.

3.1.1 Finite dimensions of the scattering volume. — Because in our experiment the position of the director was fixed at the glass walls we can express the fluctuations of the local director as follows :

$$\delta \mathbf{n}(\mathbf{r}, t) = \frac{1}{2} \sum_{m} \left(\delta \mathbf{n}_m(t) \right)_0 e^{i\mathbf{k}_m \cdot \mathbf{r}}, \qquad (7)$$

with

$$(k_i)_m = m \frac{\pi}{d_i}$$
 $(i = x, y, z)$. (8)

These relations hold because of the boundary conditions. The term d_i is the size of the sample in the i = x, yor z direction. In these light scattering experiments the scattering wave vector \mathbf{q} is related to the wave vector \mathbf{k}_m , as will be shown.

Although \mathbf{k}_m has discrete values, the intensity of the scattered light is a continuous function of the scattering angle; this is because the dimensions of the scattering volume are finite. Therefore we shall extend the light scattering analysis by taking the finite dimensions of the sample into account. When we substitute equation (7) into (4) we get :

$$\delta \mathbf{n}(\mathbf{q}, t) = \frac{1}{V} \frac{1}{2} \sum_{m} (\delta \mathbf{n}_{m}(t))_{0} \int_{V} d\mathbf{r} e^{i(\mathbf{q} - \mathbf{k}_{m}) \cdot \mathbf{r}} .$$
 (9)

The integral can be written as a product of three integrals :

$$\frac{1}{V} \int_{V} d\mathbf{r} \ e^{i(\mathbf{q} - \mathbf{k}_{m}) \cdot \mathbf{r}} = \frac{1}{x_{0}} \int_{-\frac{1}{2}x_{0}}^{\frac{1}{2}x_{0}} dx \ e^{i(q_{x} - (k_{x})_{m}) \cdot x} \times \\ \times \frac{1}{y_{0}} \int_{-\frac{1}{2}y_{0}}^{\frac{1}{2}y_{0}} dy \ e^{i(q_{y} - (k_{y})_{m}) \cdot y} \\ \times \frac{1}{z_{0}} \int_{-\frac{1}{2}z_{0}}^{\frac{1}{2}z_{0}} dz \ e^{i(q_{z} - (k_{z})_{m}) \cdot z},$$

where x_0 , y_0 and z_0 are the sizes of the scattering volume. For our sample, where $y_0 \approx z_0 \approx 1$ mm it holds that $y_0, z_0 \gg \lambda_0$. Hence we can write

$$\frac{1}{y_0} \int_{-\frac{1}{2}y_0}^{\frac{1}{2}y_0} dy \ e^{i(q_y - (k_y)_m).y} \times \frac{1}{z_0} \int_{-\frac{1}{2}z_0}^{\frac{1}{2}z_0} dz \ e^{i(q_x - (k_x)_m).z} = \\ = \delta_{q_{y_0}(k_y)_m} \cdot \delta_{q_{x_0}(k_x)_m},$$

where $\delta_{i,j}$ denotes the Kronecker symbol. The thickness of the scattering volume $x_0 = d_x = 50 \ \mu m$ is nevertheless large compared to λ_0 , but too small for the x-th component of the integral to be considered as a delta function. However, because $d_v = 1$ cm and $d_z = 3$ cm the spacings of $(k_y)_m$ and $(k_z)_m$ are too small to be resolved by our experimental set-up. Unlike $(k_x)_m$, which can only have discrete values, as is shown in figure 3, $(k_y)_m$ and $(k_z)_m$ were taken as varying continuously.



Fig. 3. — Example of a plot for comparing $(k_x)_m$, q_x and the scattering angle θ for $n_{\perp} = 1.5$ and $n_{\parallel} = 1.7$.

Hence,

$$\frac{1}{V} \cdot \int_{V} \mathbf{d\mathbf{r}} \, \mathrm{e}^{i(\mathbf{q}-\mathbf{k}_{m})\cdot\mathbf{r}} = \left\{ \frac{\sin\left(\frac{1}{2} \, x_{0} \left(q_{x} - \left(k_{x}\right)_{m}\right)\right)}{\frac{1}{2} \, x_{0} \left(q_{x} - \left(k_{x}\right)_{m}\right)} \right\} \times \delta_{q_{y},\left(k_{y}\right)_{m}} \cdot \delta_{q_{x},\left(k_{x}\right)_{m}}$$

Using this result equation (9) becomes :

$$\delta \mathbf{n}(\mathbf{q}, t) = \sum_{m} \delta \mathbf{n}_{(k_{x})m, q_{y}, q_{z}}(t) \left\{ \frac{\sin\left(\frac{1}{2} x_{0}(q_{x} - (k_{x})_{m})\right)}{\frac{1}{2} x_{0}(q_{x} - (k_{x})_{m})} \right\}.$$
(10)

This means that $\delta n(q, t)$ is the summation over all $\delta \mathbf{n}((k_x)_m, q_y, q_z; t)$ weighted by the function

$$\left\{\frac{\sin\left(\frac{1}{2}x_0(q_x-(k_x)_m)\right)}{\frac{1}{2}x_0(q_x-(k_x)_m)}\right\},\,$$

which has a maximum at $(k_x)_m = q_x$. The viscoelastic data can be determined from the relaxation times of the NLC, which in turn follow from the auto-correlation function $\langle \mathbf{n}_{\mathbf{k}_{m}}(t) \mathbf{n}_{\mathbf{k}_{m}}(0) \rangle$, as will be demonstrated later. In our light experiments, however, we measure quantities related to $\langle \mathbf{n}(\mathbf{q}, t) \mathbf{n}(\mathbf{q}, 0) \rangle$. Equation (10) provides a link between the measured quantities and the calculated ones.

If the finite dimensions of the scattering volume are taken into account in the case of cross-section measurements we obtain values which differ by 2-3% from those found when we neglected the finite dimensions, i.e.

$$\delta \mathbf{n}(\mathbf{q}, t) = \delta \mathbf{n}_{\mathbf{k}_{m}}(t)$$
.

3.1.2 Relation between the fluctuations of the director and the scattering cross section. - The kinetic properties of the director are characterized by the viscoelastic ratios of the NLC. Information about these properties can be obtained from the spectral intensity of the fluctuations in the scattered light intensity. If one takes as an orthonormal base \mathbf{e}_1 , \mathbf{e}_2 , \mathbf{e}_3 , where

$$\mathbf{e}_3 \equiv \mathbf{n}_0, \mathbf{e}_2 \perp (\mathbf{k}_m, \mathbf{n}_0) \text{ and } \mathbf{e}_1 \perp (\mathbf{e}_2, \mathbf{e}_3),$$

then the expression for the free energy becomes quadratic in $\delta \mathbf{n}_{\mathbf{k}_m}$ [9]. Therefore the equipartition theorem holds for every degree of freedom. In our case, according to the configuration of figure 2 where $q_z = 0$ because $\mathbf{q} \perp \mathbf{n}_0$, the variance becomes [1]:

$$\langle \left| \left(\delta n_{(k_x,k_y,0)_m} \right)_{\alpha} \right|^2 \rangle = \frac{k_{\rm B} T}{V'(K_{\alpha} \, k_m^2)}, \qquad (11)$$

where

$$k_m^2 = (k_x)_m^2 + (k_y)_m^2 = (k_1)_m^2 + (k_2)_m^2$$

and where $\alpha = 1, 2$ according to the orthonormal base (e_1, e_2, e_3) . K_1 and K_2 correspond to the Frank elastic constants associated with splay and twist respectively. The term k_B is the Boltzmann constant, T the temperature and V' the sample volume.

The differential scattering cross section per solid angle can be written in terms of the auto-correlation function A as follows [10] :

$$\frac{\mathrm{d}\,\sigma}{\mathrm{d}\Omega} \sim A(\mathbf{q},0)\,. \tag{12}$$

Hence if we put the results of (10) and (11) into (5) we have :

$$\frac{\mathrm{d}\sigma}{\mathrm{d}\Omega} \sim \sum_{m} \sum_{\alpha=1,2} \left| \langle \left| \left(\delta n_{(k_{\alpha})m,q_{y},0} \right)_{\alpha} \right|^{2} \rangle \times \right. \\ \left. \times \left\{ \frac{\sin^{2} \left(\frac{1}{2} x_{0} (q_{\alpha} - (k_{\alpha})_{m}) \right)}{\frac{1}{2} x_{0} (q_{\alpha} - (k_{\alpha})_{m})} \right\} \times \left. G_{\alpha}^{2} \right|, \qquad (13)$$

where the indices $\alpha = 1$, 2 refer to the base (\mathbf{e}_1 , \mathbf{e}_2 , \mathbf{e}_3). Note that this base depends on \mathbf{k}_m . As a consequence the summation symbols in equation (13) cannot be exchanged. In order to simplify the mathematics, however, we define only one base (\mathbf{e}_1 , \mathbf{e}_2 , \mathbf{e}_3) related to \mathbf{q} instead of to \mathbf{k}_m and then the summation symbols can be exchanged. Now we can split (13) into two parts, each with its own summation. The splitting procedure will introduce an error into the calculations of K_{α} is much smaller than 1 %. So in our experiments we can neglect this error and we can base (\mathbf{e}_1 , \mathbf{e}_2 , \mathbf{e}_3) on \mathbf{q} and \mathbf{n}_0 . We shall give more details about the calculations of K_{α} in section 3.1.3.

3.1.3 Determination of the splay/twist elastic ratio by differential cross section measurements. — In section 3.1.2 we have given the relation between the scattering cross section and the elastic constants. It follows from (11) that

$$\langle | (\delta n_{(k_x)_m, q_y, 0})_{\alpha} |^2 \rangle = \frac{k_{\rm B} T}{V'} \frac{1}{K_{\alpha}((k_x)_m^2 + q_y^2)}.$$
 (14)

Because the mean intensity $I(\mathbf{q})$ of light scattered at the angle θ is proportional to $d\sigma/d\Omega$ we may write for (13) :

$$I(\mathbf{q}) \sim Q(\mathbf{q}) \cdot \left(\sum_{\alpha=1,2} \frac{G_{\alpha}^2}{K_{\alpha}}\right),$$

where

$$Q(\mathbf{q}) \equiv \sum_{m} \left\{ \frac{1}{((k_{x})_{m}^{2} + q_{y}^{2})} \right\} \times \left\{ \frac{\sin\left(\frac{1}{2} x_{0}(q_{y} - (k_{x})_{m})\right)}{\frac{1}{2} x_{0}(q_{y} - (k_{x})_{m})} \right\}^{2}.$$
 (15)

The factor $Q(\mathbf{q})$ can be calculated numerically for each \mathbf{q} . By varying θ the well-known geometric factor G_{α}^2 changes and measurements of $I(\mathbf{q})$ allow us to determine the ratio K_1/K_2 .

Note that it is sufficient to measure only the relative change of I as a function of the scattering angle. Hence the absolute value of I is not needed.

3.1.4 Determination of the viscoelastic properties from spectral noise analysis. — The expression for the noise intensity spectrum of the scattered light obtained using our self-beat technique is given by the convolution integral of the spectrum of the scattered electric field; this expression holds if the field fluctuations are Gaussian [2]. The spectrum of the scattered electric field consists of two Lorentzians, i.e. one due to the splay deformation and the other to the twist deformation. In our configuration (see Fig. 2) we shall not measure the bend deformation, but only the splay and twist deformation [2]. Therefore, for the noise intensity spectrum of the scattered light we get

$$S_{\Delta I}(\omega, \mathbf{q}) = G_1^4 \frac{(2 \Delta \omega_1)}{K_1^2 q^2 (\omega^2 + (2 \Delta \omega_1)^2)} + \\ \ll \text{ splay } \rangle$$

+ $2 G_1^2 G_2^2 \frac{(\Delta \omega_1 + \Delta \omega_2)}{K_1 K_2 q^2 (\omega^2 + (\Delta \omega_1 + \Delta \omega_2)^2)} \\ \ll \text{ splay/twist mixture } \rangle$

+
$$G_2^{4} \frac{(2 \Delta \omega_2)}{K_2^2 q^2 (\omega^2 + (2 \Delta \omega_2)^2)}$$
. (16)
 $\ll \text{ twist } \gg$

This spectrum consists of three Lorentzians, weighted by functions of $G_{\alpha}^2/K_{\alpha} q$ ($\alpha = 1, 2$). Fortunately G_1 tends to zero for small scattering angles ($\theta \leq 5^{\circ}$) and only the twist term remains, while for angles $\theta > 20^{\circ}$, G_2 can be neglected and the splay term dominates. So in each of these two cases we have only one Lorentzian with a half-bandwidth $\Delta \omega_{1/2} = 2 \Delta \omega_{\alpha}$ ($\alpha = 1$, splay; $\alpha = 2$, twist), where according to the slow mode expression $u_{s_{\alpha}}$ from [1]:

$$\Delta \omega_{\alpha} \equiv u_{s_{\alpha}} = \frac{K_{\alpha} q^2}{\eta_{\alpha}}.$$
 (17)

The spectrum also consists of a fast mode term [1]. This fast mode is associated with a diffusion of vorticity. The half-bandwidth $u_{s_{\rm F}}$, however, is of the order of $10^9 \, {\rm s}^{-1}$ and the contribution of the fast mode is much smaller than that of the slow mode, so we can neglect this term.

From equation (17) it follows that if we plot $\frac{1}{2}(\Delta \omega_{1/2})_{exp}$ versus q^2 we expect straight lines with a gradient equal to the viscoelastic ratios. The scattering wave vector can be varied by varying the scattering angle θ (see Fig. 2).

In fact equation (16) should contain summation over \mathbf{k}_m , as was pointed out in section 3.1.2, but in our case the error introduced by using equation (16) is small with respect to the experimental error of about 5 %.

3.1.5 Determination of the splay/twist elastic ratio from the mixture mode. — Another way of deriving K_1/K_2 is to determine the scattering vector **q** where the mixture contribution is at its maximum. In this case the contribution of the splay and the twist terms are equal and the bandwidth of the mixture mode is the mean of the splay and twist mode bandwidths, i.e.

$$(\Delta \omega_{1/2})_{\text{exp.,mixmode}} = \sum_{\alpha=1,2} \Delta \omega_{\alpha}. \quad (18)$$

Because $\Delta\omega_1$ and $\Delta\omega_2$ can be measured separately, as was explained in section 3.1.3, we can calculate $(\Delta\omega_{1/2})_{\text{mixmode}}$ and find out at what **q** this value equals $(\Delta\omega)_{\text{exp}}$. When the mixture mode contribution at its maximum

$$\frac{G_1^2}{K_1} = \frac{G_2^2}{K_2}.$$
 (19)

Hence from a measurement of q_{mix} there follows the corresponding scattering angle θ , which in turn gives G_1 and G_2 . The ratio K_1/K_2 can then be calculated with the help of equation (19). The advantage of this method is that the data are obtained from noise measurements which do not contain the typical experimental errors associated with measurements of the angular distribution of scattered light.

3.1.6 Corrections in the case of light scattering experiments on flat samples. — In our set-up involving light scattered by birefringent material the scattered light is refracted as it leaves the NLC, according to Snell's law, i.e. $\sin \theta_L = n \cdot \sin \theta \cdot \theta$ and θ_L are the scattering angles inside and outside the medium respectively; *n* is the refractive index, which, in the case of birefringent material like NLC, is angular dependent, i.e. $n = n(\theta)$. In angular dependent light scattering investigations one has to take absorption effects and multiple scattering into account. Furthermore the measured data have to be corrected, as is described below.

i) As the scattered light leaves the NLC, part of it will be reflected and the amount of light will depend on the scattering angle and the direction of polarization. The transmissivity is based on the Fresnel formulae [11] which have to be used to calculate the original scattered light intensity.

ii) Because the detector area is finite and at a constant distance from the scattering volume, one samples within a solid angle $d\Omega_L$ with fixed dimensions. The relation between the solid angle outside and inside the medium, $d\Omega_L$ and $d\Omega$, respectively is given by Chatelain [12] :

$$\mathrm{d}\Omega_{\mathrm{L}} = n^2 \, \frac{\cos\theta}{\cos\theta_{\mathrm{L}}} \, \mathrm{d}\Omega \; . \tag{20}$$

iii) The measured anode current is proportional to the intensity of the scattered light and hence to the differential cross section, i.e. $d\sigma/d\Omega_L$, from which $d\sigma/d\Omega$ can be determined according to equation (20). For the cross section, measured within the solid angle $d\Omega$, one can write :

$$\mathrm{d}\,\sigma \sim \int_{\alpha_{\mathrm{dq}}} \int A(\mathbf{q},0) \,\mathrm{d}\mathbf{q} \simeq A(\mathbf{q},0) \cdot \alpha_{\mathrm{dq}},$$

where α is the area in **q**-space, consisting of all possible points representating all possible scattering vectors **q**. The subscript **dq** denotes that we have taken a finite area around **q**, which has size **dq** and corresponds to $d\Omega$. One can easily prove that $\alpha_{dp} = \frac{1}{\lambda_0^2} n^2 d\Omega$, hence

$$\frac{\mathrm{d}\sigma}{\mathrm{d}\Omega} \sim \frac{1}{\lambda_0^2} n^2 A(\mathbf{q}, 0) \,. \tag{21}$$

It should be noted that when the refractive index is angular-dependent, equation (21) has to be taken into account.

3.2 THE DISTORTION VISCOSITY AS A FUNCTION OF TEMPERATURE. — Experimental values for static physical quantities of NLC seem to be in reasonable agreement with theoretical values. Very few data on the dynamical physical quantities are available and comparisons with theory are rare.

3.2.1 Relations between the splay and twist viscosities and the Leslie coefficients. — The viscous properties of NLC are described by six so-called Leslie coefficients [13]. The Orsay-group [1] derived the following expressions for the splay (η_1) and twist (η_2) viscosities in terms of the Leslie coefficients :

$$\eta_1 = \gamma_1 - \alpha_3^2 / \eta_b$$
 and $\eta_2 = \gamma_1$,

where $\gamma_1 = \alpha_3 - \alpha_2$ is the rotational viscosity and $\eta_b = \frac{1}{2} (\alpha_3 + \alpha_4 + \alpha_6)$ is a Miesowicz constant. Although the Leslie coefficients may be negative, the viscosities such as η_1 , η_2 , η_b and γ_1 must always be positive. Hence we can write :

$$\frac{\eta_1}{\eta_2} = 1 - \frac{\alpha_3^2}{\eta_b \cdot \gamma_1} \le 1.$$
 (22)

From investigations on MBBA [14] and DIBAB [15] it is concluded that α_3 is very small compared to η_b and γ_1 . Therefore $\eta_1 \approx \eta_2$.

From our experiments we derive the ratios η_1/K_1 , η_2/K_2 and K_1/K_2 . Hence from these data we are able to determine the ratio η_1/η_2 and compare this with equation (22).

3.2.2 The viscoelastic ratio as a function of temperature and ordering. — The elastic and the viscosity constants are expected to depend on the state of alignment of the rod-like molecules of the NLC [16]. The state of alignment can be given by an order parameter S, defined by $S \equiv \frac{3}{2} \langle \cos^2 \theta \rangle - \frac{1}{2}$, where θ is the angle between the elongated axis of a molecule and the director. As shown in the literature [17, 18] the anisotropy of the mass susceptibility, i.e. $\Delta \chi^{g}$, is linear with this order parameter S, i.e.

$$\Delta \chi^{\mathbf{g}} \equiv \frac{(\chi_{\parallel} - \chi_{\perp})}{\rho} = c.S. \qquad (23)$$

Here χ_{\parallel} and χ_{\perp} are the magnetic susceptibility constants for magnetic fields parallel and perpendicular to \mathbf{n}_0 respectively. If $\Delta \chi^{\mathbf{g}}$ is measured as a function of temperature one finds S as a function of temperature [19]. The elastic as well as the viscosity constants also depend on the order parameter S. Several authors [19-21] have concluded from calculations and measurements that for nematics the Frank elastic constants are proportional to S^2 . Hence $K_a \approx c_a \cdot S^2$ $(\alpha = 1, 2 \text{ or } 3, \text{ representing splay, twist or bend respec-}$ tively), where c_{α} is a constant that depends only on molecular properties. Martins and Diogo [7] derived that S was dependent on the rotational viscosity. Unfortunately there have been very few investigations on the dynamical quantities of NLC. By measuring η_1 and η_2 as a function of temperature and by measuring the temperature dependence of S, one can also determine the S dependences of η_1 and η_2 and compare them with the theoretical relation.

Results reported by several authors [6, 7, 14, 22] let us consider a phenomenological relation for the twist viscosity coefficient :

$$\eta_2 = \gamma_1 = S^{\beta} \cdot e^{\varepsilon(S)/kT} \qquad (\beta \gtrsim 0) \,. \tag{24}$$

The exponential factor is quite a usual one for normal or isotropic liquids [23]. The energy term $\alpha(S)$ is the so-called activation energy for one particle. We can assume that $\alpha(S)$ is proportional to S according to the mean field theory [24], i.e. $\alpha(S) = \varepsilon_0 S$ [7]. In spite of this, several authors [6, 14] find that $\epsilon(S)$ is independent of S, i.e. $\epsilon(S) = \epsilon_0$. They consider ϵ as an activation energy for the rotation of a molecule around an axis perpendicular to the long axis of the molecule. In other words, if $\epsilon = \epsilon_0 S$, then this activation energy is due to collective interaction effects. On the other hand, if $\epsilon = \epsilon_0$, this energy is only related to individual effects of the molecules.

4. Experimental results. — For typical plots of experimental results which we derived with the help of our experimental arrangement, we refer to papers recently published by van Eck and Zijlstra [2, 25]. Our experimental investigations have led us to conclude that absorption effects and multiple scattering need not be taken into account because they are negligible. It has been verified that the observed scattered light is due only to director-fluctuations. This was done by measuring light scattered by the same sample but at a temperature above the clearing temperature $T_{\rm NI}$. In this case the observed detector current is not due to light scattering caused by director-fluctuations but is caused by density fluctuations, reflection effects, or dark current. It turns out that in this case the measured anode current is smaller than 0.001 of the anode current caused by scattering by crystals in the nematic phase. It should be noted that we worked with crossed polarizers.

Because the dimensions of the solid angle of observation are not infinitely small one measures in fact over a certain distribution of scattering angles. We have calculated, however, that the ensuing systematic error is much smaller than the experimental errors, so it can be neglected.

Table I shows the measured data for the splay/twist viscoelastic ratios at different temperatures, obtained from noise measurements. In this table data are also given for the splay/twist elastic ratios obtained from light intensity measurements and from noise measurements in the mixture mode.

4.1 VISCOELASTICITY. — The viscoelastic ratios are derived using the methods outlined in section 3.1.4. The scattering angle θ_L was varied between 5° and 25° so that only homodyne data were measured, which were not influenced by any heterodyne mixing. Heterodyne mixing will occur when the detected light mixes with the original laser light. Van Eck et al. [8] showed that this occurred for scattering angles of less than 3°. To be convinced that in a homodyne set-up the results are not influenced by any heterodyne mixing effects one can compare these results with the results from a pure heterodyne set-up. Because the bandwidth of a pure homodyne spectrum must differ from the bandwidth of the heterodyne spectrum by a factor 2 one is able to assess the purity of the homodyne spectrum. We did this by making use of the same heterodyne set-up as was used and described by van Eck and Zijlstra [2] (cf. Figs. 3 and 4 of [2]). We found

Table I. — The measured values of the splay (1) and the twist (2) viscoelastic ratios and the splay/twist elastic ratios of OHMBBA.

where

$T/T_{\rm NI}$	η_1/K_1 × 10 ⁹ sm ⁻²	$\frac{\eta_2/K_2}{\times 10^9 \text{ sm}^{-2}}$	$(K_1/K_2)_{c}$
0.990 5	6.41 + 0.12	11.8 + 0.7	1.88 +
0.987 0		13.3 ± 1.0	
0.985 0		_	1.90 ±
0.977 1	7.04 ± 0.15	14.1 ± 0.5	2.02 ±
0.970 0	7.35 ± 0.20	17.2 ± 1.5	2.06 ±
0.962 0	8.05 ± 0.25	20.0 ± 1.0	2.04 ±
0.9550	9.8 ± 0.5	21.1 ± 0.5	1.94 <u>+</u>
0.948 0	9.6 ± 0.3	23.5 ± 0.5	1.99 ±
0.940 6	10.8 ± 0.2	26.0 ± 1.5	2.09 ±
0.932 4	12.5 \pm 0.3	32.3 ± 1.0	$2.02 \pm$



Fig. 4. — Example of a log-log plot of the measured values of $\Delta \omega_{exp}$ versus q^2 for $T/T_{NI} = 0.9905$. Because

 $\Delta\omega_{\rm exp} = 2 \Delta\omega_{\alpha} = 2(K_{\alpha}/\eta_{\alpha}) q^2,$

with $\alpha = 1$ or $\alpha = 2$ in the splay mode or the twist mode respectively, we expect in these modes straight lines with a slope of + 1. The ratio K_{α}/η_{α} can be determined from the position of the line.

that their bandwidths at angles $> 5^{\circ}$ were half the bandwidths found in the homodyne experiment, just as we had expected. It is noted that the number of coherence areas, subtended by the detector is of no importance in our case since it does not affect the measured half-bandwidths at all. A typical plot of $\Delta \omega_{exp}$ versus q^2 is shown in figure 4. In our configuration (cf. Fig. 2) the following relation for q^2 holds :

$$q^{2} = \left(\frac{2 \pi}{\lambda_{0}}\right)^{2} \left\{ n_{\parallel}^{2} + n_{\perp}^{2} - 2 n_{\parallel} n_{\perp} \cos \theta \right\},$$

 $(K_1/K_2)_{\text{mix mode}}$ crosssect. 1.70 ± 0.35 0.02 0.06 1.9 ± 0.3 0.04 0.06 0.08 1.9 ± 0.3 $1.9 \hspace{0.2cm} \pm \hspace{0.2cm} 0.3$ 0.02 0.04 1.7 ± 0.3 0.04 1.91 ± 0.18 0.06 1.8 ± 0.3 0.02 1.6 ± 0.3

$$\theta = \arcsin\left(\frac{1}{n_{\perp}}\sin\theta_{\rm L}\right)$$

and where n_{\perp} and n_{\parallel} are the refractive indices of the NLC relating to the ordinary and extraordinary waves respectively (\perp and \parallel refer to electric field polarizations perpendicular and parallel to the director respectively). In order to calculate q^2 from θ_L , we used data for n_{\perp} and n_{\parallel} from Leenhouts [4]. Although the solidstate — nematic transition temperature, i.e. T_{SN} , is 44 °C we were still able to measure somewhat below this temperature because of undercooling. Figure 5 shows the experimental results for the splay/twist



Fig. 5. - Experimental data for the viscoelastic ratios $(\eta/K)_{\alpha}$ versus $T/T_{\rm NI}$ for $\alpha = 1$ (splay), circles, and $\alpha = 2$ (twist), dots.

viscoelastic ratios as a function of the reduced temperature $T/T_{\rm NI}$. The arrow indicates $T_{\rm SN}/T_{\rm NI}$.

4.2 ELASTICITY. — As was pointed out in section 3.1.3, we investigated the ratio between the splay and twist elastic constants $(K_1 : K_2)$ at different temperatures by measuring the angular intensity distribution of the scattered light as a function of the scattering angle θ , paying due attention to what we wrote in section 3.1.6.

As was proved recently by van Eck and Zijlstra [2], the time averaged anode current of the multiplier is directly proportional to the intensity of light observed by the PMT and is directly coupled with the integral of the frequency spectrum and the number of coherence areas per area of the aperture (cf. Fig. 5 of [2]). Since the solid angle subtended by the detector is independent of the scattering angle the observed anode current is proportional to the detected light intensity. Although there are alternative methods [25, 26] for deriving $K_1 : K_2$ from $I(\theta)$, we have plotted the quantities $J \equiv I/Q$ versus $(G_1^2 - G_2^2)$ (see Fig. 6). I and Q



Fig. 6. — Example of a plot of J versus $(G_1^2 - G_2^2)$ for $T/T_{\rm NI} = 0.9620$. The extrapolated values J(+1) and J(-1) give J(+1)/J(-1) which corresponds to the elastic ratio K_1/K_2 .

are defined in equation (15). We choose to plot J because it is linear with $(G_1^2 - G_2^2)$, as follows from (17) and from $G_1^2 + G_2^2 = 1$, i.e.

$$J \sim \frac{G_2^2}{K_1} + \frac{G_2^2}{K_2} = \frac{K_1 + K_2}{2 K_1 K_2} - \frac{K_1 - K_2}{2 K_1 K_2} (G_1^2 - G_2^2).$$
(25)

This relation has been verified experimentally as shown in figure 6, but it has not been verified for a few points where $(G_1^2 - G_2^2)$ goes to -1. The reason for this is that at small scattering angles the scattered light is detected with unscattered light.

If one considers J as a function of $G_1^2 - G_2^2$ it follows from equation (25) that $K_1/K_2 = J(-1)/J(+1)$. Hence it is possible to determine $K_1 : K_2$ by extrapolating the curve. The range of scattering angles is limited by the dimensions of the heat stage holder. Figure 7 shows the experimental results for the splay/ twist elastic ratio as a function of the reduced temperature $T/T_{\rm NI}$ obtained from the angular distribution of the scattered light. This figure also shows the results obtained with the mixture mode technique (cf. section 3.1.5). The dashed line is the best fit to the data from Leenhouts [19]. $T_{\rm SN}/T_{\rm NI}$ is indicated by an arrow.



Fig. 7. — The elastic ratio K_1/K_2 versus the reduced temperature $T/T_{\rm NI}$. The dots are from the intensity measurements. The circles are from the spectral density measurements. The broken curve is from Freedericksz transition data [19].

5. Discussion. — 5.1 VISCOSITY. — As was suggested in section 3.2.1, we plot η_1/η_2 versus the reduced temperature, as is shown in figure 8. In order to calculate η_1/η_2 we can use the data for $K_1 : K_2$ obtained from the angular dependency distribution of the scattered light. We can conclude that for all points except one $\eta_1/\eta_2 \leq 1$, as expected from equation (22).

Fig. 8. — $\eta_1/\eta_2 \equiv \eta_{splay}/\eta_{twist}$ versus T/T_{NI} , from calculations of η_2/K_2 and η_1/K_1 with (K_1/K_2) obtained from the angular dependency of the scattered light.

Investigations of the order and temperature dependence of η_1 and η_2 were carried out as suggested in 3.2.2 using experimental data for $\Delta \chi^{g}$, K_1 and K_2 from Leenhouts [18, 19]. Because neither β nor $\varepsilon(S)$ can be determined directly we chose values for β and $\varepsilon(S)$ and then tested them. We chose $\beta = 0$, 1 and 2 and $\varepsilon(S) = \varepsilon_0 S$ and ε_0 . By dividing the values of η_2 and η_1 by $(\Delta \chi^{g}) \sim (S)^{\beta}$ we compensate the factor S^{β} . The logarithmic value of these results ought then to be of the type $\varepsilon(S)/kT$. Assuming that $\varepsilon(S)/kT \sim 1/T$ or $\sim S/T$ we can now plot these values versus T^{-1} or $\Delta \chi^{g}/T$. The curve which fits best to a straight line then provides us with the most acceptable values for β and $\varepsilon(S)$.

In figures 9a to 9f six plots are shown; we can conclude that the rotational or twist viscosity shown in figure 9f fits best to a straight line. It follows that

$$\eta_2 = \gamma_1 = c \cdot \exp(\varepsilon_0 S/kT) \,. \tag{26}$$

As a matter of fact, if we, like Prost [6], consider the kinematic viscosity $v_{\alpha} = \eta_{\alpha}/\rho$ instead of the dynamic viscosity η_{α} no difference is observed, within the accuracy of the data. Since the T and S dependence of γ_1 is determined mainly by the exponential, the exponent of the pre-exponential factor cannot be determined unambiguously. One can only hope to obtain better information about the pre-factor in the range of temperatures where S changes strongly with temperature. Therefore measurements of γ_1 will have to be done in the proximity of the nematic isotropic transition temperature.

From the slope of the curve in figure 9f we calculated ε_0 in equation (26), where we took $S_{\rm NI} = 0.31$ from Leenhouts [18]. We get $\varepsilon_0 = 0.22$ eV, while from the mean field theory [24] it follows that $\varepsilon_0 \approx 0.2$ eV, so these results are in rather good agreement.

As was pointed out in section 3.2.1 the splay viscosity should be written as a combination of viscosity terms. On the other hand, there is no theoretical analysis available from which we can predict how η_1 will behave as a function of temperature or of order. Figure 9f shows, however, that this dependence is the same as that found for η_2 but not at temperatures close to the nematic isotropic transition temperature.

5.2 ELASTICITY. — Figure 7 shows that the data for the splay/twist elastic ratio obtained from the angular distribution of the scattered light and those obtained from the mixture mode agree within the accuracy of the measurements. Data obtained from Freedericksz transitions [19], however, are about 10 %-20 % lower than our values. This systematic difference was also observed for other nematics such as N₄ and DIBAB [25, 27]. At present no satisfactory reason for this difference has been found. One argument could be that in the case of the Freedericksz experiment the condition of strong anchoring was not fulfilled, although investigations done with a variety of sample thicknesses [19] demonstrate that this condition



Fig. 9. — The natural logarithm of combinations of η_{α} and $\Delta \chi^{g}$ with $\alpha = 1$ (splay), circles, and $\alpha = 2$ (twist), dots, plotted versus $T_{\rm NI}/T \sim T^{-1}$ and versus

$$(\Delta \chi^{\rm g}/T)/(\Delta \chi^{\rm g}/T)_{\rm NI} \sim S/T$$

in order to determine the order parameter dependency of the twist viscosity. Obviously η_{twist} versus $(\Delta \chi^{g}/T)/(\Delta \chi^{g}/T)_{\text{NI}}$ fits best a linear function, so $\eta_{\text{twist}} (=\cdot \gamma_1) = c \cdot \exp(\epsilon S/kT)$.

was fulfilled. Another criticism is that the volume dependence of the Freedericksz transition is neglected in the theory because its derivation is based on the Helmholtz free energy for distortion, which implies constant volume. This assumption is doubtful, however, because the distortion of the nematic by the magnetic field will certainly change the volume. In practice one always works at constant pressure, so the Gibb's free energy should be used.

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